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International Centre for Theoretical Physics**



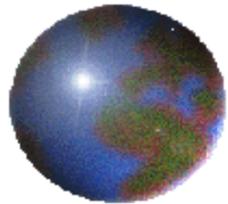
2333-1

**Workshop on Science Applications of GNSS in Developing Countries
(11-27 April), followed by the:
Seminar on Development and Use of the Ionospheric NeQuick Model
(30 April-1 May)**

11 April - 1 May, 2012

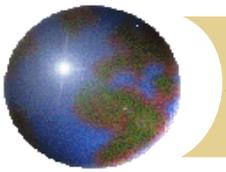
Evolution to Modernized GNSS Ionospheric Scintillation and TEC Monitoring

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*AJ Systems/GPS Silicon Valley
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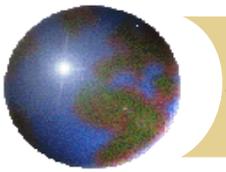
*Evolution to Modernized GNSS
Ionospheric Scintillation and TEC
Monitoring*

Dr. A.J. Van Dierendonck, AJ Systems

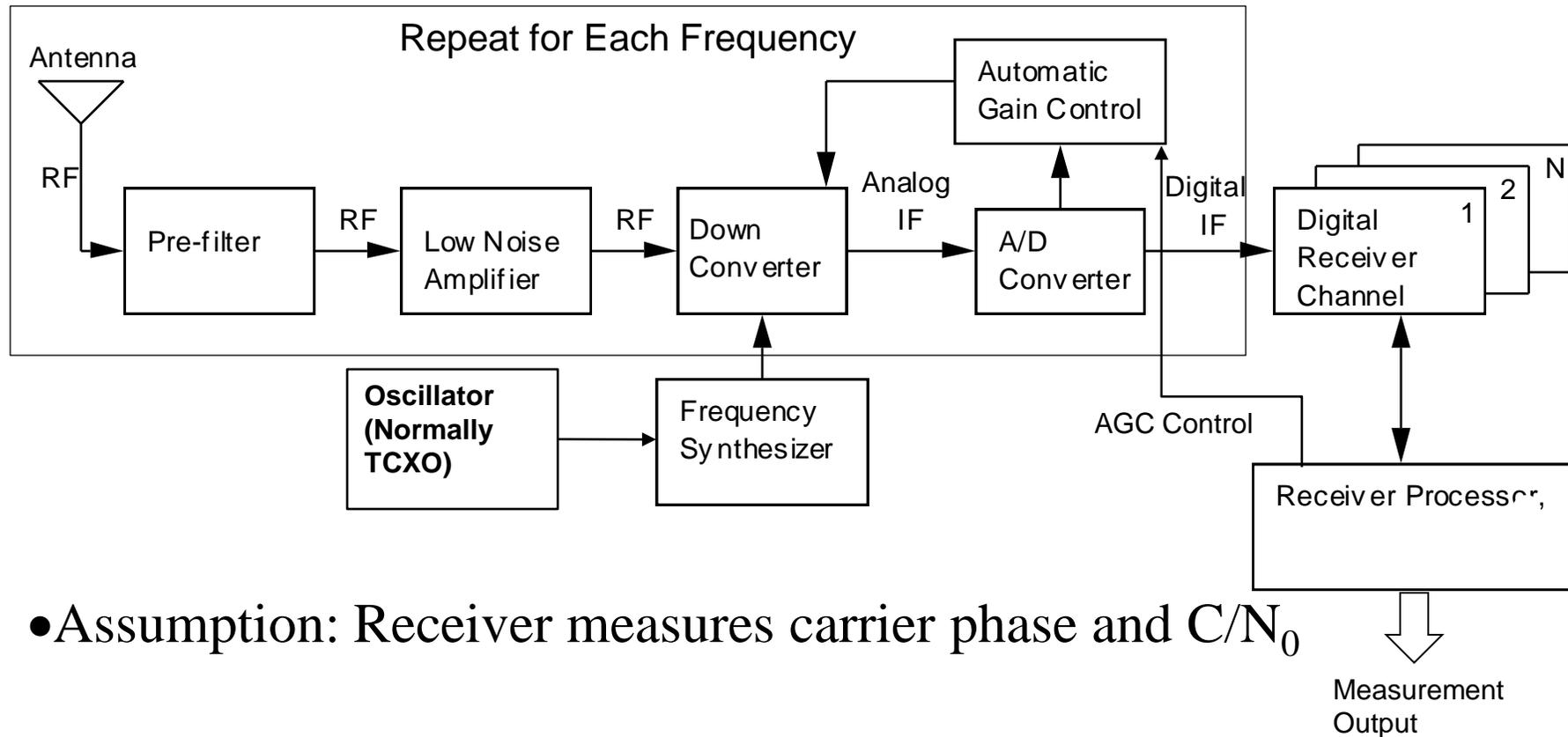


Tutorial Outline

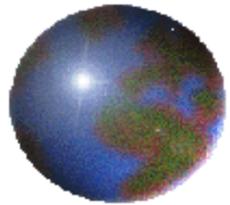
- ⊕ Short Review of GPS Receivers
 - ⊞ Emphasizing what functions are affected by scintillation
 - ⊞ Emphasizing modifications implemented for measuring scintillation effects
- ⊕ Amplitude and Phase Scintillation Measurements
- ⊕ Measurement Limitations
 - ⊞ How well does the receiver perform in a scintillation environment?
 - ⊞ How can a GNSS receiver be designed to better operate in a scintillation environment?
- ⊕ TEC Measurements
 - ⊞ Measuring TEC or satellite and/or receiver inter-frequency biases?
- ⊕ Example Measurements
 - ⊞ GPS Satellites
 - ⊞ SBAS Geostationary Satellites



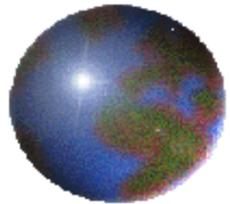
Multiple Frequency GNSS Receiver Functional Block Diagram



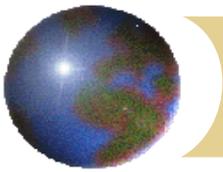
- Assumption: Receiver measures carrier phase and C/N_0



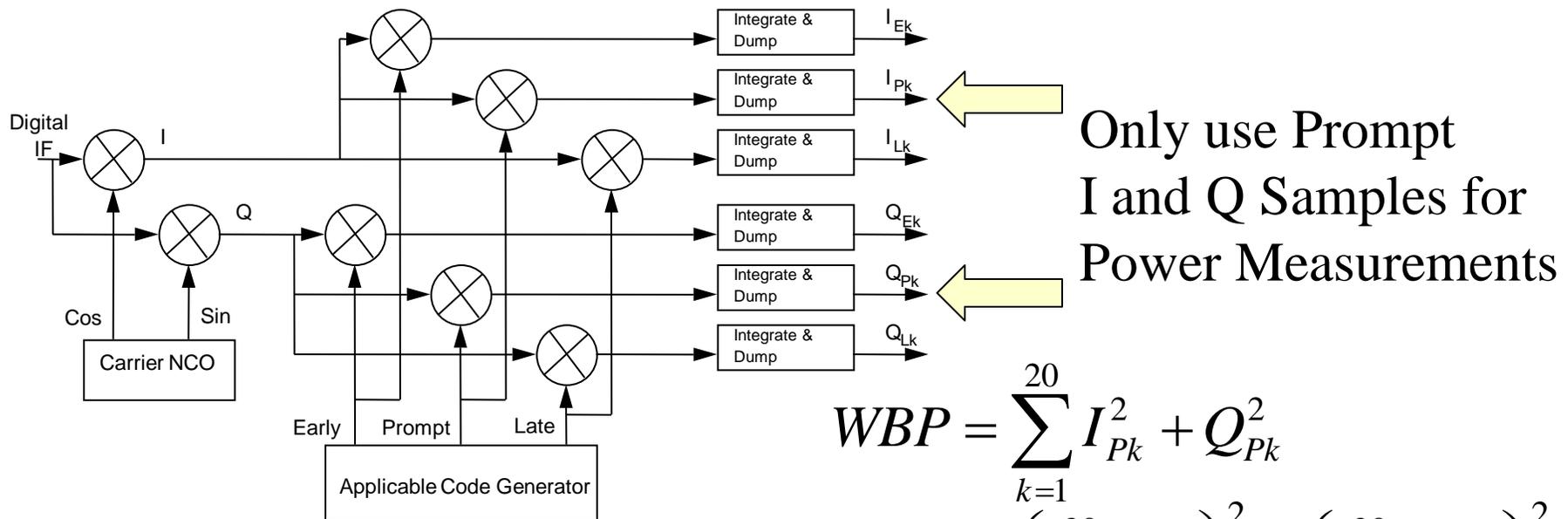
GNSS Receiver Modifications for Scintillation Monitoring



Measuring Amplitude Scintillation

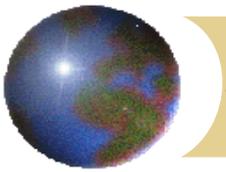


Typical Receiver Channel for Amplitude (Power) Measurements



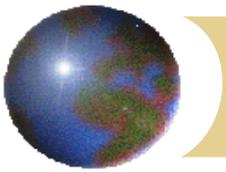
$$WBP = \sum_{k=1}^{20} I_{Pk}^2 + Q_{Pk}^2$$

$$NBP = \left(\sum_{k=1}^{20} I_{Pk} \right)^2 + \left(\sum_{k=1}^{20} Q_{Pk} \right)^2$$



Signal Intensity Samples

- ⊕ Signal Intensity samples are based upon Narrowband (NBP) and Wideband (WBP) Power Measurements (50 samples/second)
 - ⊕ $SI_k = NBP_k - WBP_k$
 - ⊕ Difference between NBP and WBP is proportional to received signal power
 - Theoretically cancels noise power in the mean
 - Practically, it doesn't completely – correction made later
- ⊕ Samples collected and stored over 60 seconds
 - ⊕ Thus, 3000 samples every minute
 - ⊕ These 50 sps samples are available as an output



Computing S4 (1)

- ✦ Total S4 is standard deviation of normalized Signal Intensity

- ✦
$$S4_{Total} = \sqrt{\frac{\langle SI_k^2 \rangle - \langle SI_k \rangle^2}{\langle SI_k \rangle^2}}$$

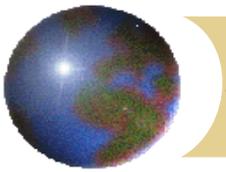
- ✦ Scale factor of Signal Intensity is ambiguous, but this normalization with average value over 60 seconds takes care of that

- ✦ Desirable to remove the effects of receiver noise, theoretically computed as

- ✦
$$S4_{N_0} = \sqrt{\frac{100}{\hat{S}/N_0} \left[1 + \frac{500}{19 \hat{S}/N_0} \right]}$$

