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Nuclear technology applications of ceramics, composites and other nonmetallic materials

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Nonmetallic materials are being used or considered for a wide range of fission and fusion energy applications

- Microencapsulated fuel systems for gas-cooled and accident-tolerant water cooled reactor designs
- SiC/SiC and CFC composites for structural applications
- Neutron control systems for fission reactors
- Diagnostic applications (optical fibers, windows, bulk insulators, MI cables)
- Plasma heating systems
- Fusion ceramic breeders
- Fission waste storage forms

• This presentation will focus on the first two topics in this list



Materials performance is key for economic and safe fission reactor operation in current LWRs

- Heat generation in UO₂-based fuel pellets
- Heat transfer across Zr alloy cladding
- Numerous core internal structures to securely position core
- Reactor pressure vessel for containment of fission products
- Piping and steam generator equipment for heat conversion to electricity









Evolution of coated particle fuel missions

Generality	1960s	>1980s	2000s
	 Ceramic coated particle fuel developed for extreme performance in nuclear rockets (ROVER/NERVA) TRISO used for large graphite reactors (HTRs) 	 TRISO fuel adapted for high temperature operation in modular HTR 	 Evidence of exceptional burnup of ceramic TRISO fuel suggests potential use in management/ utilization/ destruction of TRU used fuel
	Deep Burn ut the high bur capabilitie of TRISO for Deep Dive_1006	ilizes nup es uel	DOE Deep Burn Project



Micro-encapsulated fuels for high-burnup applications



Targeted Modeling Activities:

- Kernel Stability Through Gettering
- Ag and Pd Diffusion in SiC & ZrC
- Thermal Transport
- Irradiation Effects on PyC & ZrC

TRISO Kernel Activities:

- Fabrication of uniquely small kernels
- Inclusion of getter and BP within kernel

TRISO Coating Activities:

- ZrC Coating Development
- ZrC Properties and Irradiation Eff.



Recent irradiation tests have demonstrated high reliability of micro-encapculated fuels

- Fuel recently developed at ORNL and irradiated in ATR at INL under AGR program sponsorship
- Global performance record for particle fuel: ~19% of LEU consumed, zero fuel failures
 - More than 2× the previous record
 - More than 3× current LWR fuel
 - Not a single TRISO fuel particle failure since beginning of irradiation ~ 3 year ago
- Significant step for TRISO nuclear fuel particles for use in HTGRs

Fluence achieved at 19% burnup with fertile fuel is similar to that expected for Deep Burn TRU TRISO fuel at > 60% burnup





The LOCA at Fukushima Dai-ichi has heightened interest in re-evaluating potential accident-tolerant fuel systems

- Several potential options exist for fuel cladding
 - Oxidation-resistant austenitic steels
 - Relatively high neutron absorption and low melting temperature are concerns
 - Oxidation-resistant coatings on Zr alloy cladding
 - Mechanical robustness of cladding on anisotropic Zr alloy tubing is a concern
 - Ceramic matrix composite cladding
 - Relatively thick cladding requirement, hermetic isolation of fission products, joining techniques and lack of structural design criteria codes (e.g., ASME) are concerns







Overview of desired cladding attributes

- Very low parasitic neutron absorption
 - (dependent on spectrum; Zr is very good for LWRs)
- Good mechanical strength
 - Normal and transient high temperature conditions
- Good compatibility with coolant and fuel (including fission products)
 - varying water/steam chemistry for light water reactors
 - Normal and transient/accident conditions
- Low oxidation rate (hydrogen production) in water/steam and low oxide heat of formation
- Good thermal conductivity
- Good radiation resistance
 - (lifetime dose of ~20 dpa for zircaloy after 40-50 MWd/kgHM)
- High melting temperature
 - Provides additional safety margin for accident conditions
- Isotropic properties



