

**2445-01**

**Advanced Workshop on Nanomechanics**

*9 - 13 September 2013*

**Coherent manipulation and phonon lasing in electromechanical resonators**

Hiroshi Yamaguchi

*NTT Basic Research Laboratories*

A scanning electron micrograph (SEM) of an electromechanical resonator. The device features a central yellow rectangular region, likely a piezoelectric layer, surrounded by green and grey regions representing different materials or layers. The structure is mounted on a blue substrate. The text is overlaid on the image.

# Coherent manipulation and phonon lasing in electromechanical resonators

H. Yamaguchi, I. Mahboob, and H. Okamoto  
NTT Basic Research Laboratories

## 1. Introduction

## 2. Parametric mechanical resonators

- GaAs-based piezoelectric resonators

## 3. Two-modes coupling

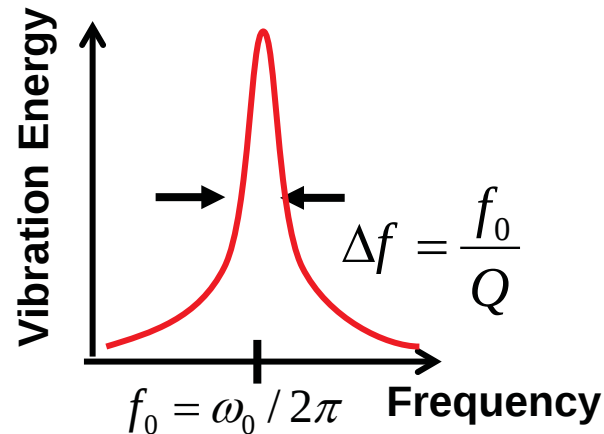
- Stress-driven inter-modal coupling
- Strong-coupling and Electromechanically-induced transparency

## 4. Three-modes coupling and all-mechanical phonon lasing

- Basic concepts of phonon lasing
- Noise-excited sharp mechanical oscillation and threshold properties

## 5. Coherent phonon manipulation in paired mechanical resonators

- Intermodal parametric coupling of two paired resonators
- Coherent control of mechanical oscillation
- Higher order parametric mixing

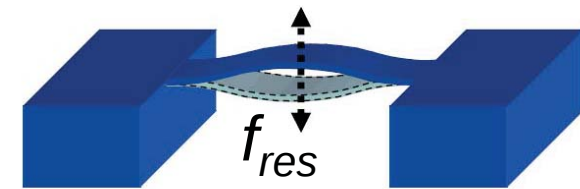


## Equation of motion

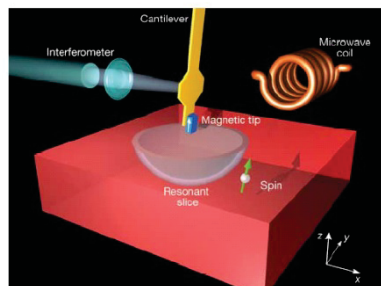
$$m \frac{d^2 x}{dt^2} + \frac{m \omega_0}{Q} \frac{dx}{dt} + m \omega_0^2 x = F \cos \omega t$$

$$x(t) = \frac{F}{\sqrt{(\omega_0^2 - \omega^2)^2 + \omega_0^2 \omega^2 / Q^2}} \cos(\omega t - \theta)$$