- ✦ This is square root of expected value of $S4^2$, given noise only

- ✦ \hat{S}/N_0 is average measured signal-to-noise density over 60 second period – also an output, as well as the above noise contribution

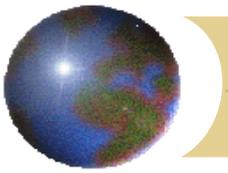


Computing $S4$ (2)

- ✚ Noise contribution is removed as follows:

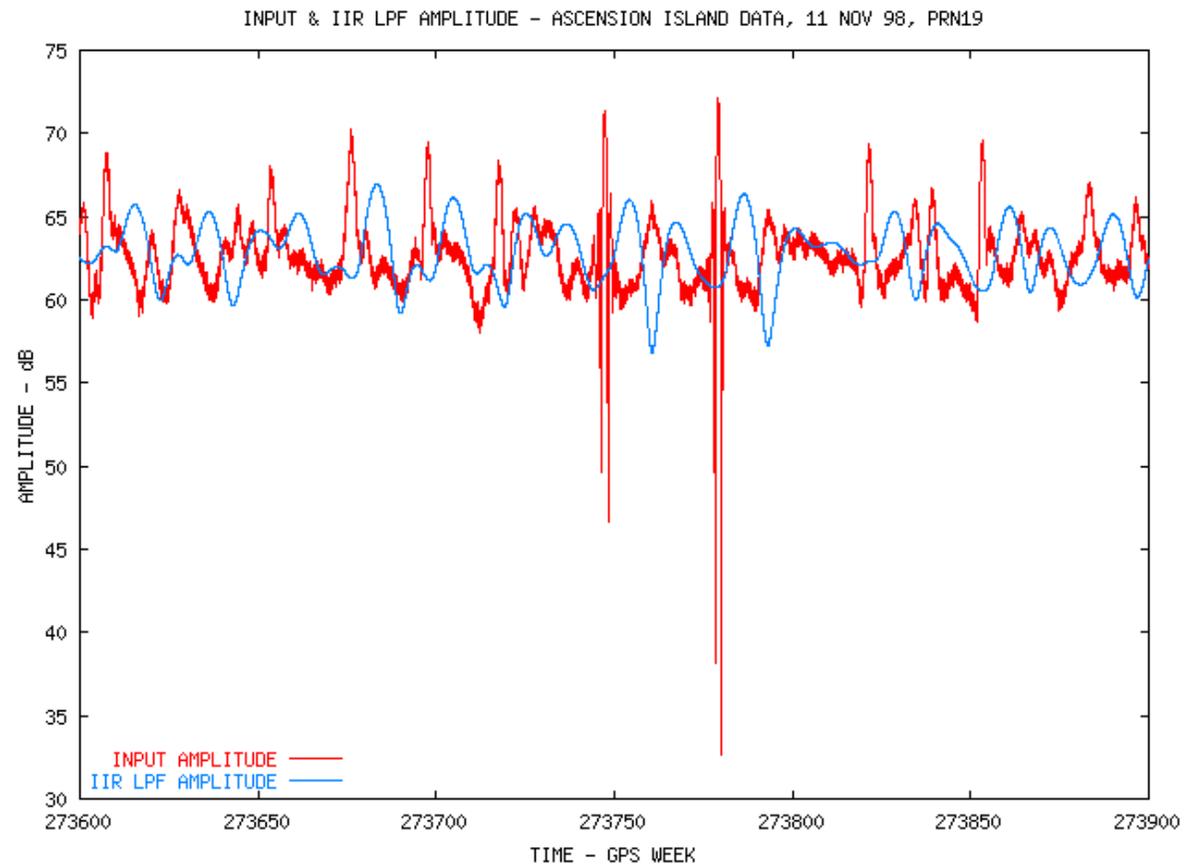
- ✚
$$S4_{Corrected} = \sqrt{\frac{\langle SI_k^2 \rangle - \langle SI_k \rangle^2}{\langle SI_k \rangle^2} - \frac{100}{\hat{S}/N_0} \left[1 + \frac{500}{19 \hat{S}/N_0} \right]}$$

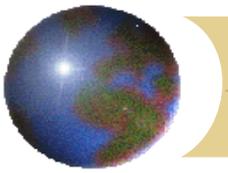
- ✚ If square-root argument is negative, set to 0 (means noise dominates any amplitude scintillation)
- ✚ This corrected value is computed off-line
- ✚ Option also exists to compute average value of SI_k as low-pass filtered value
 - ✚ This presents potentially unstable normalization because of filter delay – results in inflated $S4$ values



Low-Pass Filtering Introduces Delay in Normalization

- In low-passed version (denominator) does not line up with raw version, increasing the variance
- Possible to correct for the delay, but requires raw data buffering that is not desirable



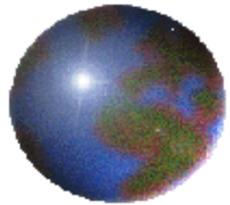


Measuring Amplitude Scintillation

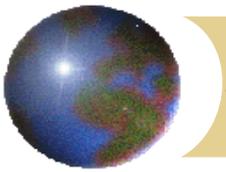
Summary

✦ Amplitude Scintillation

- ✦ Measure GNSS signal-plus-noise power
- ✦ Remove, as well as one can, noise power
- ✦ Relatively straight-forward
 - Some “detrending” issues separating scintillation fades from multipath fading – a detrending bandwidth issue
 - Detrending using averaging proves to be more stable than filtering, but results in higher S4 due to multipath fading

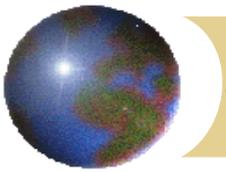


Measuring Phase Scintillation



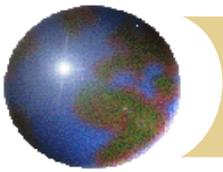
Some History Relative to Measuring Phase Scintillation Effects

- ❖ GPS Silicon Valley inherited commercialized scintillation monitoring technology from a US Air Force Small Business Innovation Research (SBIR) program
 - ❖ Toughest challenge on that program was measuring phase scintillation with standard GPS receivers using Temperature Compensated Crystal Oscillators (TCXOs)
 - TCXO phase noise masked phase scintillation effects
 - Problem solved using good Oven Controlled Oscillators (OCXOs)
- ❖ These upgraded receivers provide good phase scintillation measurements
 - ❖ Even then, there are limitations to operation in a scintillation environment

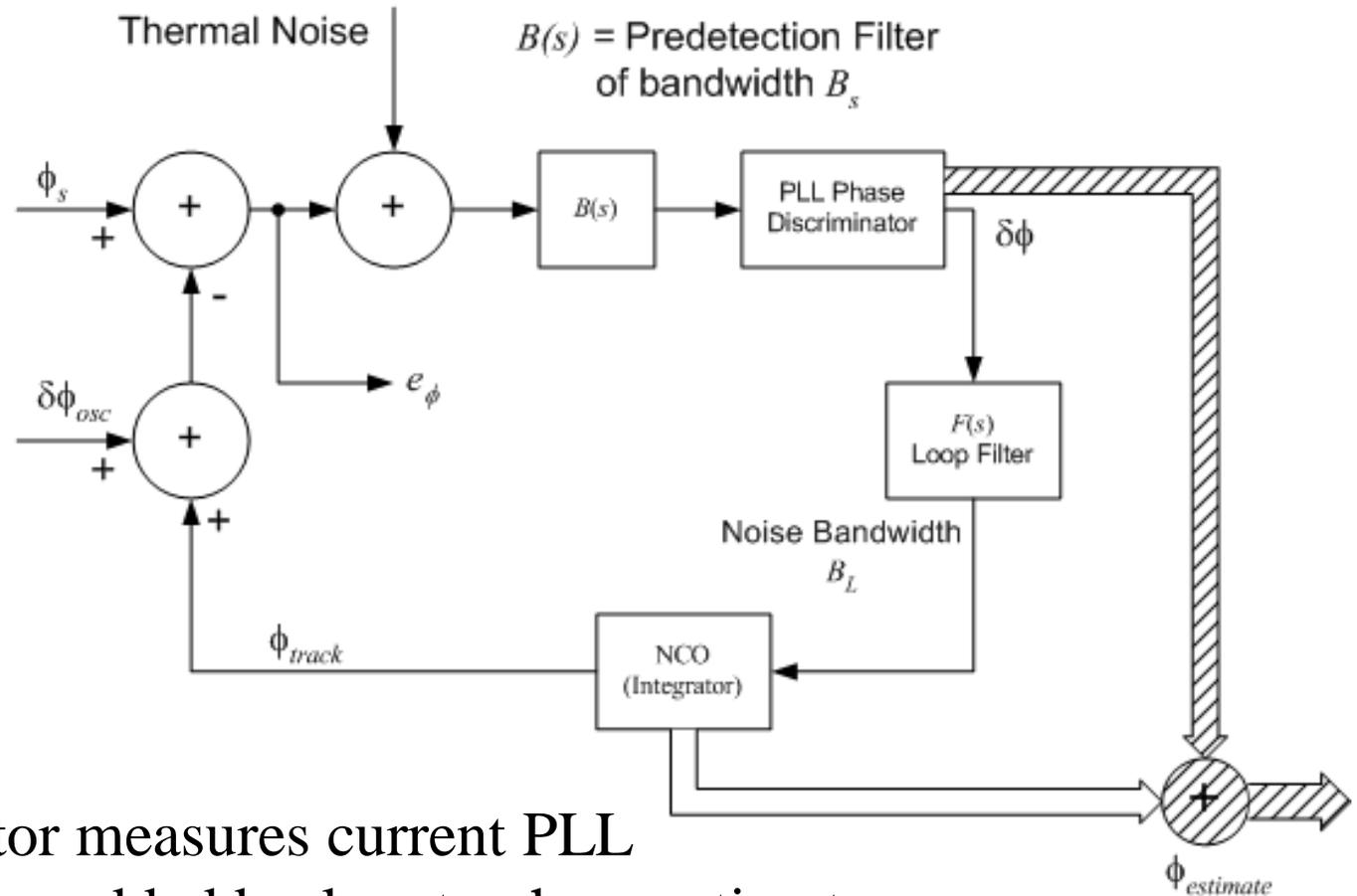


Measuring Phase Scintillation Effects

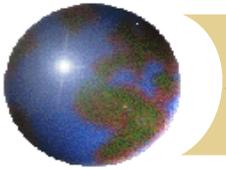
- ❖ To measure phase scintillation, GPS receiver must track signal phase using a phase lock loop (PLL)
 - ❖ Normally, weakest link in a GPS receiver
 - ❖ Measurements include perturbations of receiver and satellite oscillators
 - Mostly, these perturbations cannot be removed with “detrending”
 - ❖ Longer-term phase includes signal Doppler, multipath and ionosphere TEC (and oscillator frequency offset), mostly removed with “detrending”
- ❖ Typically, measurement bandwidth is the PLL loop bandwidth
 - ❖ Wide bandwidth makes loop more sensitive to amplitude fading, and thus, loss of lock
 - ❖ Narrow bandwidth makes loop more robust, but filters out higher-frequency phase scintillation effects
- ❖ Loop can be configured to have narrow loop bandwidth for robustness, but still provide wide bandwidth phase data



