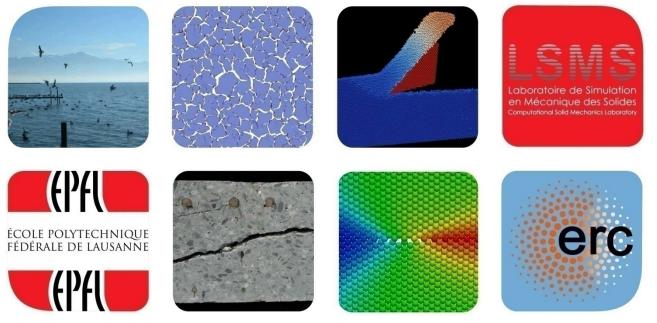
### Numerical modeling of sliding contact J.F. Molinari

- 1) Atomistic modeling of sliding contact; P. Spijker, G. Anciaux
- 2) Continuum modeling; D. Kammer, V. Yastrebov, P. Spijker

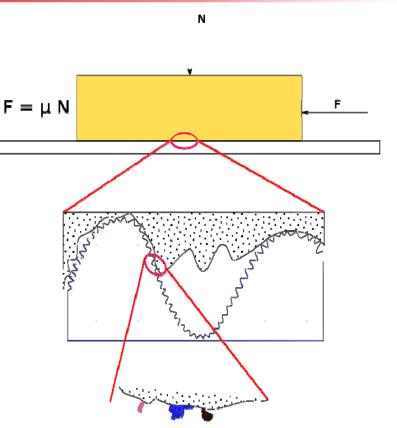
#### ICTP/FANAS Conference on Trends in Nanotribology, 2011



# Motivation

#### Friction: one of the great unsolved mystery

- Can we explain the microscopic origins of friction ? (nm)
- What happens inside an earthquake ? (km) (rated by livescience as top mystery)
- Challenge of scales (time and length)
- Complex physics (plasticity, surface roughness, third body interactions, adhesion, chemistry...)

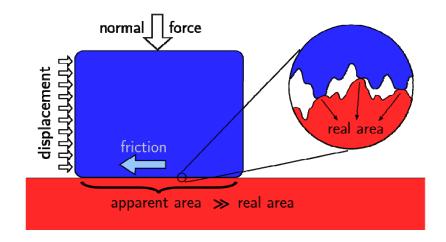






# A quick introduction

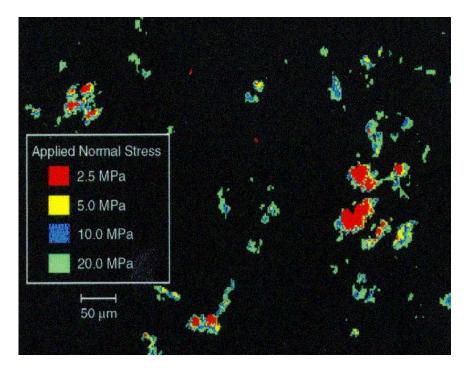
#### Historical notes on friction research



- Bowden and Tabor (1950)
  - real vs. apparent contact area
  - contact surface is rough
  - number of contacting asperities increases with load (confirmed by Dieterich)
- Theoretical models:
  - Greenwood and Williamson
  - Persson

# According to Da Vinci, Amontons, and Coulomb, **friction** is ...

- ... proportional to load
- ... independent of contact area
- ... independent of sliding speed



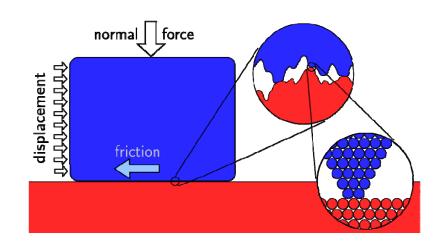


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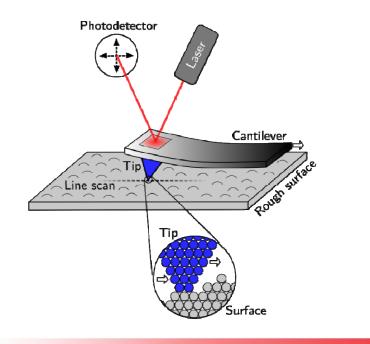
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## Toward the atomistic scale

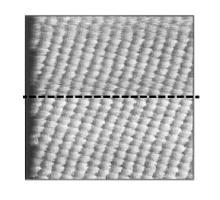
#### Nanotribology



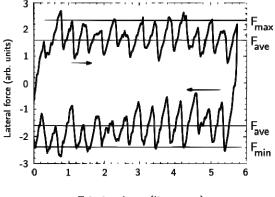
- Magnification until atomic level
- Domain of nanotribology
- Elucidate molecular origins of friction



• Experimental techniques include AFM



Lateral force image (6x6 nm)