Comparison of properties of candidate cladding base materials

	Mg	Al	Ве	Zr	Fe	Cr	Ni	V	Мо	SiC
Thermal neutron absorption cross section (barns)	0.063	0.23	0.009	0.185	2.5	3.1	4.5	5.08	2.6	0.087
Thermal conductivity (W/m-K)	156	237	201	22	80	94	91	31	138	20*
0.5 T _M (°C)	183	194	502	790	630	792	590	808	1170	1278
Crystal structure	hcp	fcc	hcp	hcp	bcc	bcc	fcc	bcc	bcc	fcc

*value for through-thickness CVD SiC/SiC composite; high purity SiC has K_{th}~350 W/m-K

Zr has one of the highest heats of oxidation; almost any other candidate is preferable in terms of heat contribution during a high temperature LOCA for the U.S. Department of Energy



Strength of some candidate cladding materials



• Mo alloys and SiC/SiC ceramic composite offer improved high temperature strength

National Laboratory

High-Pressure Steam Oxidation Tests: Comparison of the Extent of Steam Reaction

Various materials exposed to pure steam for 8 hours (various flow rates and pressures):

- Zircaloy: Pawel-Cathcart and Moalem-Olander data
- 317 Stainless Steel: ORNL high-pressure tests; thickness loss data
- NITE and CVD SiC: ORNL high-pressure tests; thickness loss data
- 310 Stainless Steel: ORNL high-pressure tests; mass gain data converted to thickness loss
- FeCrAl Ferritic Steel: ORNL high-pressure tests; mass gain data converted to thickness loss



Understanding and Testing Advanced Protection Options for LOCA conditions

Protection by : chromia (stainless), silica (SiC), or alumina (AFA steels) formers



Enhancing accident tolerance of nuclear fuel systems

 Reactor safety margin may be improved through new fuel forms with much reduced exothermic reaction, suppressed hydrogen production, and greater time to fission product release.



Evolution of Nuclear Power Systems



for the U.S. Department of Energy

M.L. Corradini, Univ. Wisc. RIDGE

Overview of fission reactor options

- Light Water Reactors (LWRs): pressurized- and boiling-water designs
 - Present fleet of nuclear power plants (UO₂ fuel, zircaloy cladding)
 - Pressing for higher performance, improved fuel reliability and accident tolerance
- "Gen-IV" High Temperature Gas-Cooled Reactors
 - High temperature process heat applications as well as electricity production;
- "Gen-IV" Na-cooled Fast Reactors
 - Close the nuclear fuel cycle by "burning" transuranic isotopes and fission product wastes from LWR plants
- Other "Gen-IV" reactor concepts
 - Supercritical water reactor
 - Molten salt reactor
 - Pb-cooled fast reactor
 - Gas-cooled fast reactor



New technology, New requirements

	Gen-III Pressurized Water Reactor	Gen-IV Fast Reactor	Very High Temperature Reactor
Coolant	Water	Sodium	Helium
Power Density (MW/m ³)	100	350	5
Coolant Temp. (C)	330	550	1000
Net Plant Efficiency (%)	34	40	50









Approaches for radiation resistance 2: Immobile defects

- Defect accumulation is limited if one or more defect types are immobile
 - Utilize materials with negligible point defect mobility at desired operating temperatures
 - A key potential consequence (particularly in ordered alloys and ceramics) is amorphization, with accompanying significant volumetric and property changes



Regime with intrinsically high point defect recombination typically occurs at too low of temperatures for power generation applications (except SiC and possibly Al₂O₃, W, Re) K
 <sup>17 Managed by UT-Battelle for the U.S. Department of Energy after S.J. Zinkle, Chpt. 3 in Comprehensive Nuclear Materials (Elsevier, 2012)
</sup>









Materials Comparison at 1000°C

			Irradiation-Induced Property Change @ 1000°C				
Material	Cost	Life	Volume	Strength	Modulus	Thermal	
	\$/Kg	(dpa)		(MPa)		Conductivity	
						W/m-K	
Superalloy	25	~5	-	-	-	-	
CFC*	~200	10-15	-5%	150→250	+20%	250→180	
SiC/SiC*	~400	>50?	+1%	75 → 75	-10%	50→20	

* does not include prototyping or NDE evaluation.