PLL Model with Wideband Phase Estimator

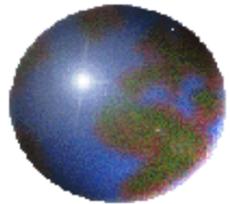


- Phase Discriminator measures current PLL 50-Hz phase error – added back onto phase estimate

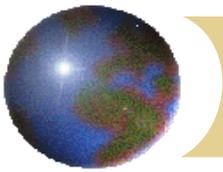


Legacy Measurements of TEC

- ⊕ Measure difference of GPS PN code phase on L1 and L2, smoothed against negative L1/L2 difference in carrier phase
 - ⊕ Legacy monitors use “semi-codeless” technique to measure on L2
 - ⊕ Does not enhance ability to measure scintillation
 - ⊕ Semi-codeless L2 has 15 to 35 dB less signal power recovery than L1
 - However, can use very low bandwidth PLL, aided with L1 Doppler phase, regaining 14 to 17 dB, depending upon C/N_0
- ⊕ Limitations
 - ⊕ Typically not available if L1 C/N_0 drops below 38 dB-Hz
 - ⊕ Must contend with L1/L2 biases
 - Satellite biases (Tau_GD and C/A-to-P) and receiver and antenna L1/L2 biases
- ⊕ Real-time accuracies on the order of 1 – 2 TECU, after calibration
 - ⊕ Also, very much affected by multipath



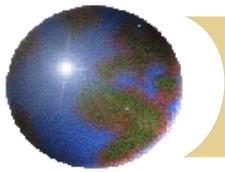
Evolution to Modernized GNSS



Legacy GSV 4004B & Antenna

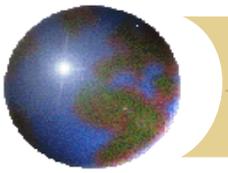


GSV4004B GPS IONOSPHERIC SCINTILLATION AND TEC MONITOR AND OPTIONAL GPS702GG ANTENNA

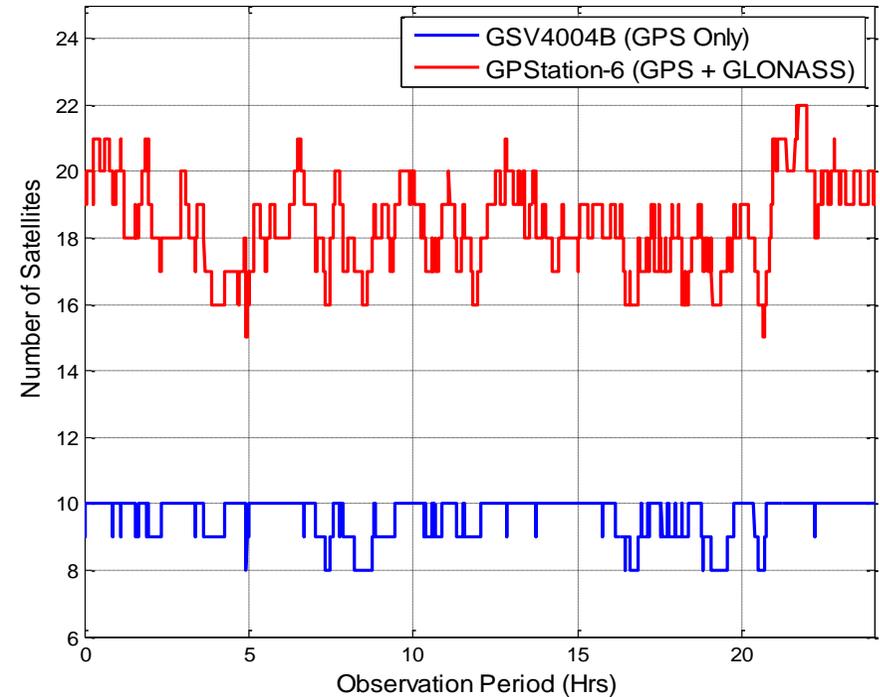
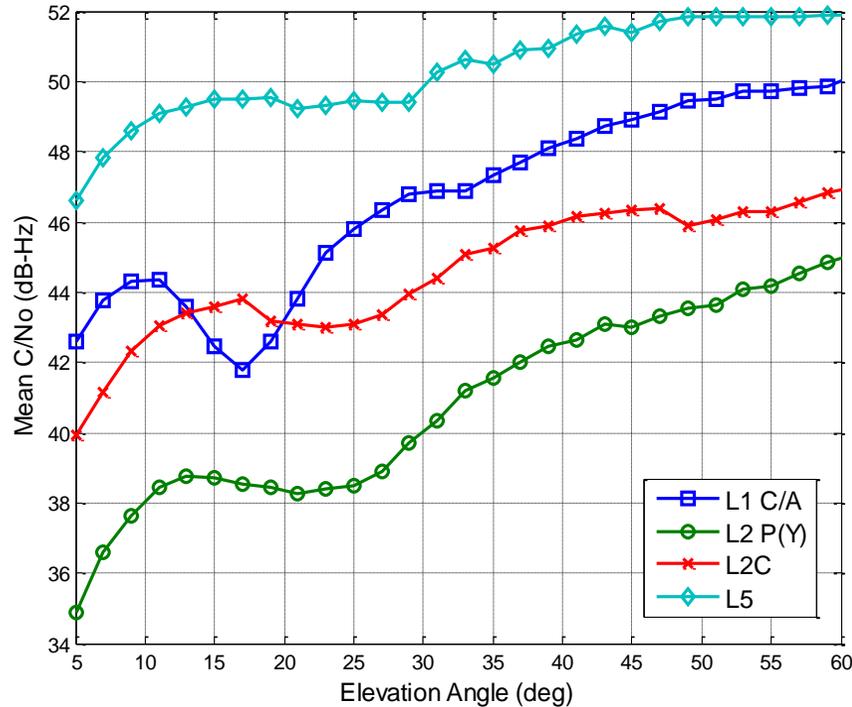


Features of GPStation-6 GISTM

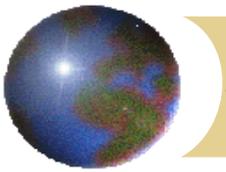
Features	GISTM Receiver (Bold Red Indicates New Features)
Channel Configuration	120 independent channels
Signal Tracking	GPS (L1, semi-codeless L2P, L2C, L5) GLONASS (L1, L2-C/A, L2P) Galileo (E1, E5A/B, E5 AltboC) SBAS (L1, L5), Compass (Upgradable)
Ionospheric Measurements	50 Hz phase and amplitude data (raw or detrended-raw)
Scintillation Indices	GPS (L1 C/A, L2C, L5), GLONASS (L1, L2) Galileo (E1, E5) , SBAS (L1, L5)
TEC (Code and Carrier)	GPS (L1/L2P, L1/L2C, L1/L5), GLONASS (L1/L2) Galileo (E1/E5A) , SBAS (L1/L5) (1 Hz raw and 4/minute smoothed)
Communication Interface	USB /RS-232/RS-422 , I/O (PPS, Event, Position Valid)



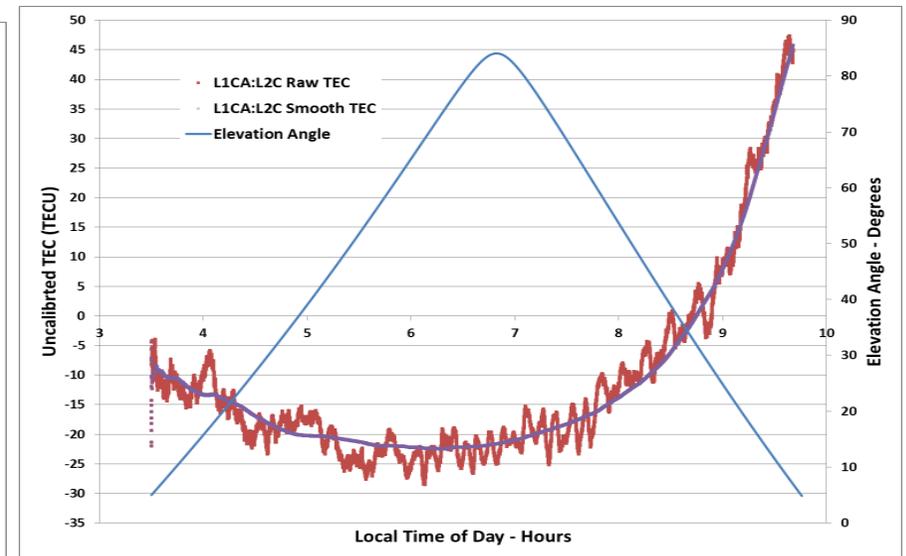
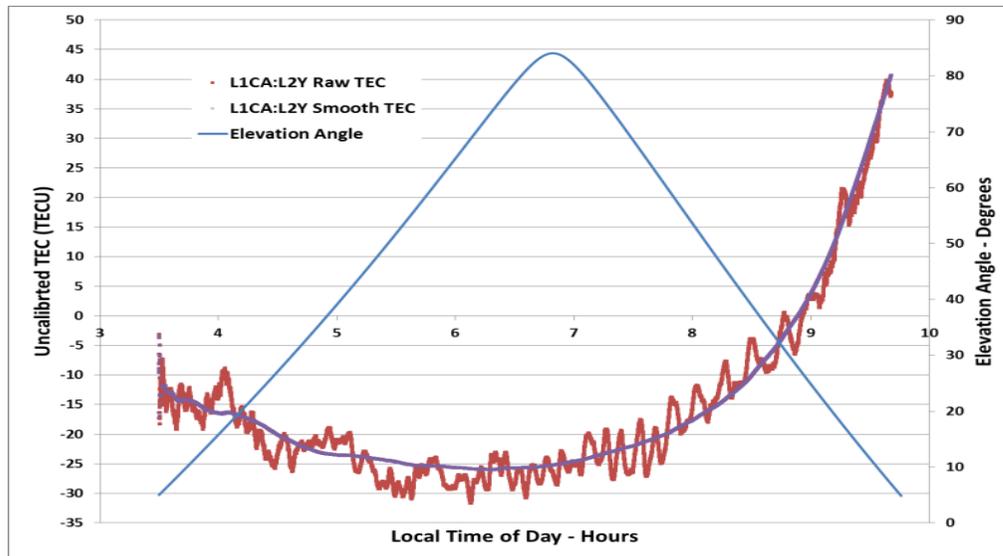
Improvements by Adding L2C and L5