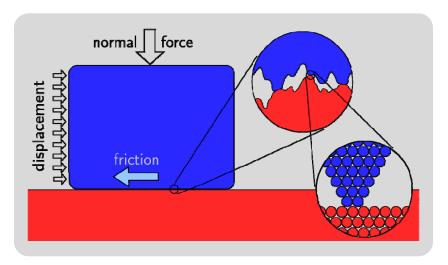


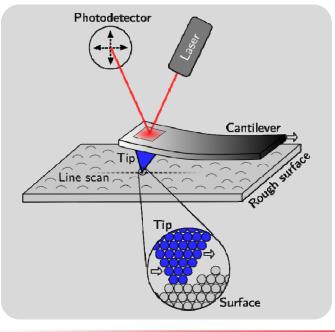




# Influence of roughness

#### Open questions...



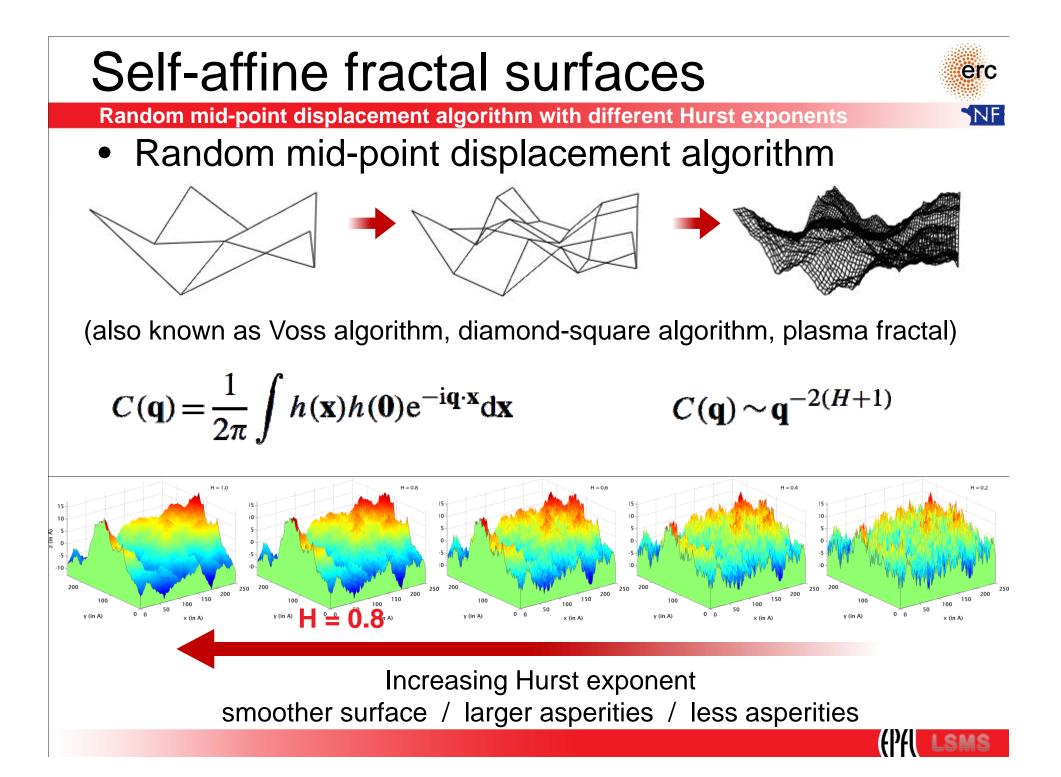


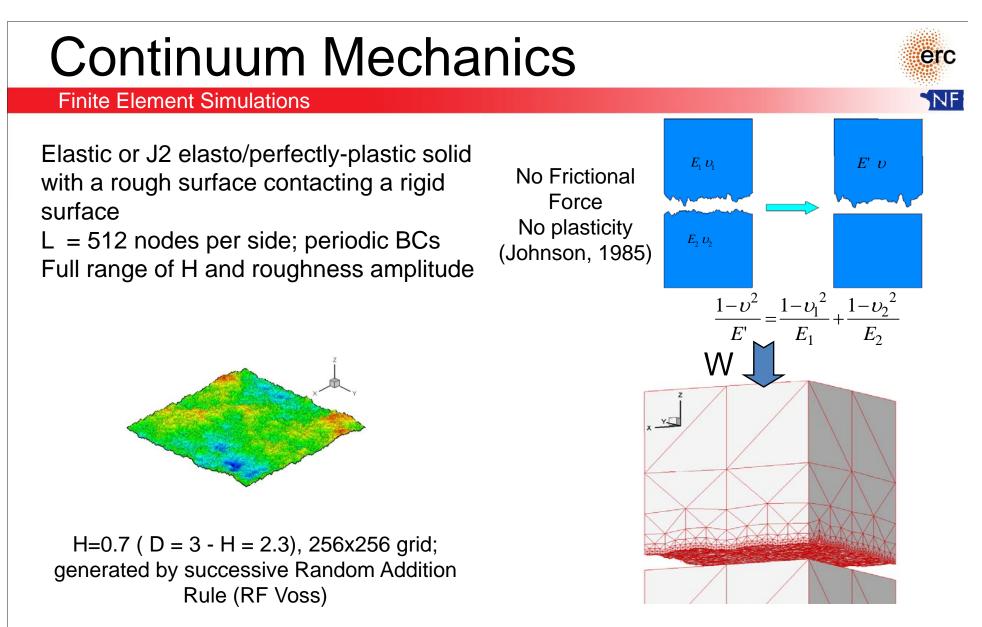
- Roughness generally not included in Molecular Dynamics modeling (flat on flat, or single tip on flat)
- Computed friction coefficients tend to be low
- Roughness, plasticity (wear) dominate at the engineering scale
- Objective: investigate atomic scale roughness
- Existence ?
- How does it influence friction?



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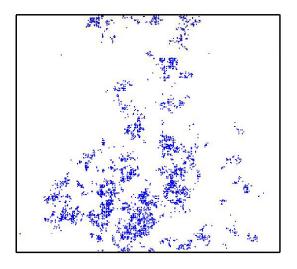


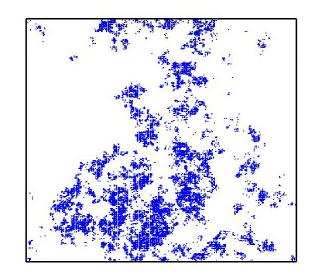


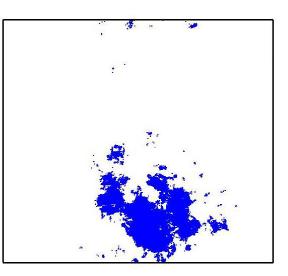
• S. Hyun, L. Pei, J.F. Molinari, and M.O. Robbins, "Finite-element analysis of contact between elastic self-affine surfaces", *Phys. Rev. E*, 2004

• L. Pei, S. Hyun, J.F. Molinari, and M.O. Robbins, "Finite-element analysis of contact between elastoplastic self-affine surfaces", *Journal of the Mechanics and Physics of Solids, 2006* 

### Complex contact morphology

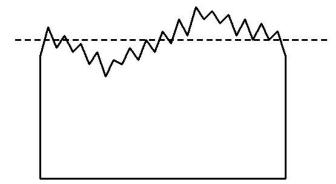






Elastic contact with A=0.0125

Elasto-plastic contact, A=0.0335 Perfectly plastic (more contact area for fixed W) Overlap or cut-off model, A=0.03



Overlap model way off: asperities elastic (long range) interactions matter!

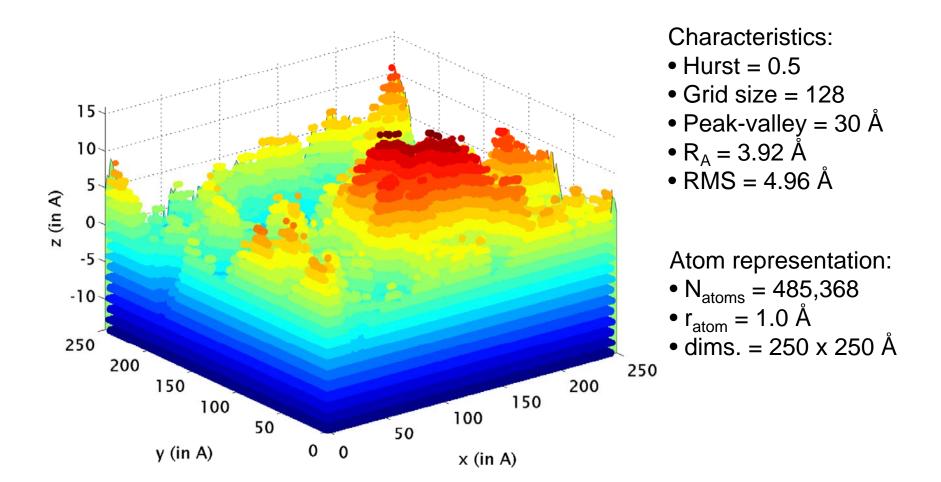
Morphology dominated by small contact clusters



## Atomic rough surfaces

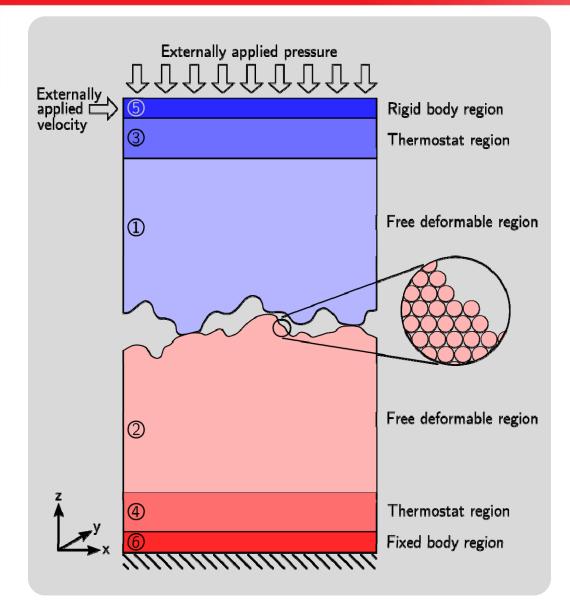
#### Top a mesoscale asperity







# MD simulation set-up



#### Material

- aluminium (FCC structure)
- diameter: 0.291 nm / mass: 27 g/mol
- Young's modulus: 68 GPa / v: 0.35

#### Potential

- Lennard-Jones
- bulk-energy: 10.3 kJ/mol
- gap-energy: 0.103 kJ/mol (weak adhesion)

#### System set-up

- 6 different regions
- dimensions: 13 x 13 x 26 nm (periodic)
- 185,000 to 240,000 particles
- top domain rotated by 21 degrees
- Langevin thermostat close to 0 K