$f_0$  : 100Hz -1GHz,  $Q$ :  $10^3$  - $10^6$



Beam resonator



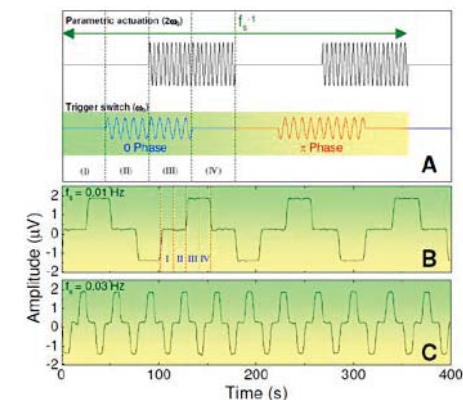
D. Rugar et al. Nature

## Ultrasensitive Force/Mass Detection

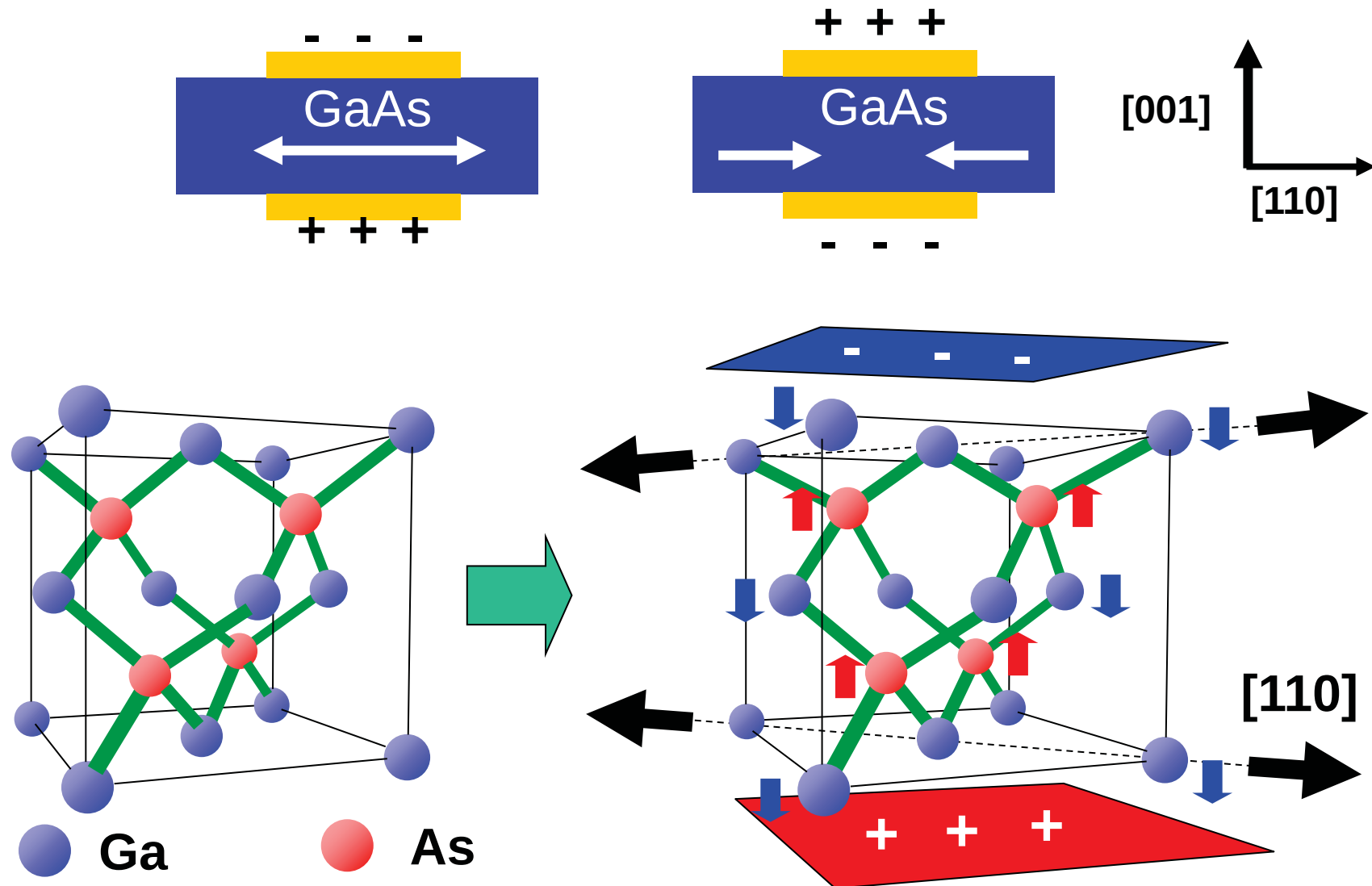
- Displacement detection up to femtometer scale (UCSB)
- Zeptogram mass sensing (Caltech)
- Single spin sensing (IBM)