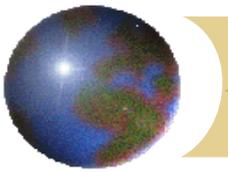
- Measured at Calgary, AB, Canada
- GPS Modernization improves Signal Quality – C/N₀
- Adding Constellations increases Number of Ionospheric Pierce Points



Comparison of L1C/A - L2C and L1C/A - L2P(Y) for Measuring TEC

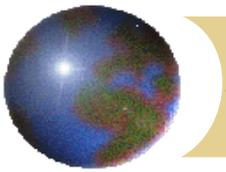


- Negative TEC because receiver is not delay calibrated

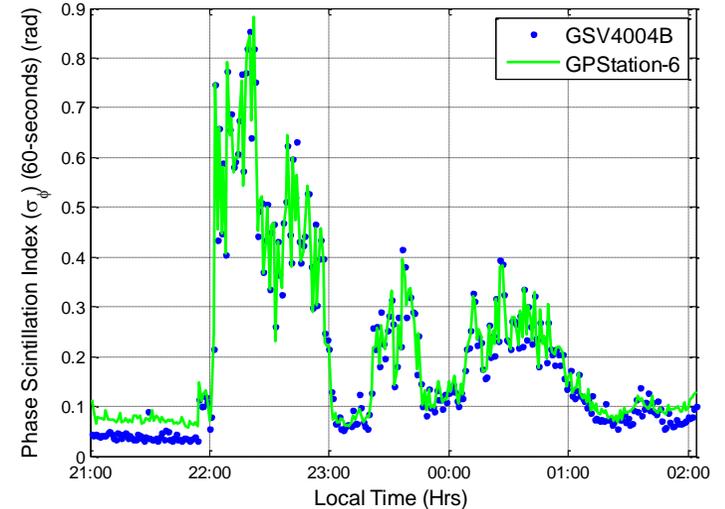
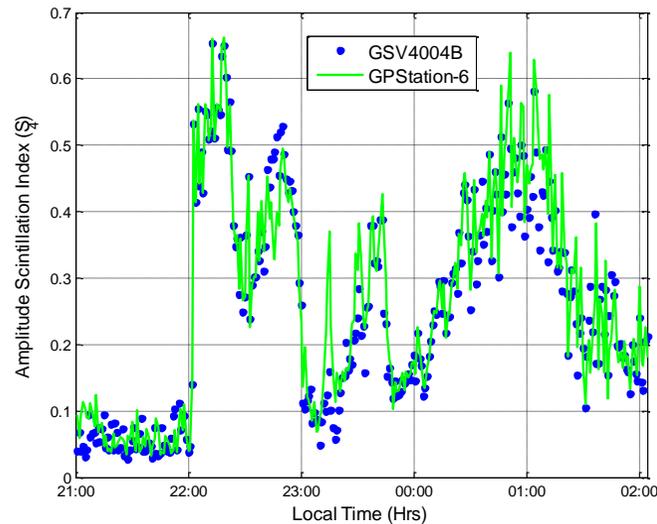


L2P(Y)/L2C TEC Performance Differences

- ⊕ Not much difference in displayed performance
 - ⊞ 3 dB loss in L2C I/Q multiplexing
 - ⊞ Wider tracking loop bandwidth on L2C
 - ⊞ Multipath errors dominate – lower chipping rate on L2C
- ⊕ However, L2C tracking much more robust and less dependent on L1 aiding
- ⊕ Larger TEC bias using L2P(Y)
 - ⊞ More filter delay of wideband signal



GPS Scintillation Measurement Comparisons

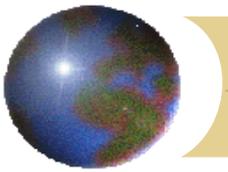


- Calama, Chile

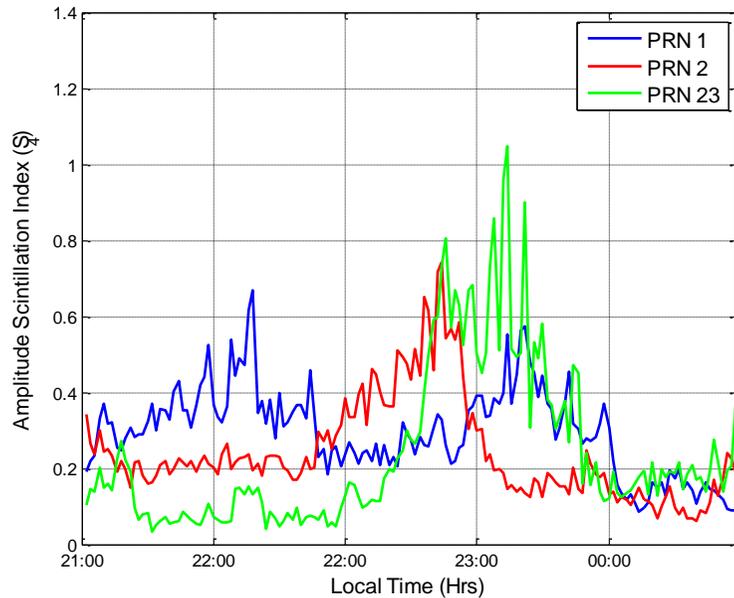
- S4 – Legacy vs Modernized

- σ_ϕ – Legacy vs Modernized

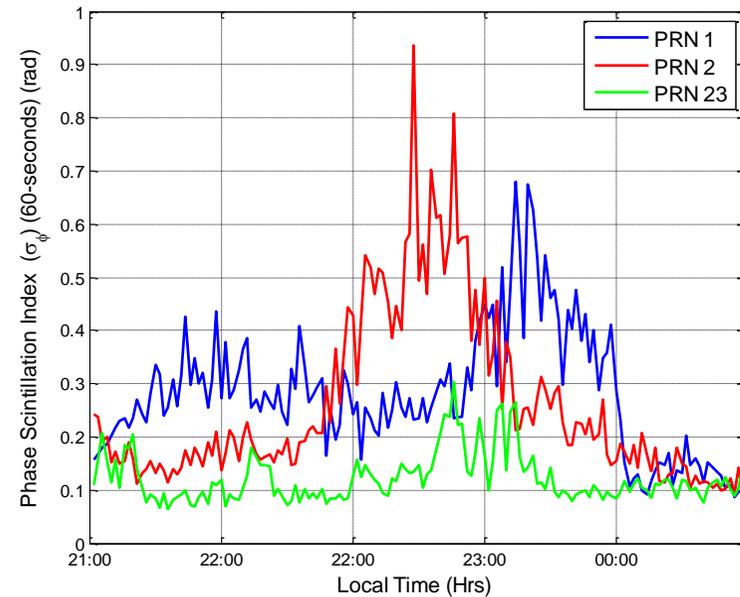
- Comparison shows excellent backward compatibility