#### Simulations (all 10 ns with 5 fs time step)

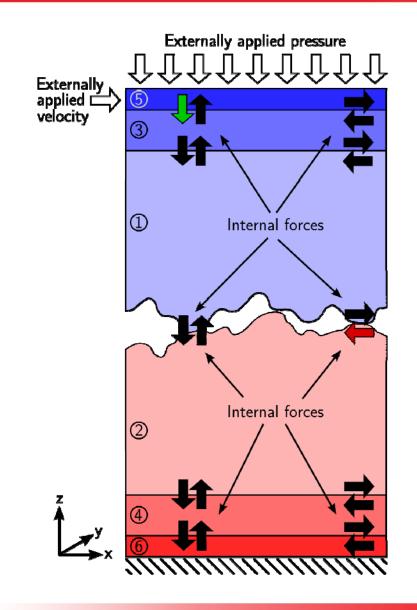
- 3 rough surfaces (0.2, 0.5, 1.0 nm)
- for every RMS 3 different surfaces
- 5 applied pressures (0.05 0.25 GPa)
- 3 high sliding speeds (2, 10, 50 m/s)



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# Simulation analysis

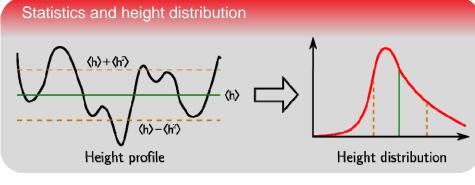


#### **Global forces**

- decompose forces per region
- allows to compute global  $\mu = F/F_N$

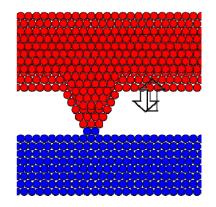
#### Change of surface characteristics

- RMS roughness / RMS slope
- Skewness, flatness



#### Contact area

- retype particles if necessary
- projected on xy-plane
- compute `true' contact area



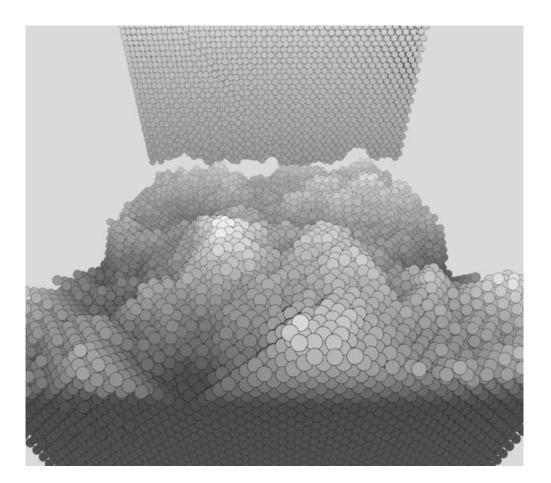


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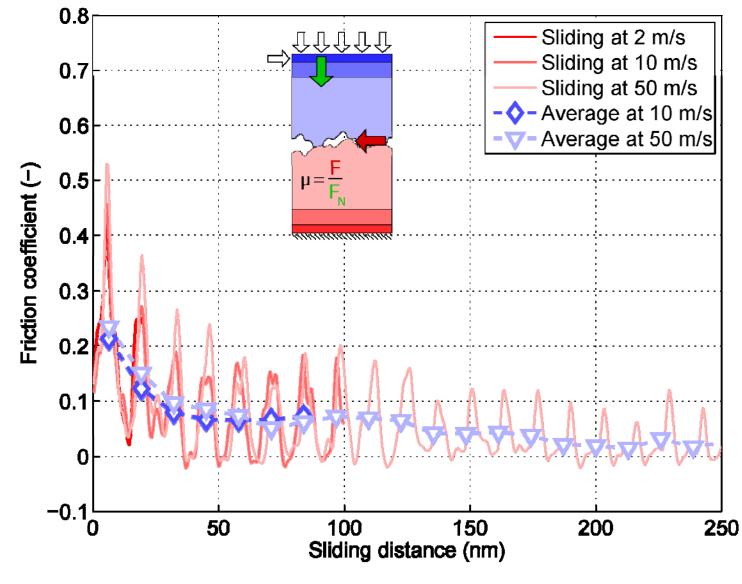
### Animation







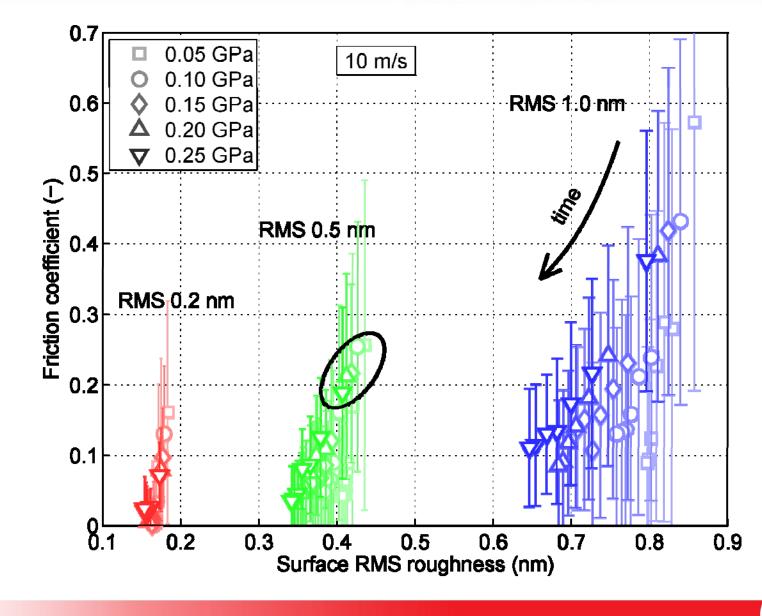
#### Friction coefficient vs. time (RMS roughness 0.5 nm / load 0.20 GPa)