NGNP	Operating Temp	Maximum Temp	Lifetime Dose
Control Rods & Guide Tubes	1200°C	1600°C	25 dpa
Upper Plenum Shroud/Core Restraint	650°C	1300°C	0.05 dpa
Floor Blocks	600°C	600°C	<0.05 dpa
Hot Duct Inner Shell	1000°C	1200°C	0.005 dpa



Composite Materials for Generation IV Reactors





Fiber-reinforced Ceramic Composites provide High Toughness vs. Monolithic Ceramics





Composite materials, whether platelet, chopped fiber, or continuous fiber reinforced are superior "engineering" materials to monolithics:

- generally higher strength, especially in tension
- higher Weibull modulus (more uniform failure)
- much higher damage tolerance (fracture toughness)



Composite Materials for Generation IV Reactors

• In all gas cooled reactors there is a need for in-core components which are subjected to tensile loading. Nuclear graphite, or other "engineering" ceramics can not be used for such applications.

• Components such as hangers and control rods are typically under modest tensile load (tens of MPa) and are not at the highest core fluence.





Yield Strength of Various Structural Materials





Performance of Candidate Alloy 800H Control Rod





Potential Need for Composite Materials for Gen IV



for the U.S. Department of Energy

Year



Development of SiC Composites for Nuclear Reactor Structural Applications: Difficult & High Risk But High Payoff

- SiC Composites Offer
 - Low radioactivity and afterheat; chemically inert (eases safety and waste disposal concerns)
 - High operating temperatures (greater thermodynamic efficiency) and low thermal neutron absorption
- The Feasibility Issues
 - Conventional SiC composites are not a hermetic barrier to fission gases
 - Thermal conductivity is reduced by irradiation
 - Little is known about mechanical property response to irradiation
 - Technology base for production, joining, design of large structures is very limited
- Key Research Topics
 - Understand the magnitude and cause of radiation effects on key properties such as thermal conductivity and strength

- Design composite structures (fiber, fiber-matrix interphase and matrix) with improved performance
- Develop the required technology base with industry and international partners



Silicon carbide composites offer engineered structures for extreme environments through tailoring of the fiber, matrix, and interphase structures



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Dimensional Change in 1-D Composite





Candidate Nuclear Graphite Compared to CFC



SiC/SiC Composites : Thermal Conductivity

Due to "interfaces" and cracks in SiC composite, thermal conductivity will necessarily be less than ideal SiC.

Present materials are significanlty lower than ~15 W/m-K reactor study goal.



Comparison of Radiation-induced Thermal Conductivity Degradation of Carbon-fiber composites





Comments on SiC and carbon fiber composites

• In order to transition from current proof-of-principal studies to an application phase for ceramic composites, a more comprehensive program is needed:

- Fundamental understanding of engineering properties such as swelling, thermal conductivity, irradiation creep, environmental corrosion, etc.
- Demonstration of scalability and component Q/A.
- Development of ASTM accepted testing standards and coordination with ASME for codification of the material.

• The ultimate choice between Carbon Fiber Composite and SiC/SiC will primarily depend on the dose and temperature of application:

- CFC's : High Irradiated Thermal Conductivity (>50 W/m-K) Limited Lifetime (10 dpa for T , ~ 700°C) (~ 1 dpa T>1000°C)

- SiC/SiC : Poor thermal conductivity (< 5 W/m-K)

Apparent Long Lifetime (> 10 dpa, T< 1300°C)







T. Kakuta et al.



Observed absorption of ITER round robin fib during fission neutron irradiation.



Summary

- Nonmetallic materials provide important capabilities for a wide range of current and proposed fission and fusion reactors
 - Generally based on high tolerance to extreme temperatures and radiation levels, or unique optical or insulating properties of ceramics
 - Microencapsulated fuel systems for gas-cooled and accident-tolerant water cooled reactor designs
 - SiC/SiC and CFC composites for structural applications
 - Neutron control systems for fission reactors
 - Diagnostic applications (optical fibers, windows, bulk insulators, MI cables)
 - Plasma heating systems
 - Fusion ceramic breeders
 - Fission waste storage forms