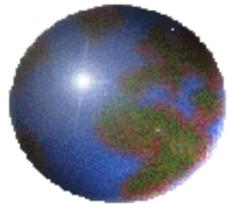
Modernized Monitor Includes GLONASS



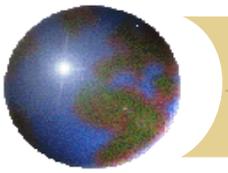
• S_4



• σ_ϕ

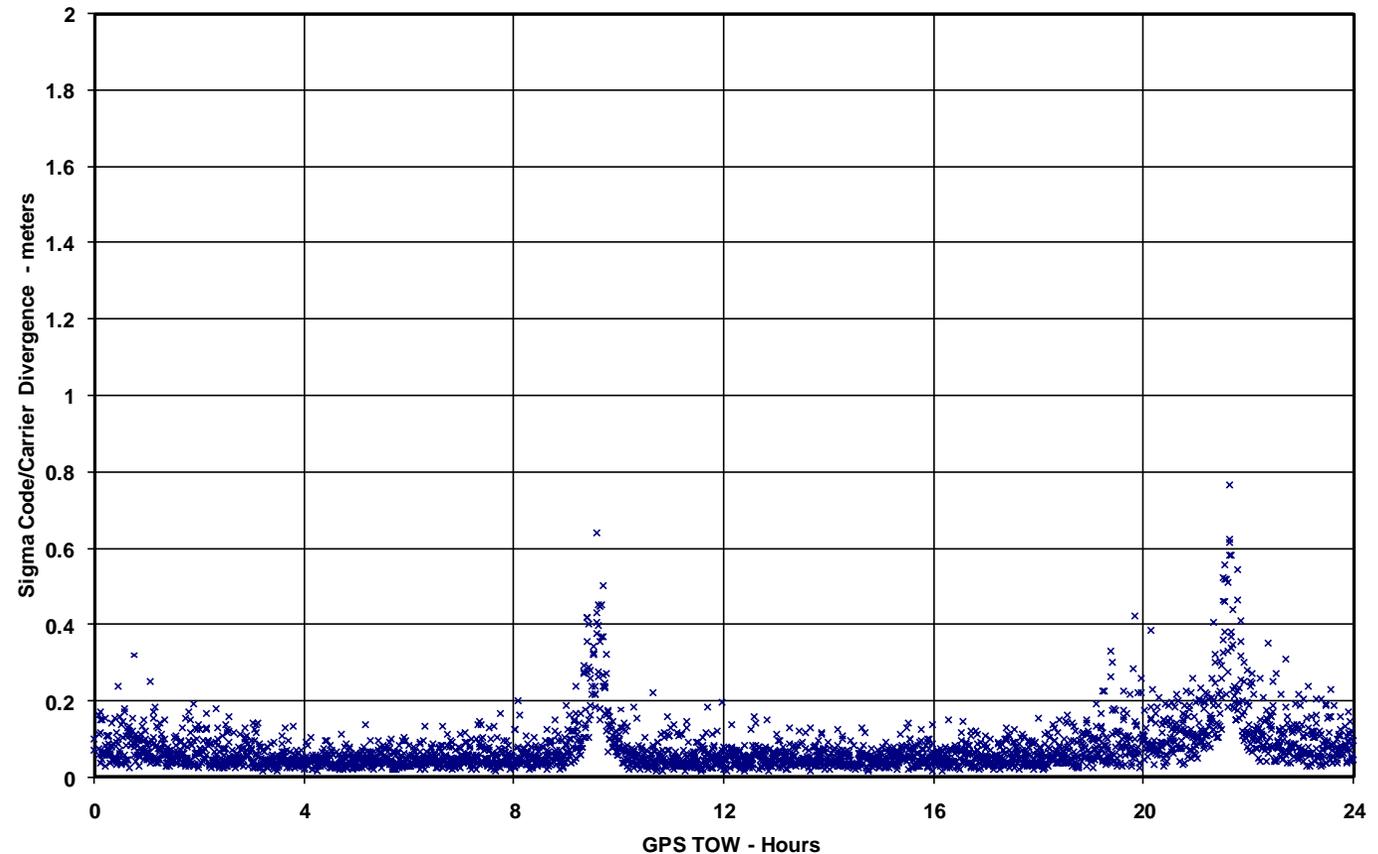


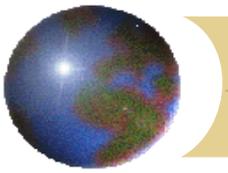
SBAS GEO Measurements



Legacy SBAS S4 Measurements in Non-Scintillating Environment

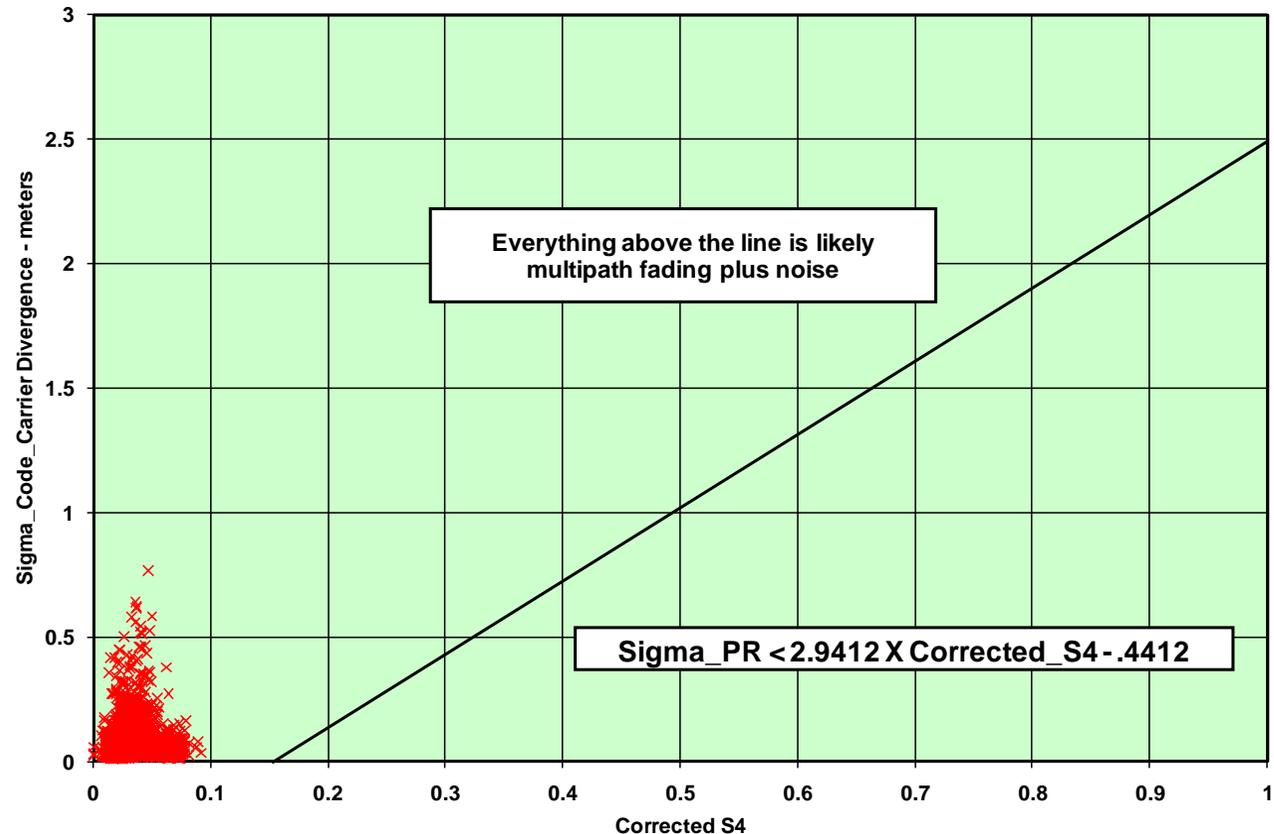
- Standing wave multipath detrends out very well
- Code/carrier divergence due to crossing Doppler of 2 GEOs

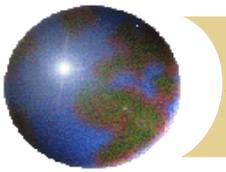




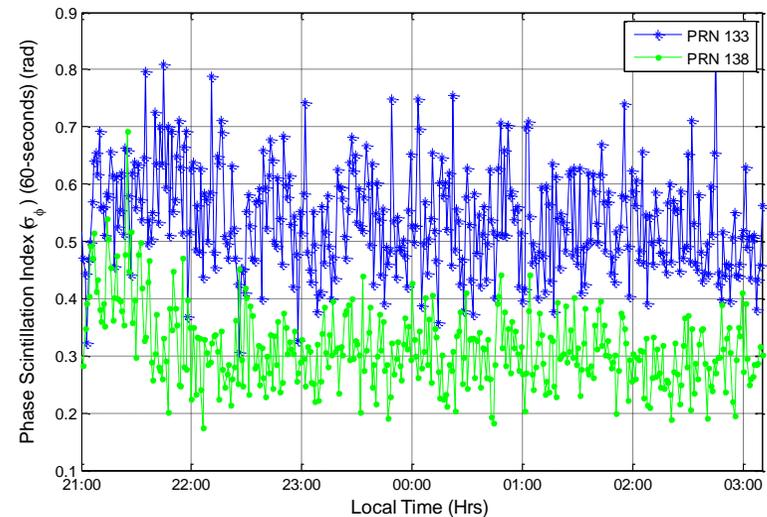
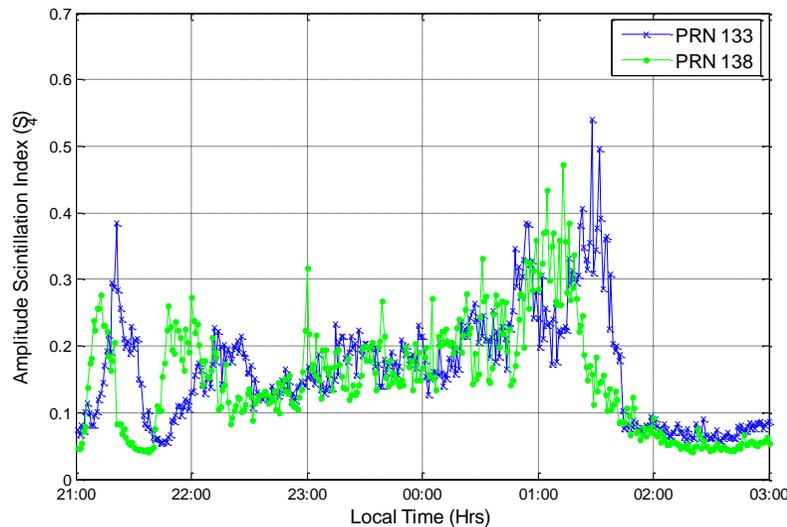
Easy to Distinguish between Multipath and Amplitude Scintillation from GEOs

- No scintillation
- Slow varying standing wave multipath



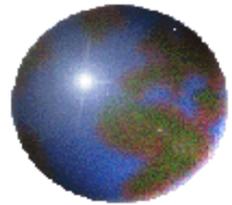


Modernized SBAS Measurements – Same Performance as Legacy Receiver

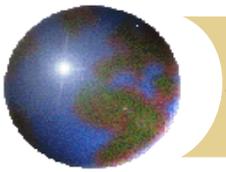


- S4
- Time difference is due to pierce point location difference

- σ_{ϕ}
- Noise is due to GEO payload transponder phase noise
- Some phase scintillation observable between 9 and 10 pm



*Scintillation Monitoring
Limitations That Apply to Both
Legacy and Modernized
Monitors*



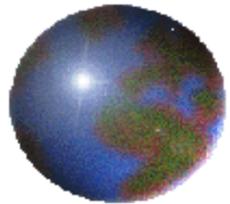
General GNSS Receiver Limitations in Scintillation Environment

⊕ Phase Scintillation

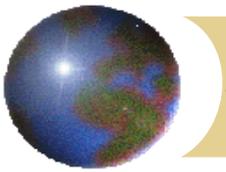
- ⊞ Generally, not a problem at L1 or L5, or on L2C
 - Unless a very narrow tracking bandwidth is used
 - No worse than low-grade TCXO typically found in GPS Receivers
 - Requires relative wide bandwidth PLL for phase tracking
- ⊞ Larger problem for “semi-codeless P(Y)” on L2
 - Very narrow bandwidth PLL coupled with erroneous (required) aiding with L1 phase (doesn't agree with Doppler aiding)

⊕ Amplitude Scintillation

- ⊞ Primary culprit for loss of phase lock
 - Deep and long fades steal signal from PLL
 - Narrower bandwidth is better, but could require a better oscillator, and may lose lock due to strong phase scintillation
 - False alarms from lock detectors during fades (apparent loss of lock)
- ⊞ Loss of data (symbols) from SBAS signals