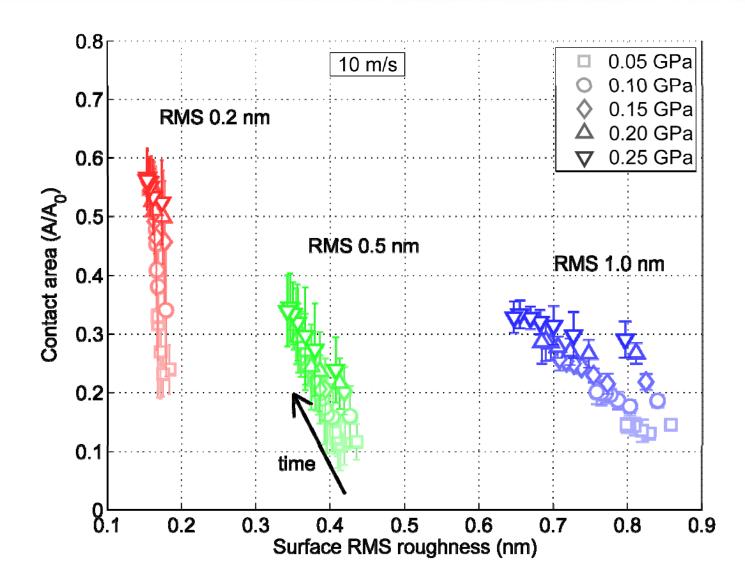
#### Friction coefficient vs. roughness







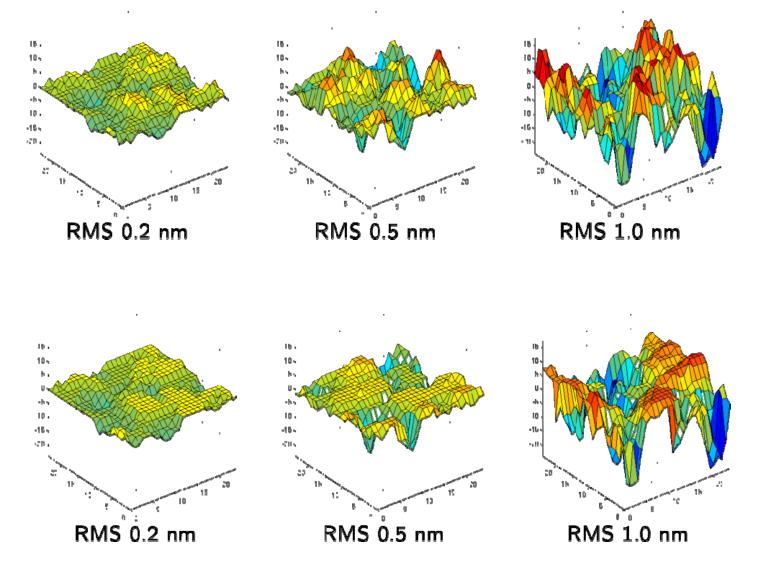
#### Surface roughness vs. contact area







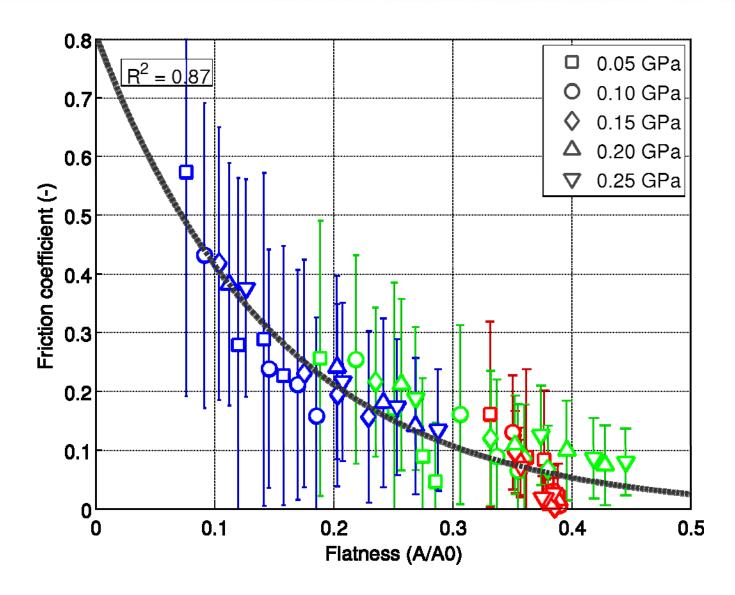
Flattening of surfaces; threshold = 20% difference in height between points







#### Flatness vs. friction; exponential decay

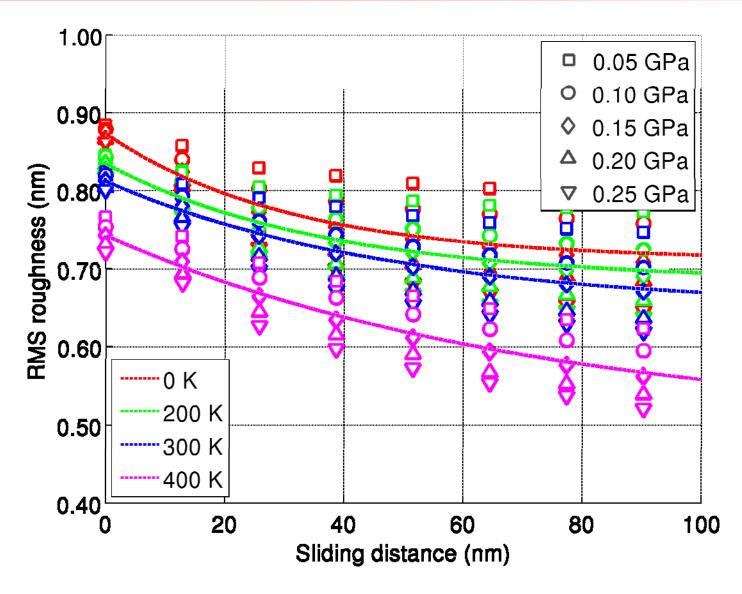






### Influence of temperature

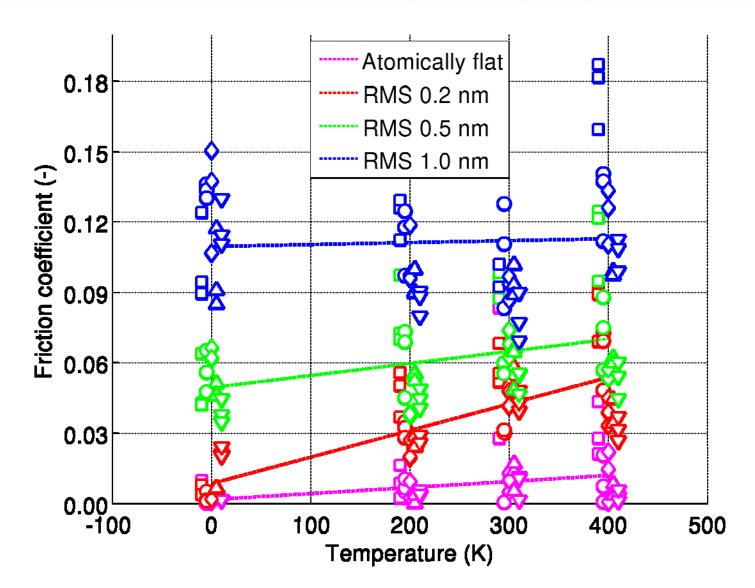
#### Change in roughness; 1 nm RMS roughness







Thermal effect – Friction coefficient vs. temperature



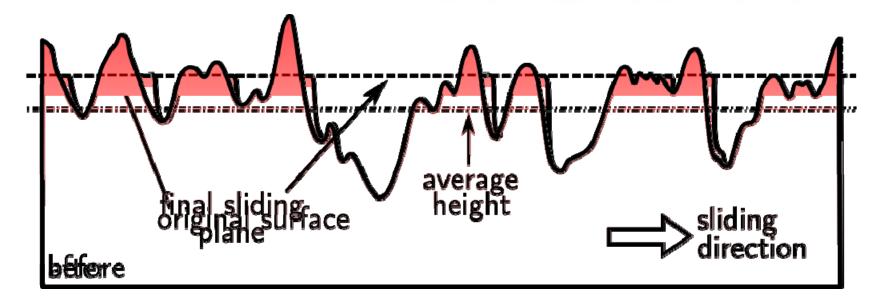


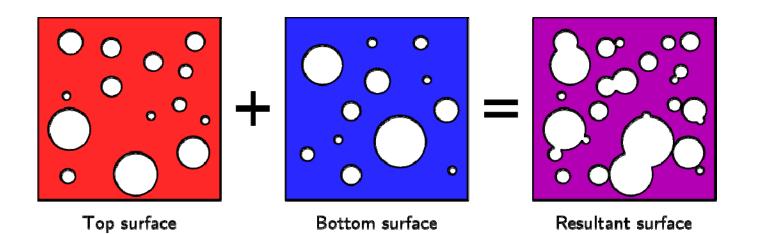






#### View on friction of rough surfaces





A 2D depiction of the sliding plane



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# Summary 1



- Rough deformable on rough deformable MD model
- Key role of roughness
  - Gives « *realistic* » friction coefficients
  - Geometric effect: friction proportional to number of atom direct collisions (scales with RMS roughness)
- But roughness decreases quickly (exp decay of friction with flatness)
- What is roughness at atomic scale?
  - Reserve of « fresh » (i.e. rough asperities)
  - Mechanisms for roughness creation? (ex: third bodies)

Publications: Comput. Mech., DOI: 10.1007/s00466-011-0574-9 (2011) Tribol. Lett., DOI: 10.1007/s11249-011-9846-y (2011) Tribol. Int., submitted (2011)



### Large scale sliding

Mode II Fracture vs. Initiation of Dynamic Sliding

- Continuum scale
- Onset of sliding
- Friction or Fracture?