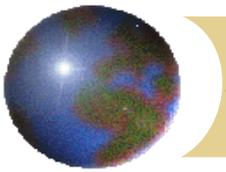


Phase Scintillation Limitations

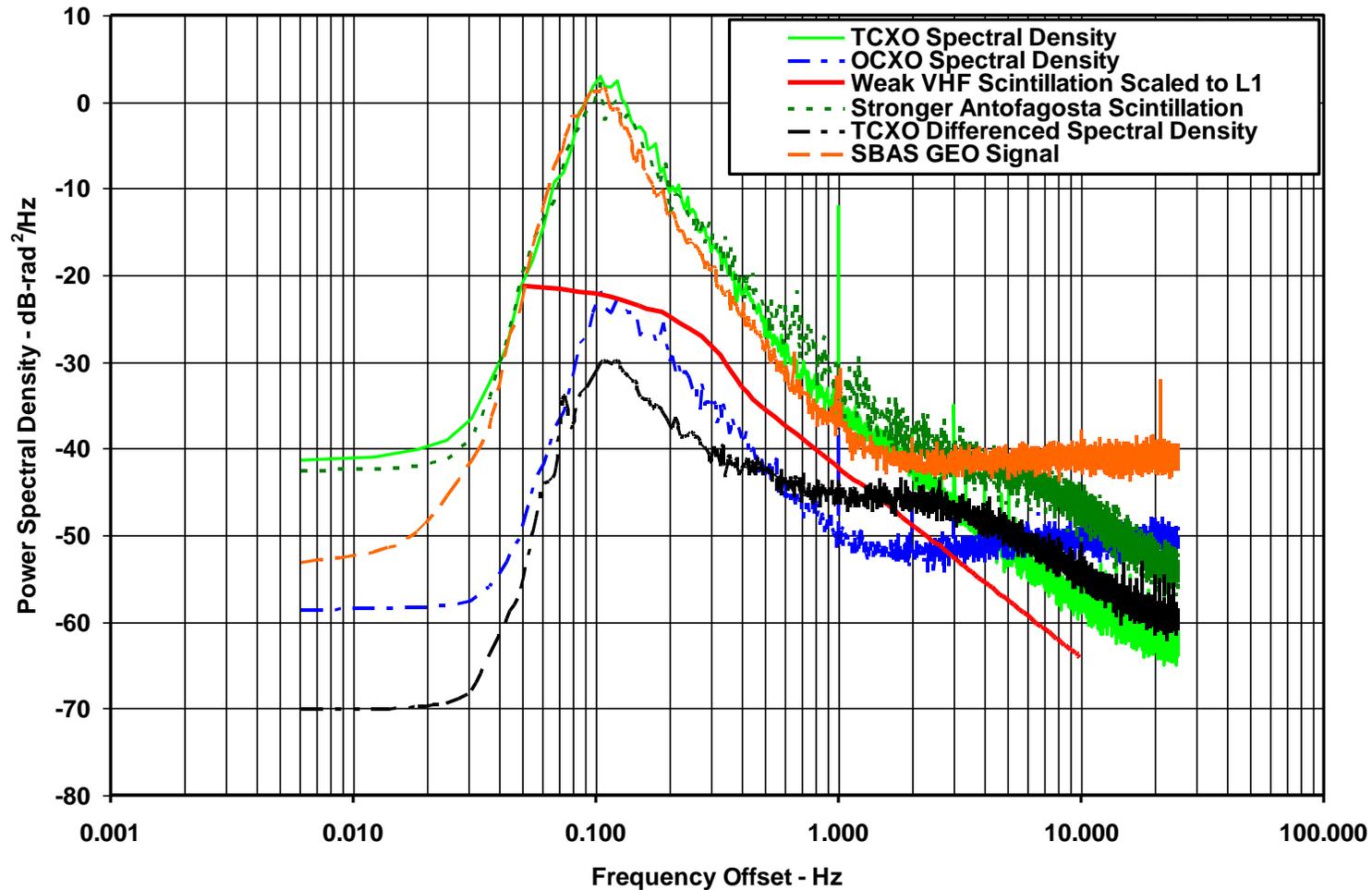


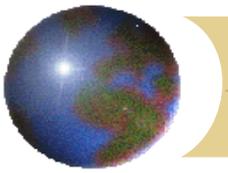
GNSS Scintillation Monitor Limitations in Phase Scintillation Environment

- ❖ Can't measure scintillation at "semi-codeless" L2 P(Y) – Loop bandwidths too narrow
- ❖ Measurement limitations on coded signals (L1, L2C and L5) dominated by receiver oscillator
 - ❖ Typical receiver oscillator phase noise masks phase scintillation (See PSDs and plots in next charts)
 - ❖ Thermal Noise limitation is about 0.1 radian @ 30 dB-Hz
 - ❖ OCXO phase noise typically better than 0.05 radians
- ❖ Limitation can be overcome by differencing phase between satellites
 - ❖ Creates a requirement for high-rate data collection and substantial post processing

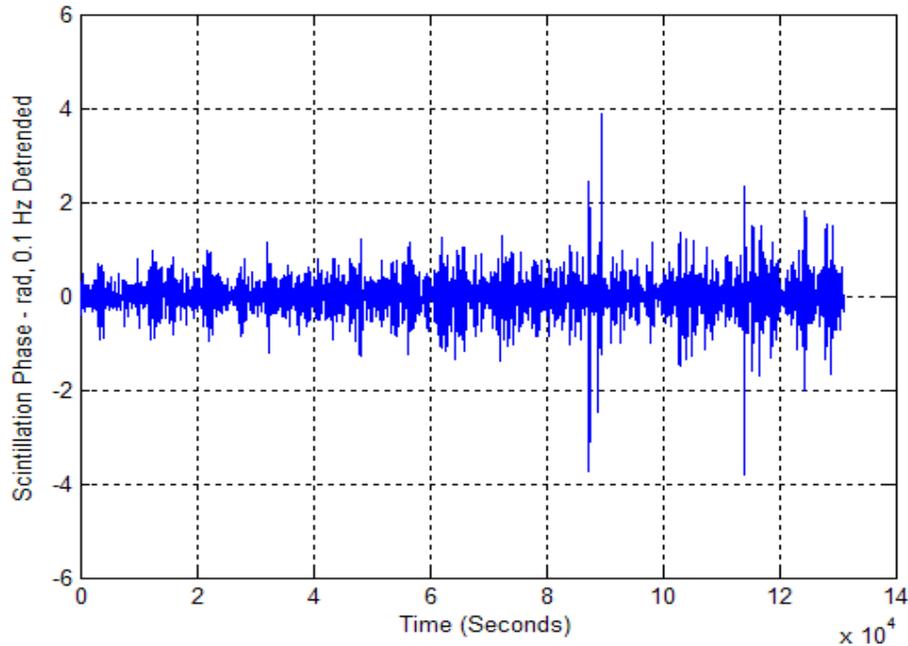


Phase Noise PSD Comparisons

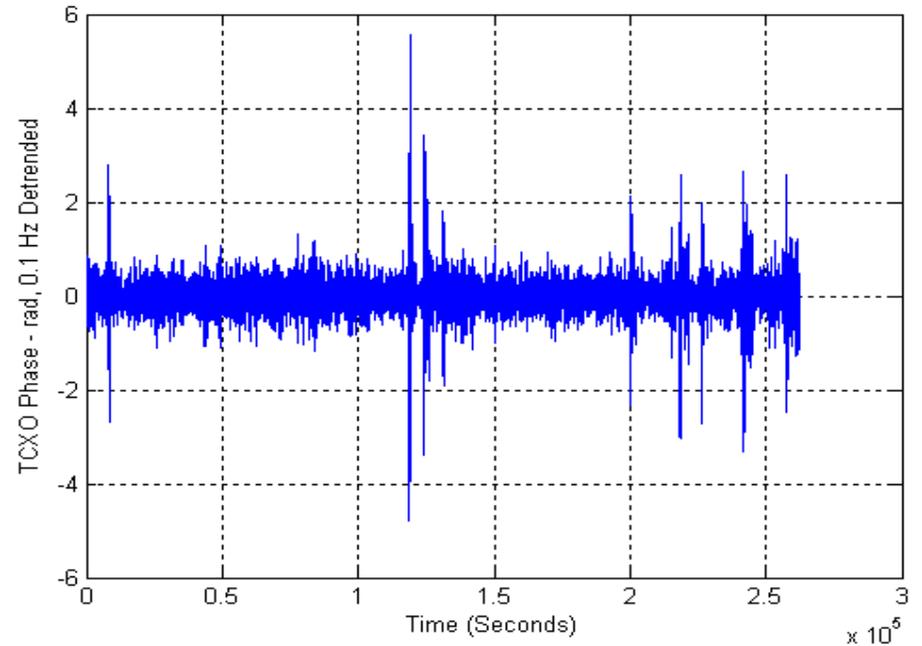




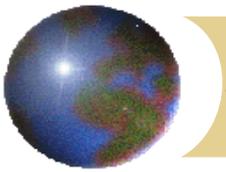
Antofagosto Phase Scintillation vs. TCXO Phase Noise



$$\sigma_{\phi} = 0.396 \text{ radians}$$

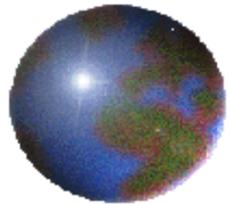


$$\sigma_{\phi} = 0.46 \text{ radians}$$

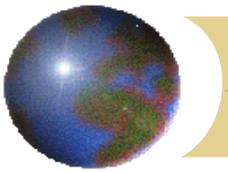


Tradeoffs Regarding Using Low-Noise Oscillators (OCXOs)

- ✦ Cost of low-noise OCXOs has diminished somewhat over recent years
 - ✦ The cost driver is their packaging with the receiver (low-volume quantities)
 - This packaging must also meeting international radiation and conductive emission (CE) requirements
- ✦ As stated, TCXO noise can be eliminated by differencing phase across satellites
 - ✦ Creates a data storage and post-processing burden
 - ✦ Receiver tracking bandwidth must be kept high, preventing tracking in noisy conditions and during deep fades



Amplitude Scintillation Limitations



Scintillation Monitor Limitations in Amplitude Scintillation Environment

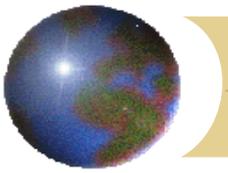
✦ Amplitude Scintillation

✦ High S4 can cause loss of phase lock

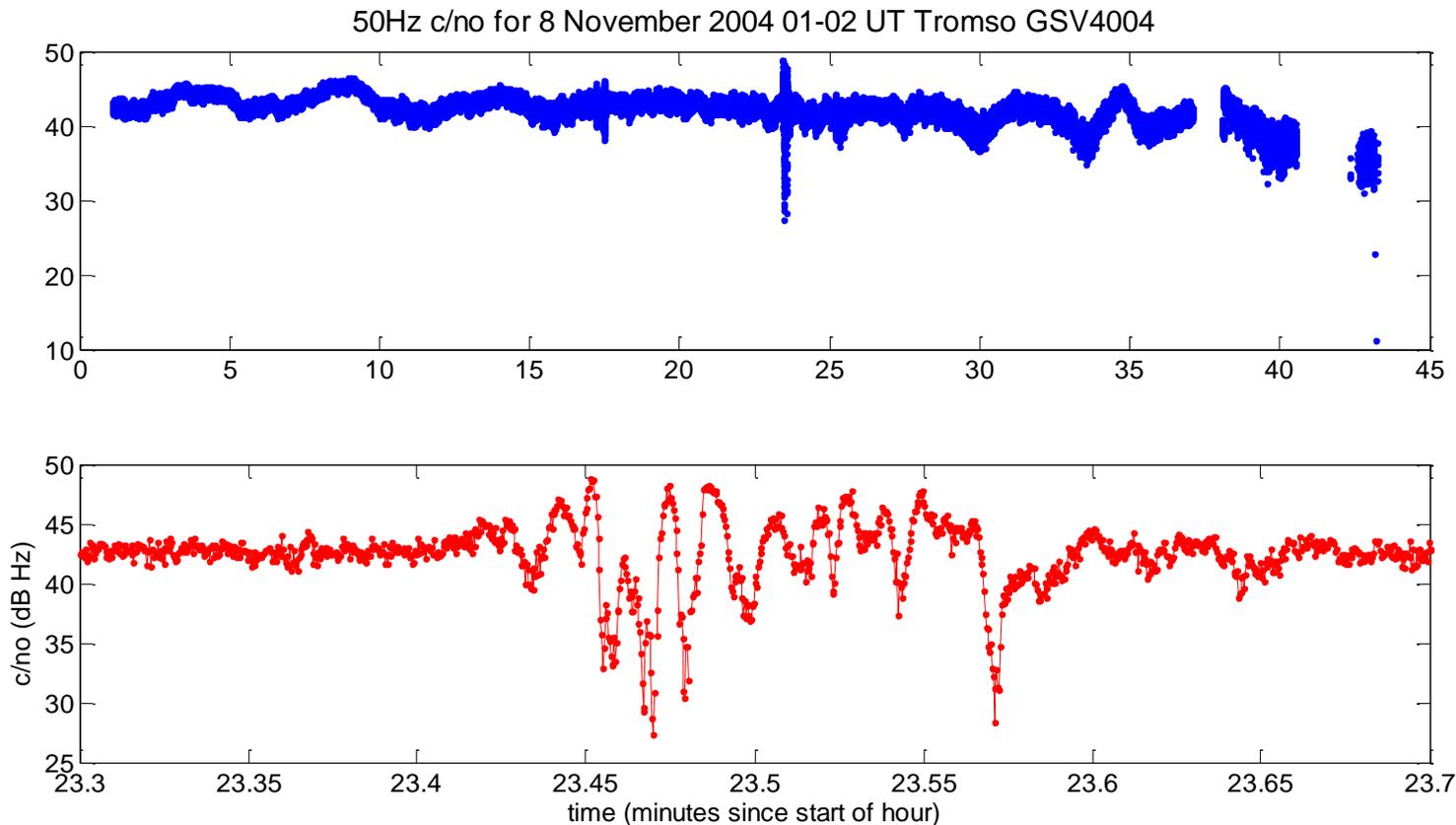
- S4 is still usually valid – it is based upon non-coherent power measurements, at least for short to medium length fades
- See state diagram