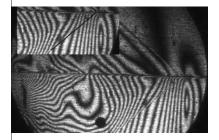




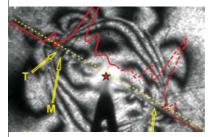
### Lab earthquakes

Experimental results for quasi-static shear loading

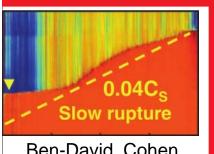




Coker, *Lapusta, Rosakis* JMPS 2005

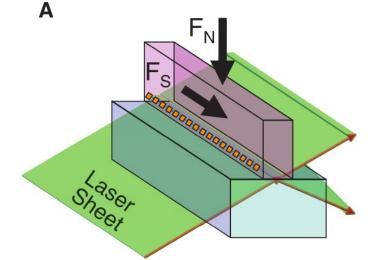


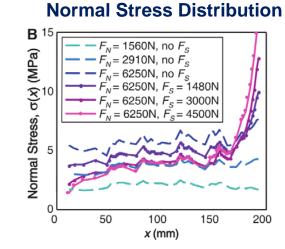
Lu *et al.* PNAS 2007



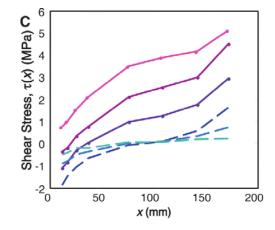
Ben-David, Cohen, Fineberg, Science 2010

#### PMMA Interface under Quasi-static Shear Loading





#### **Shear Stress Distribution**





### Lab earthquakes

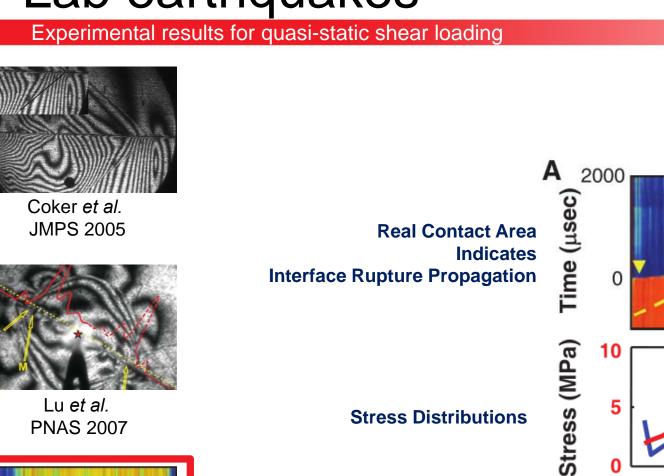
0.04Cs

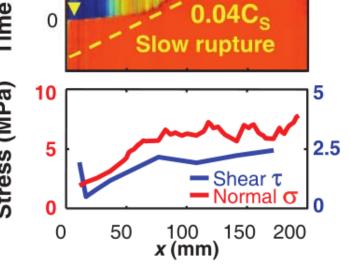
**Slow rupture** 

Ben-David *et al.* Science 2010



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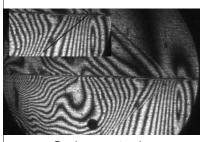




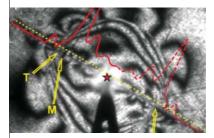
### Lab earthquakes



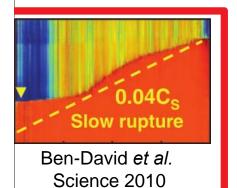
Experimental results for quasi-static shear loading



Coker *et al.* JMPS 2005

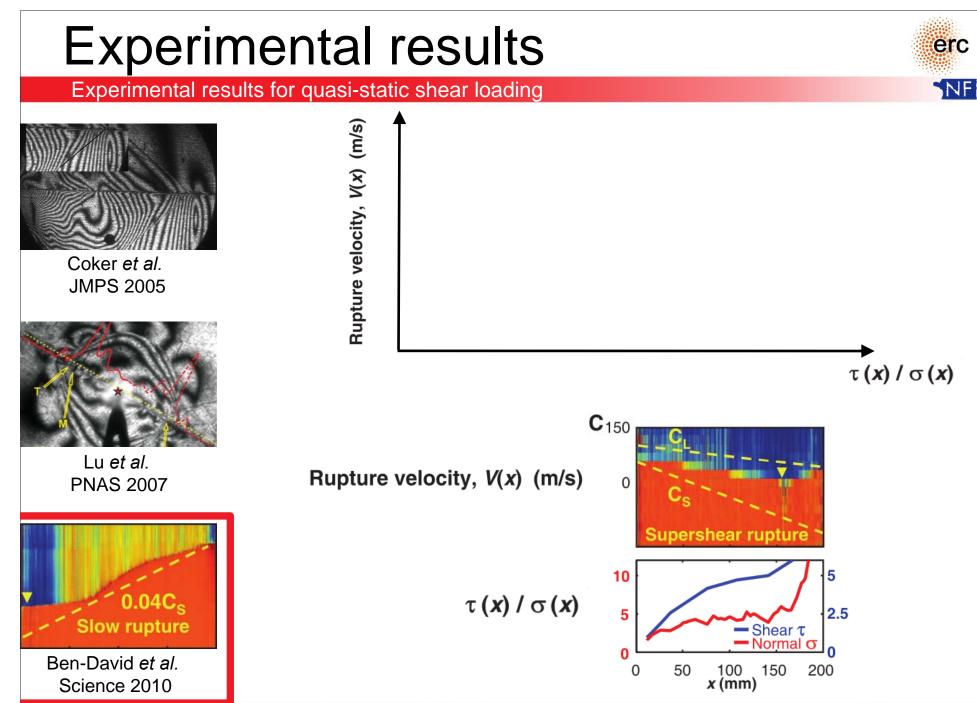


Lu *et al.* PNAS 2007

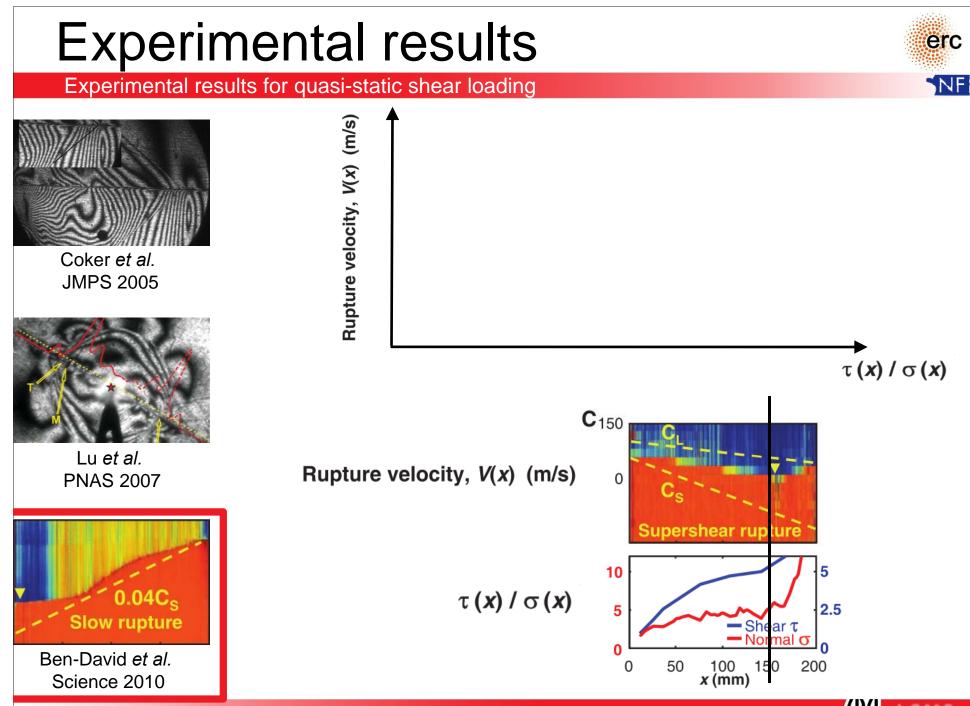


 ${f B}_{400}$ **C**150 **A** 2000 Time (µsec) 0 0 0.04C 0 Sub-Rayleigh **Slow rupture** rupture Supershear ruptur Stress (MPa) 10 10 5 5 10 2.5 2.5 5 5 2.5 Shear  $\tau$ Normal  $\sigma$ Shear  $\tau$ Normal  $\sigma$ - Shear  $\tau$ -Normal o 0 0 0 O 100 150 200 **x (mm)** 100 150 **x (mm)** 100 150 200 x (mm) 0 50 0 50 200 0 50 **D**(150) 150 0 **F** 300 **E** 300 150 150 0 Ω Stress (MPa) 7.5 7.5 15 7.5 15 Shear  $\tau$ Normal  $\sigma$ Shear τ Normal σ Shear τ Normal σ 10 5 10 10 5 5 2.5 2.5 5 2.5 5 5 0 100 150 200 **x (mm)** 100 150 **x (mm)** 100 150 **x (mm)** 50 0 50 200 0 50 200 0

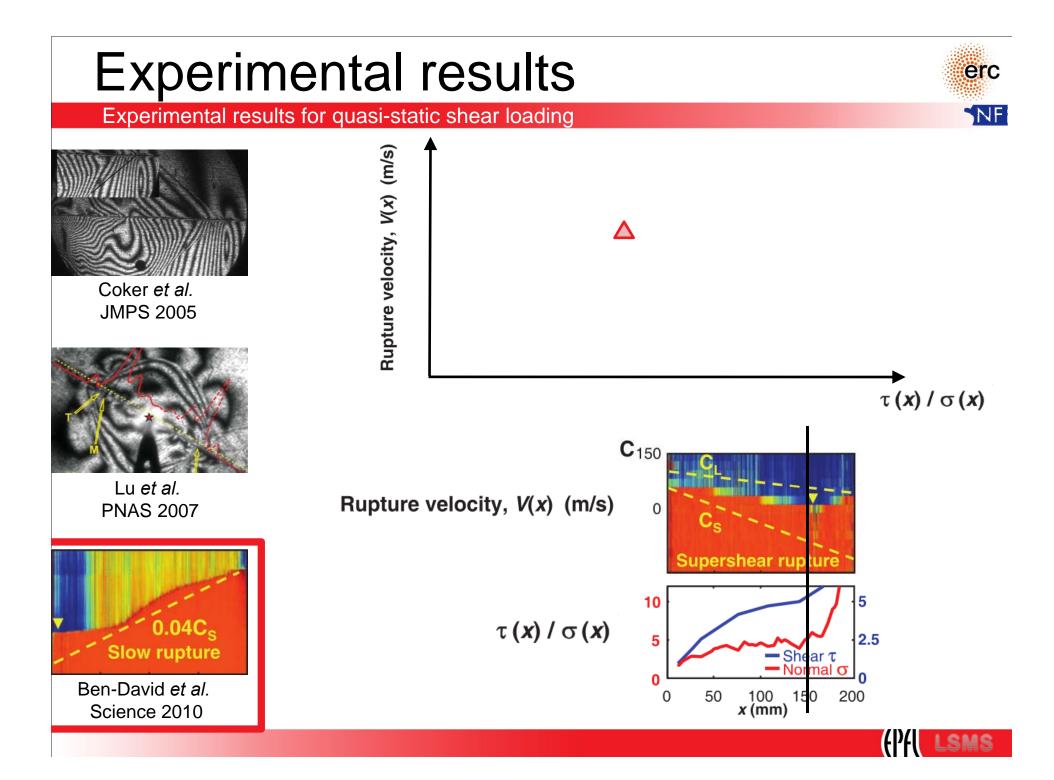


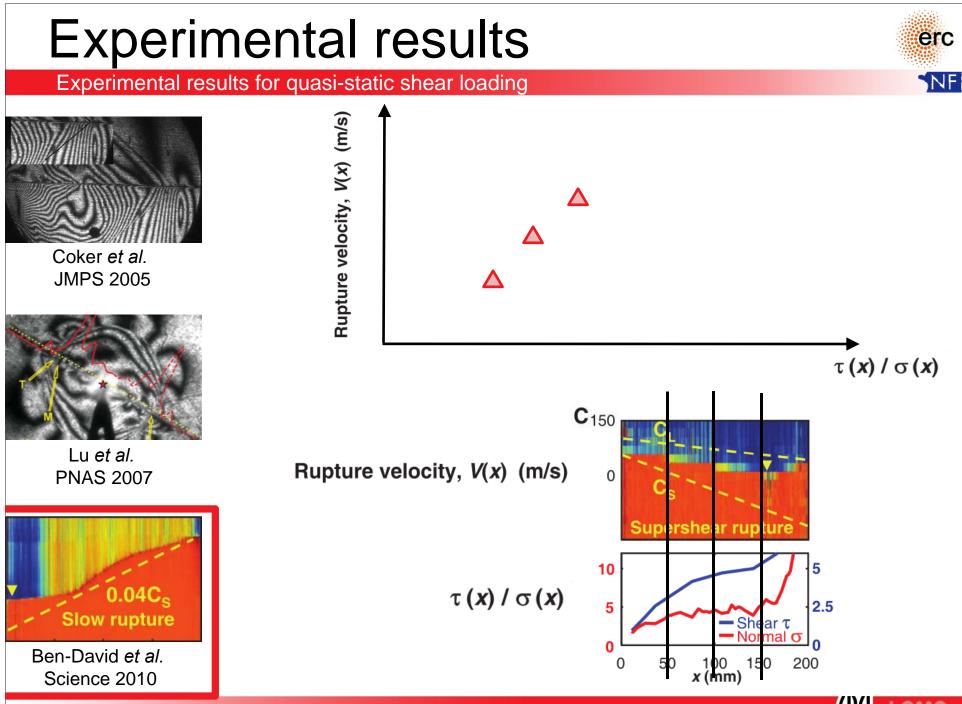










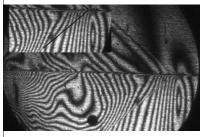




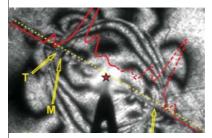
### **Experimental results**



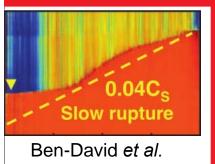




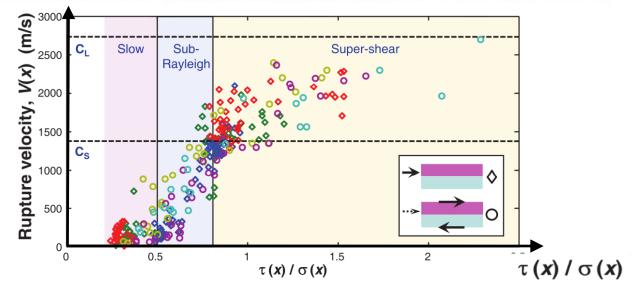
Coker et al. **JMPS 2005** 

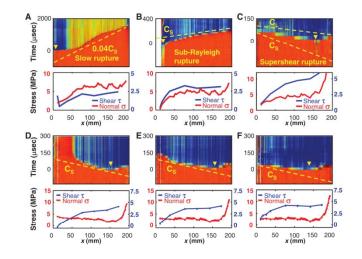


Lu et al. **PNAS 2007** 



Science 2010

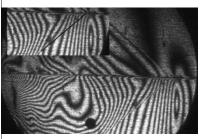




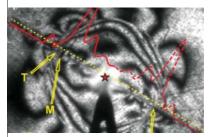


## **Experimental results**

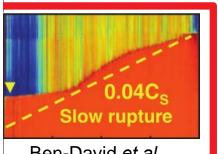
Experimental results for quasi-static shear loading



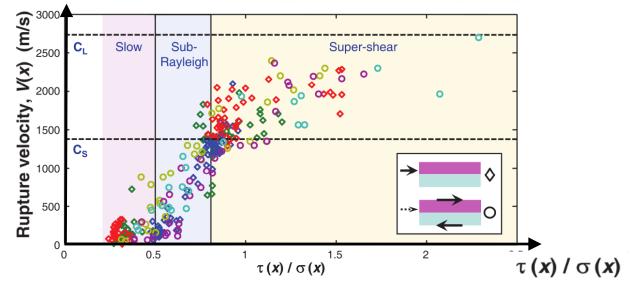
Coker *et al.* JMPS 2005



Lu *et al.* PNAS 2007



Ben-David *et al.* Science 2010



Features:

All modes of rupture velocity reproduced Local friction can be much higher than macroscopic value Key role of heterogeneities

#### Fracture energy analogy:

#### More energy needed to break interface

→higher local interface strength

- $\rightarrow$  more real contact area
- $\rightarrow$  more local normal stress