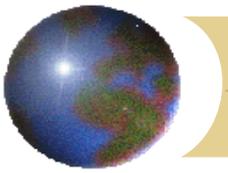
✦ Multipath fading limits minimum S4 capability

- Longer duration, but shallow fades
- Can be detected and eliminated because multipath also causes code/carrier phase divergence – scintillation does not



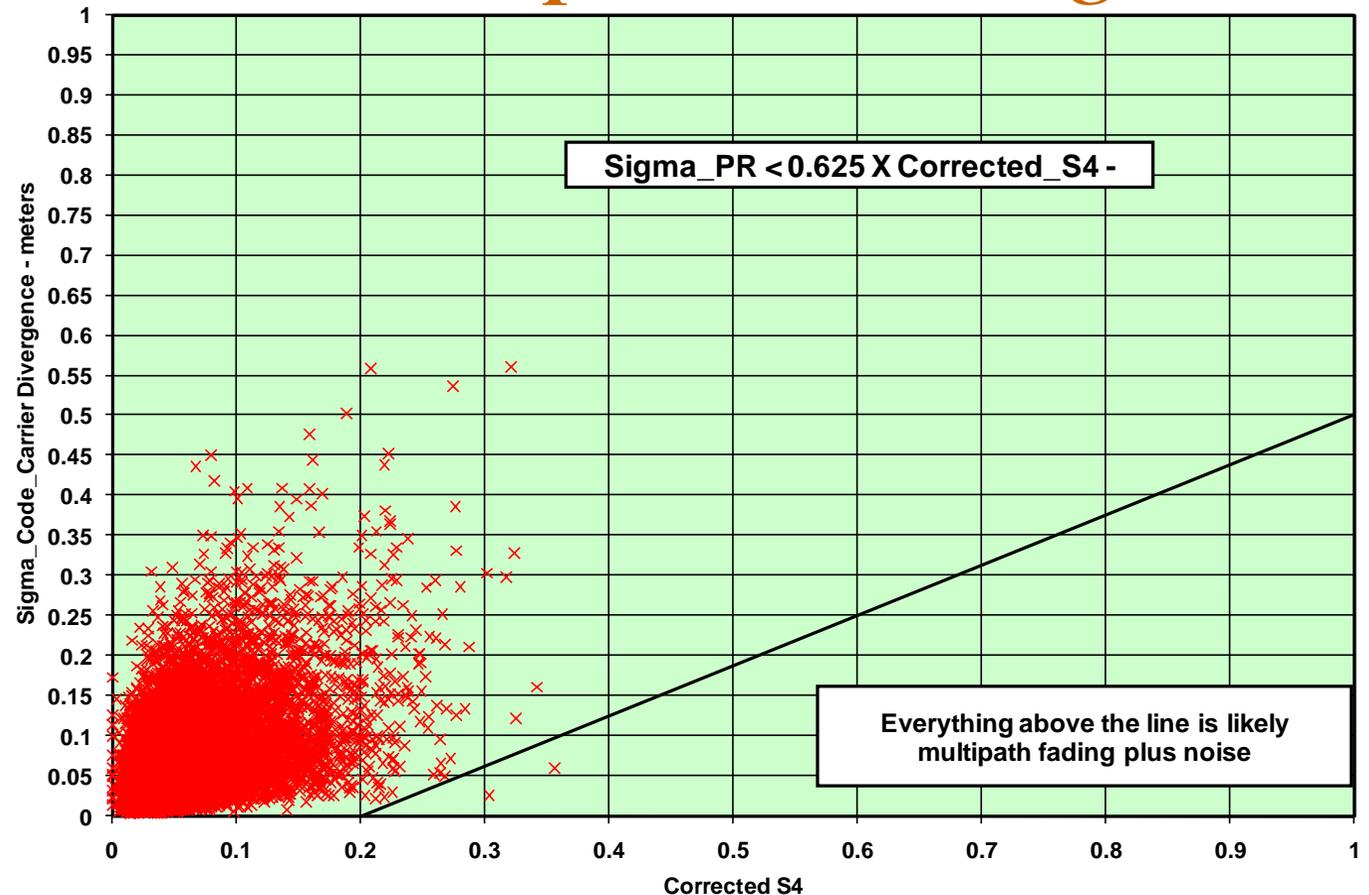
Fade Depths and Widths Using 50 Hz Amplitude Samples

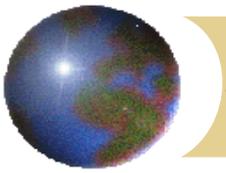




Distinguishing Between Amplitude Scintillation and Multipath Fading

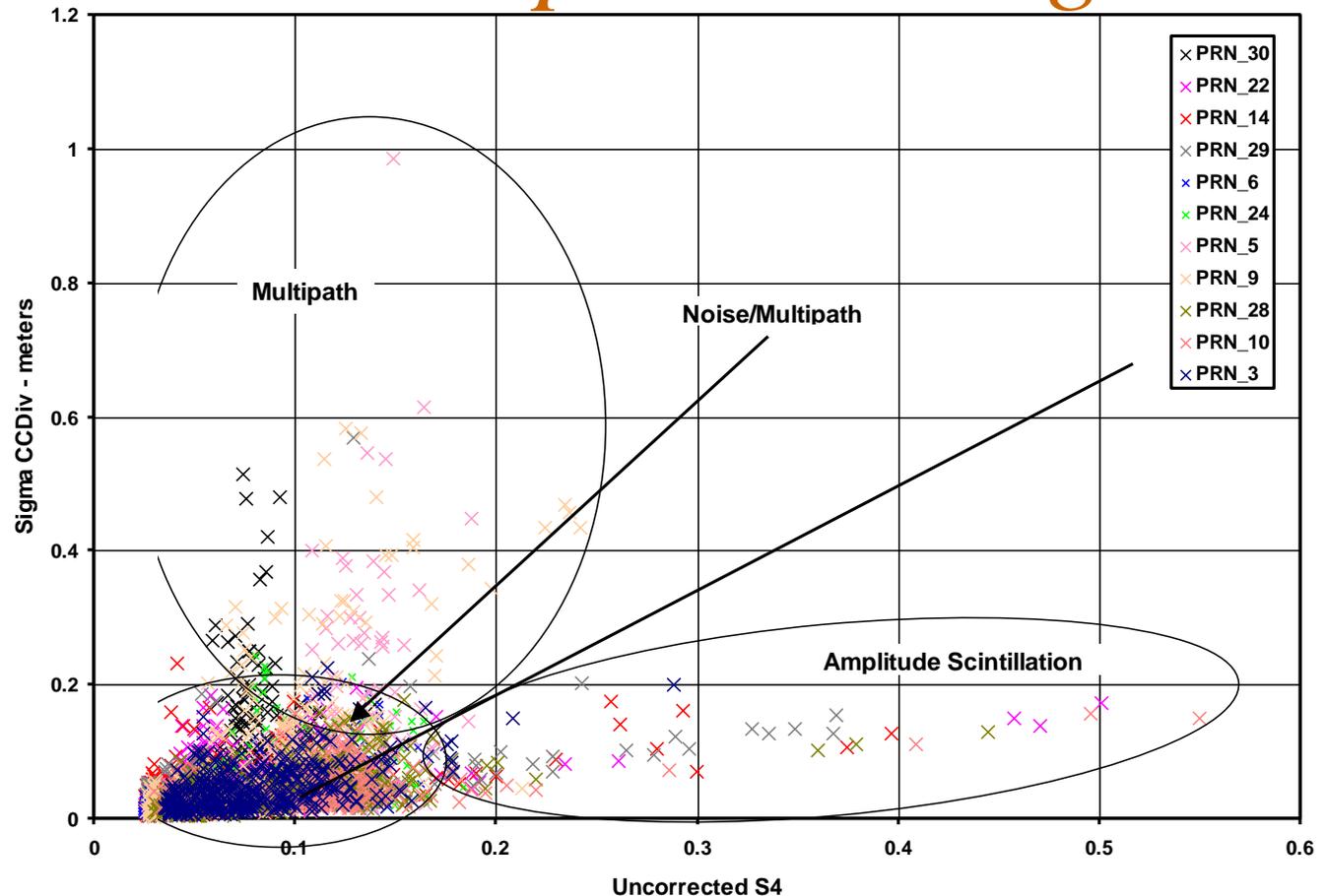
- No Scintillation
- Varying Multipath
- All GPS Satellites

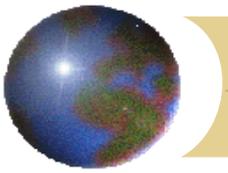




Distinguishing Between Amplitude Scintillation and Multipath Fading

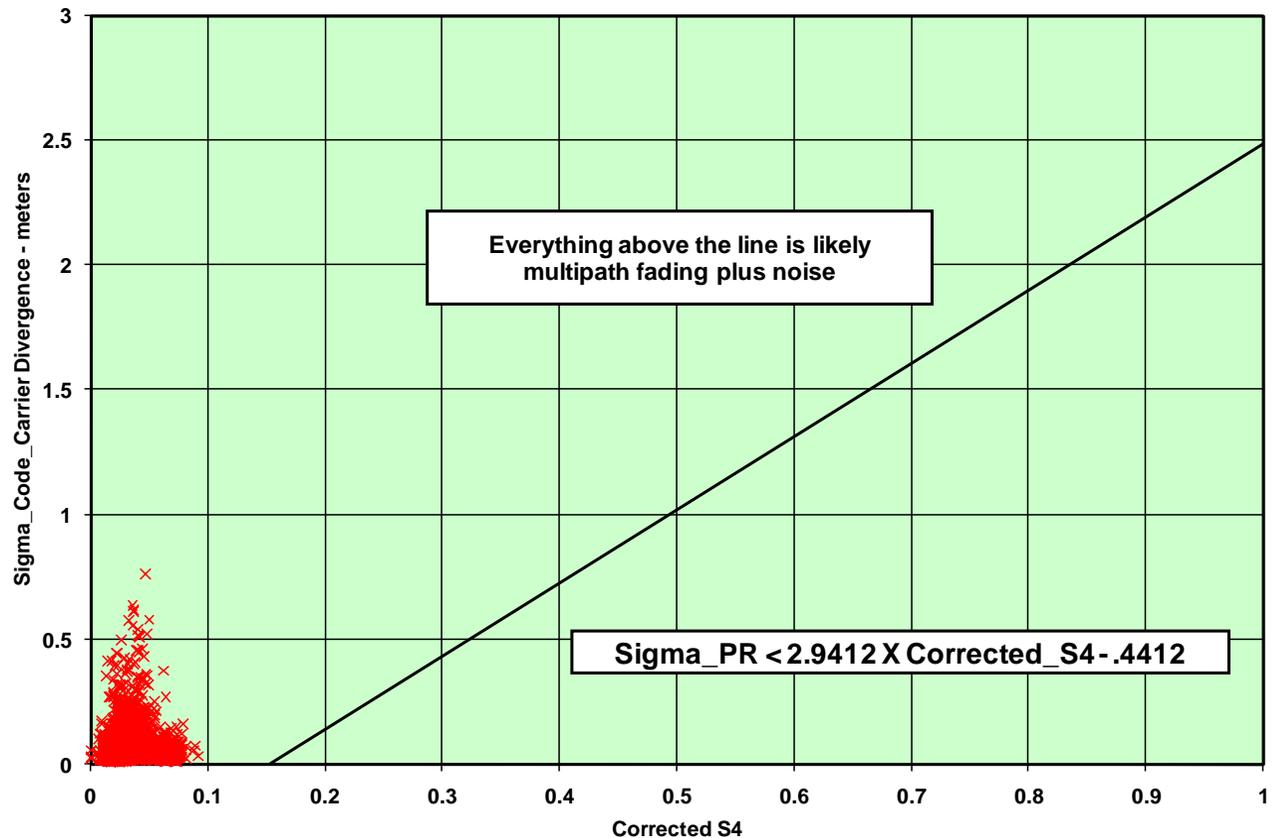
- Moderate Scintillation
- Varying Multipath
- All GPS Satellites

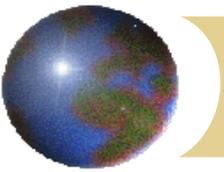




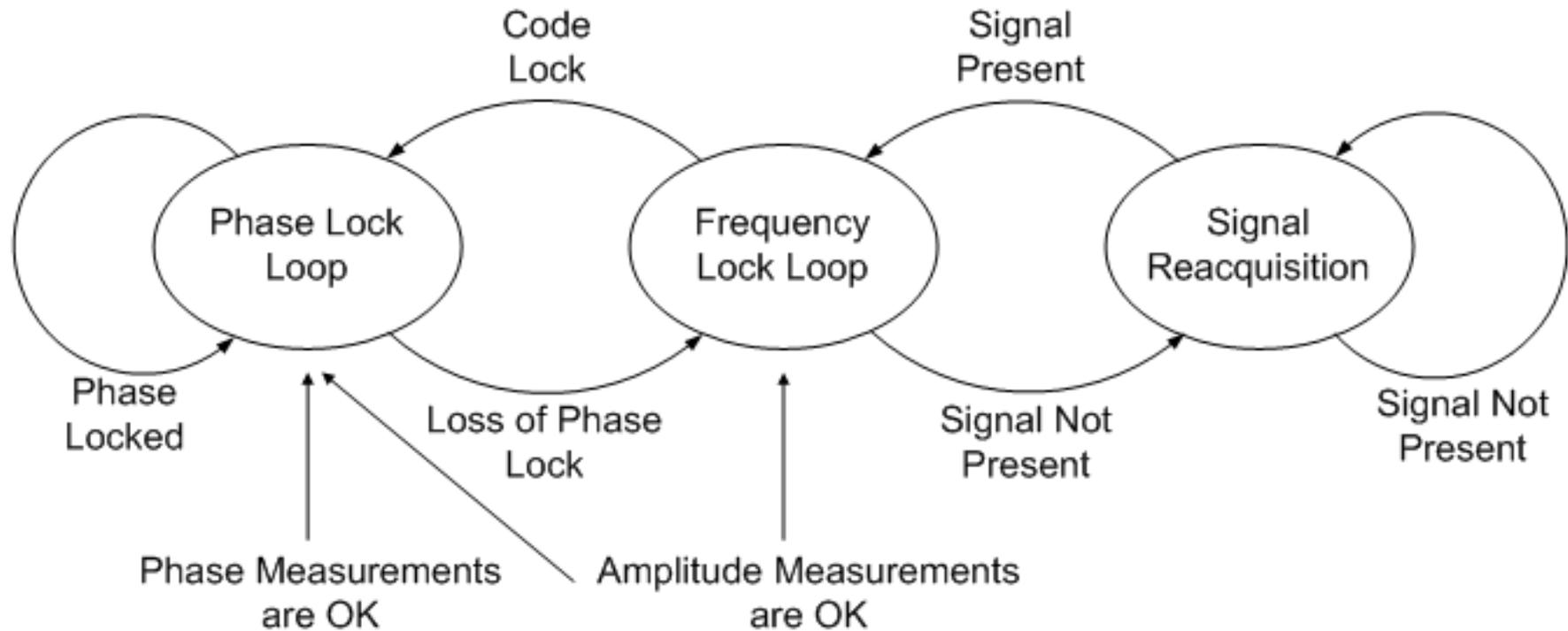
Multipath Fading Tracking SBAS Signals

No Scintillation,
Slow Varying Multipath
2 SBAS Geostationary
Satellites

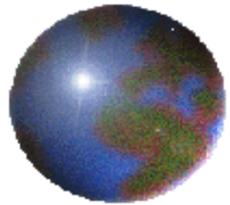




Signal Tracking State Diagram

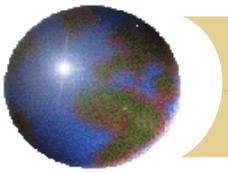


- Not necessarily implemented in all receivers, but is in Scintillation Monitors described here

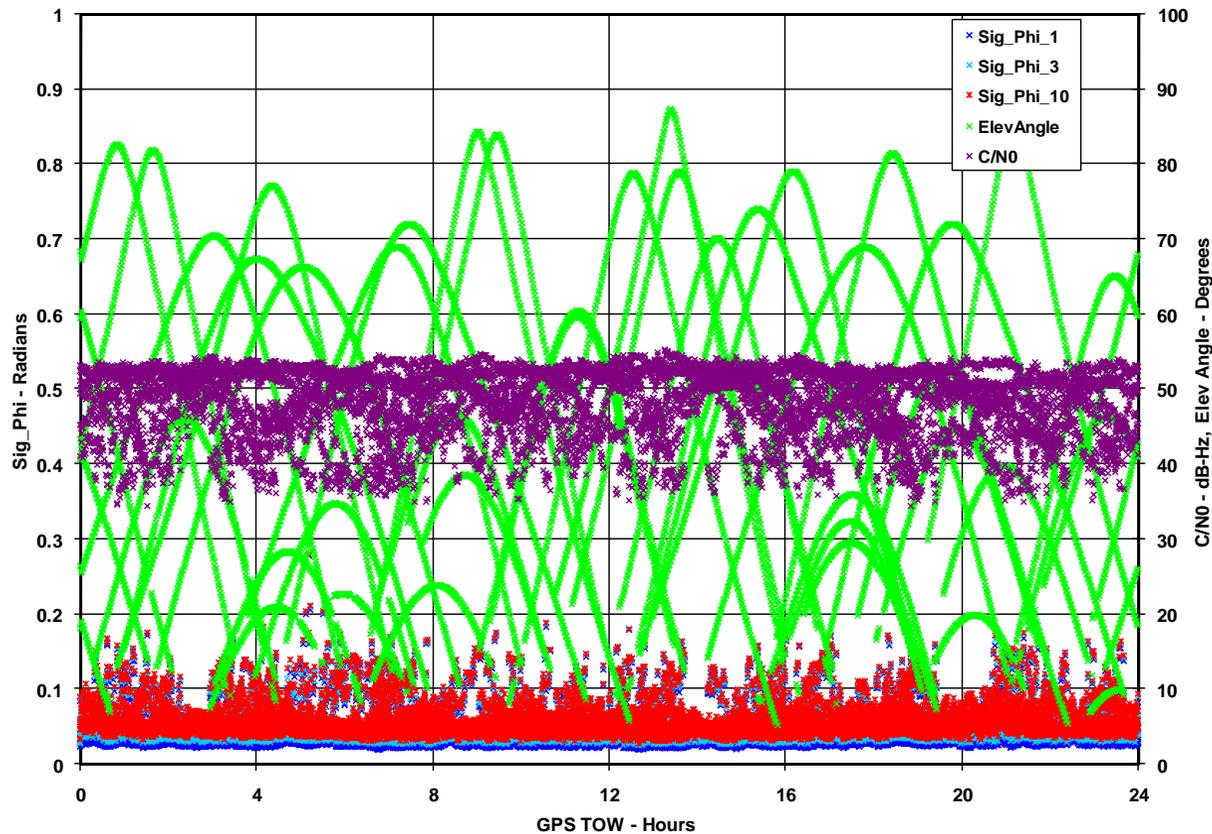


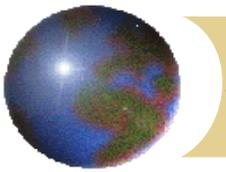
Example Phase Measurements Collected in San Francisco Area

Non-Scintillation Environment



Typical Plot of 1, 3 and 10 Second Sigma-Phi from All Satellites in View





SBAS GEO Phase Measurements

- Phase Degraded by GEO Transponder Code/Carrier Control
- However, constant 45 degree elevation — no multipath effects