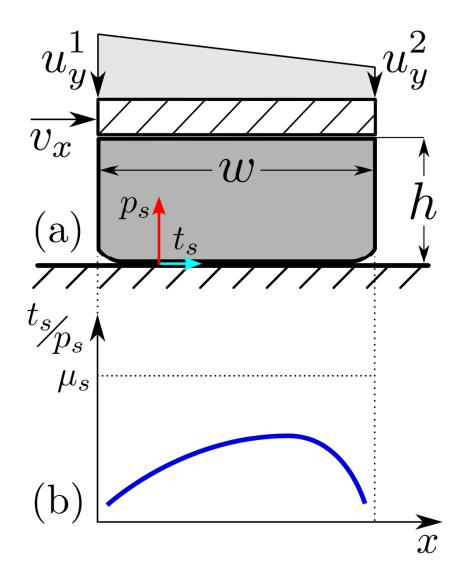
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### Numerical model

Explicit FE; energy-conserving contact

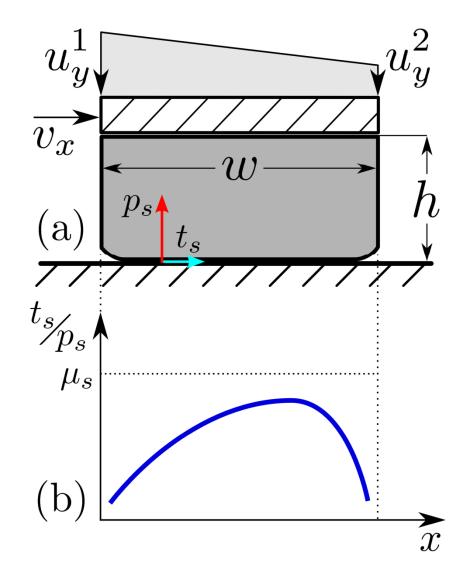






### Problem setup

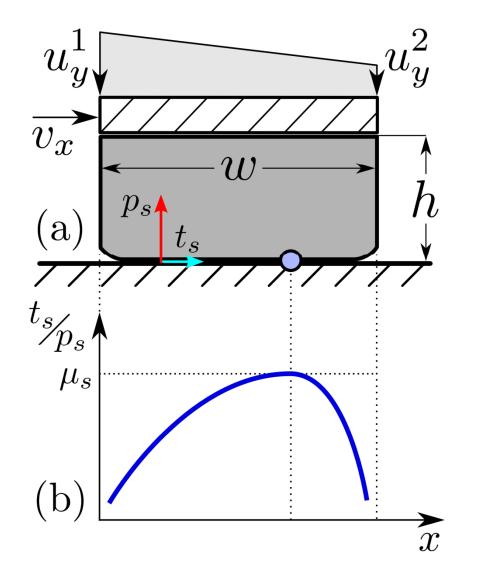






### Problem setup

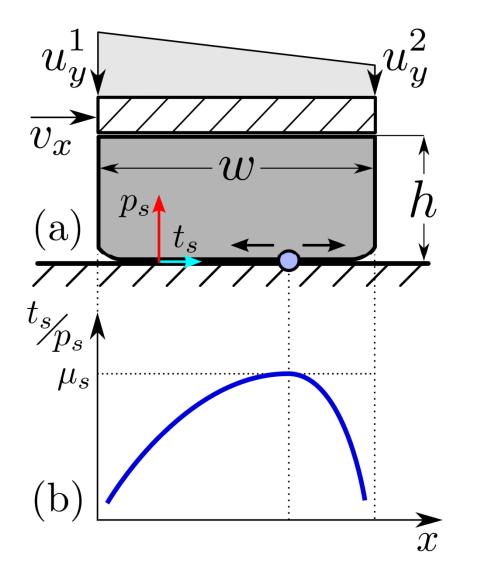






### Problem setup

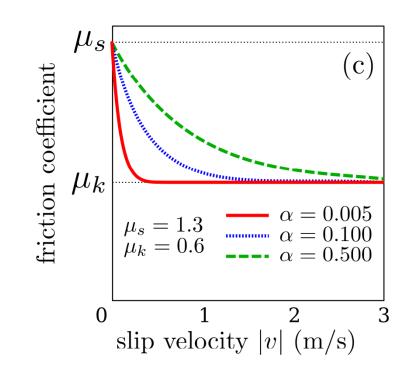






# Velocity weakening friction law

Tangential resistance is proportional to the contact pressure

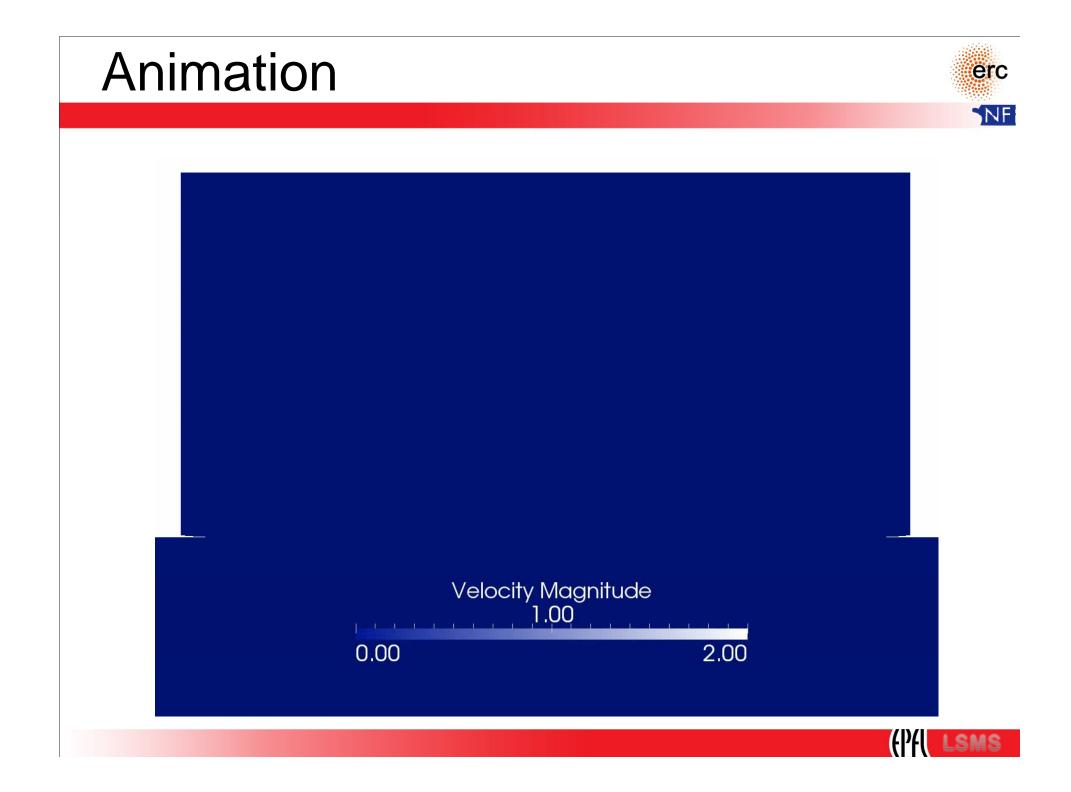


$$\mu = \mu_{s} + (\mu_{k} - \mu_{s})(1 - \exp(-|v|\sqrt{(\mu_{s} - \mu_{k})/\alpha})),$$

v is the material slip velocity,  $\mu_s$ ,  $\mu_k$  are the static and the kinetic friction coefficients,  $\alpha$  is the transition parameter

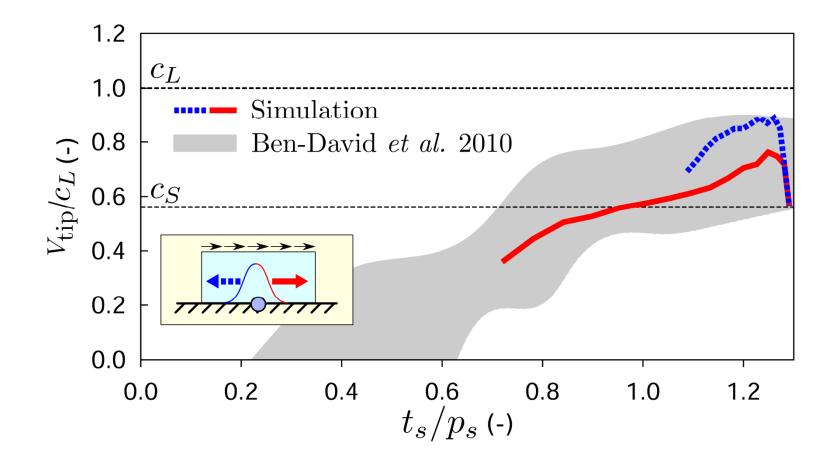


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### Comparison with experiments

Matches but... non uniqueness of Vtip

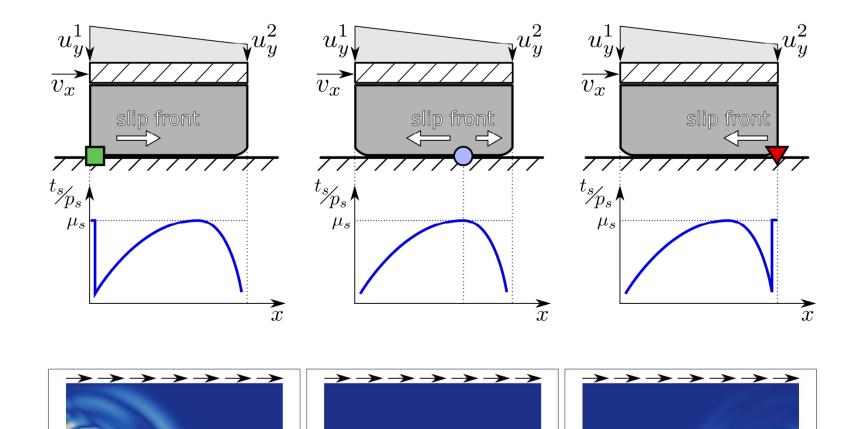




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#### Spontaneous and triggered slip initiations

#### **Directionality effect?**



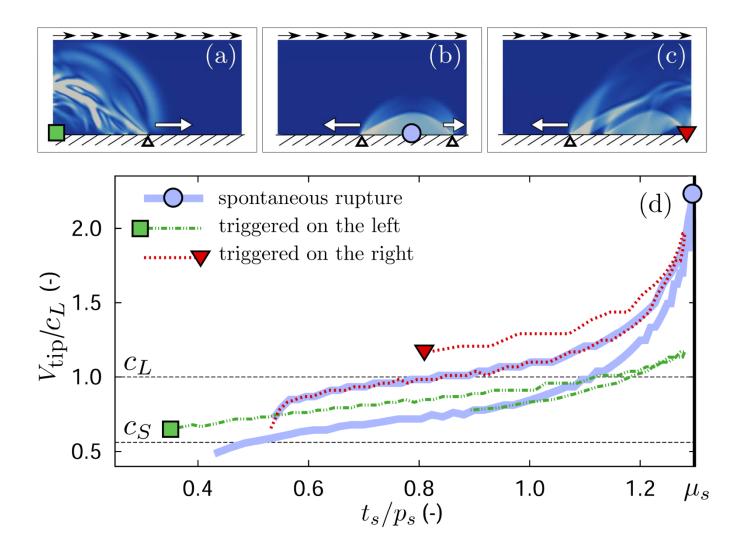
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#### Spontaneous and triggered slip initiations

#### **Directionality effect?**

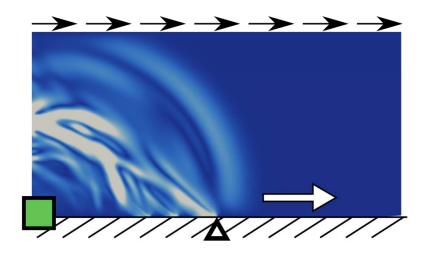


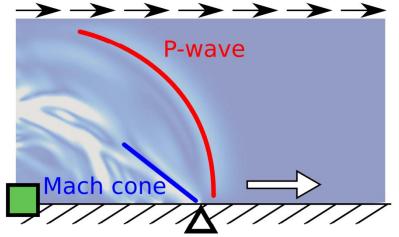


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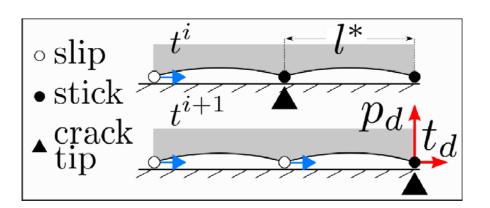
### In front of the slip front

#### Things change ...





Tip of the slip front



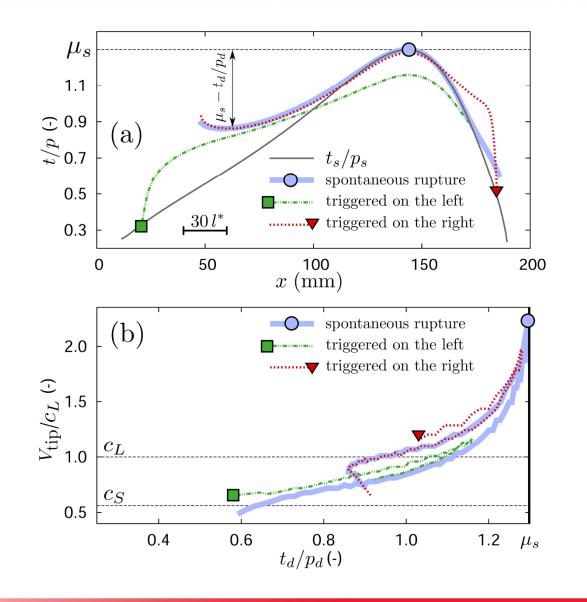




### In front of the slip front

#### Dynamic effects help



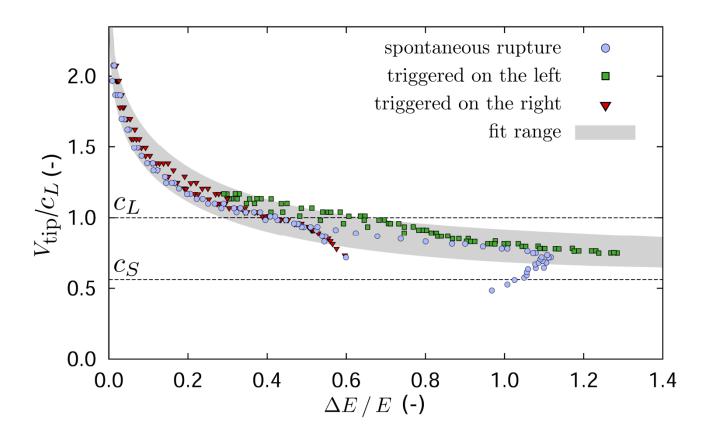




### Slip velocity as a function of local energy

Back to fracture mechanics analogy

$$\Delta E/E = \frac{E_{\text{needed}} - E_{\text{stored}}}{E_{\text{stored}}}$$

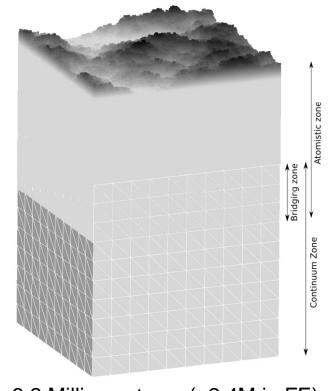




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# Conclusions

- Simple model gives consistent observations (with Ben-David et.al 2010 Science paper)
  - Tau-Sigma ratio exceeds global friction coefficient
  - Rupture velocity depends on local tau-sigma ratio
- Additional observations
  - Different rupture modes
  - Non uniqueness of Vtip
  - Explained by energy flux (dynamics)
- Perspectives
  - More sophisticated friction law
  - Deformable-deformable contact
  - Interface heterogeneity
  - Access dynamic fields experimentally
- Adding roughness would be nice
  - At what scale roughness breaks down?
  - Challenge for multiscale modeling



3.2 Millions atoms (+2.4M in FE) Isms.epfl.ch