## Signal processing

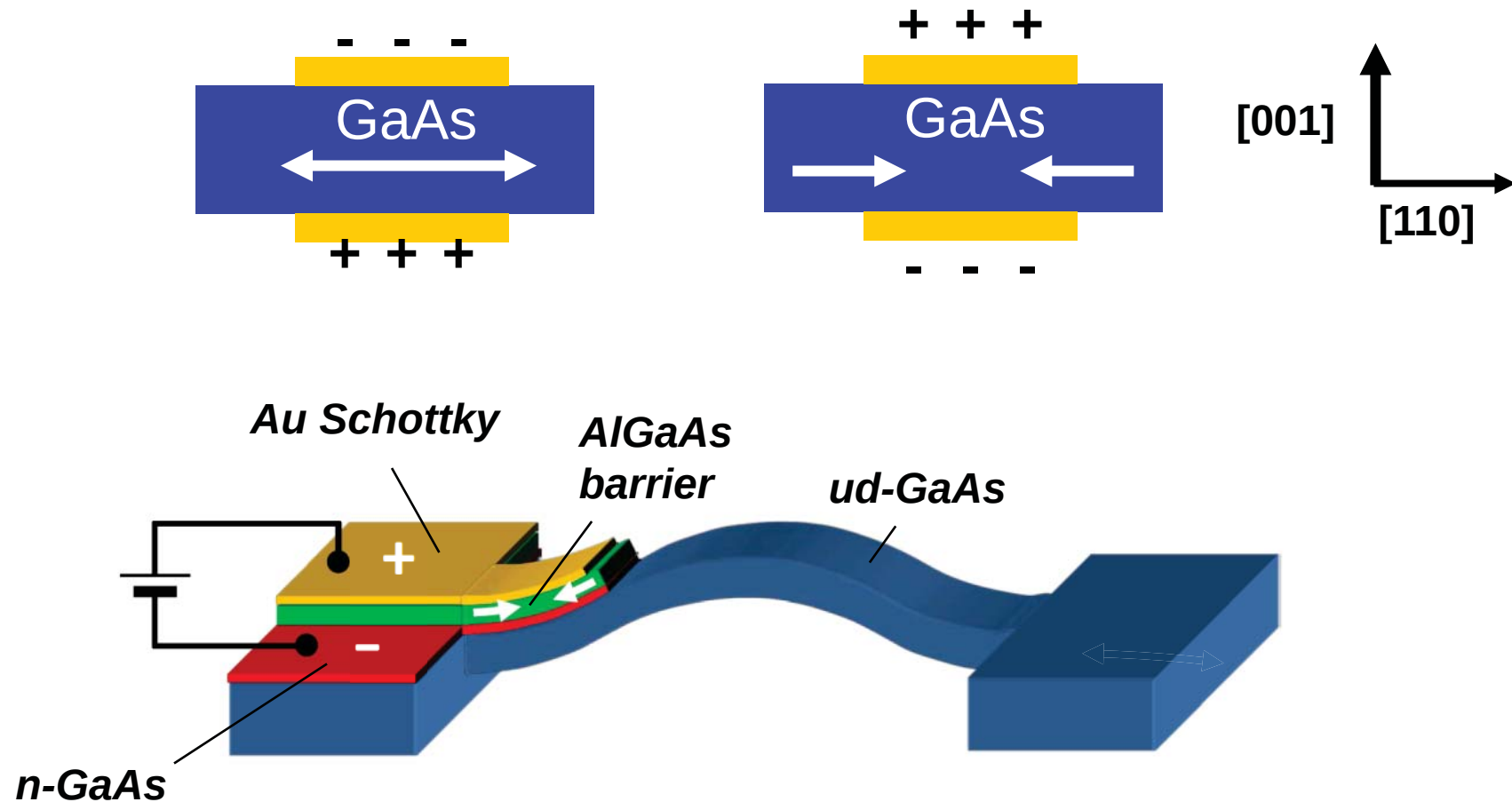
- Bistability in nonlinear Duffing resonators (Boston, APL 2004)
- Mechanical Parametron Computers (NTT, Nature Nano. 2008)



## Stress-voltage transduction



## Stress-voltage transduction

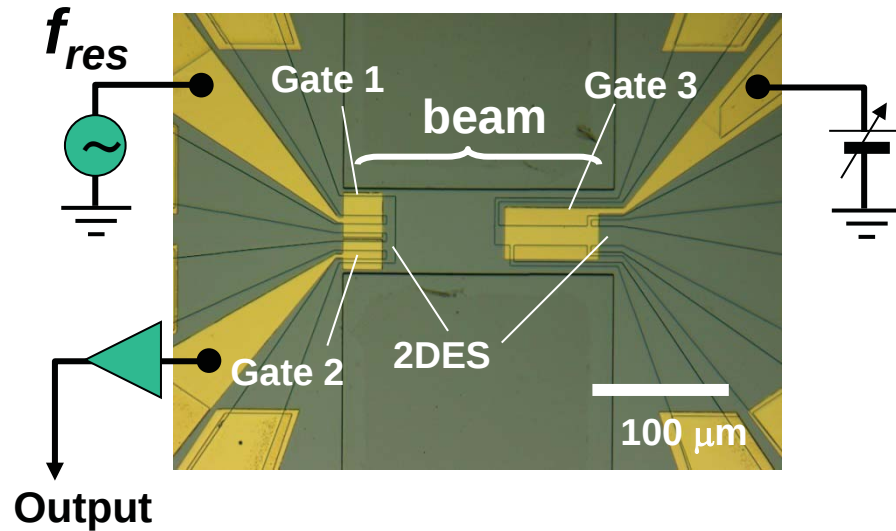


**Electrical actuation, detection and frequency control**

S.C. Masmanidis, et al. *Science* 317, 780 (2007)

I. Mahboob and H. Y., *Nature Nanotechnology* 3, 275 (2008)

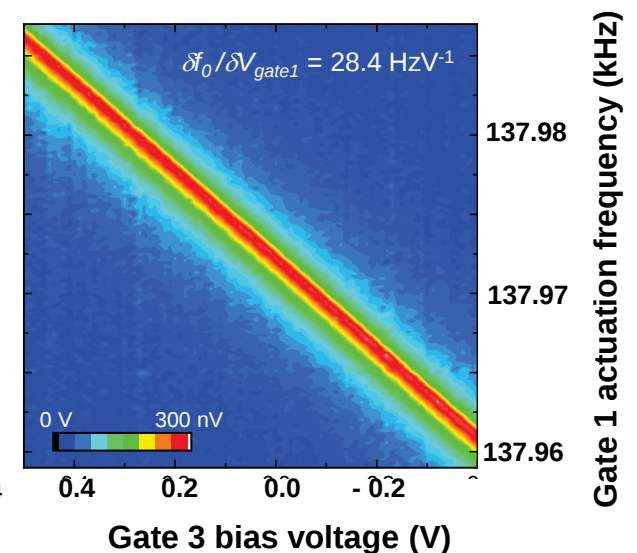
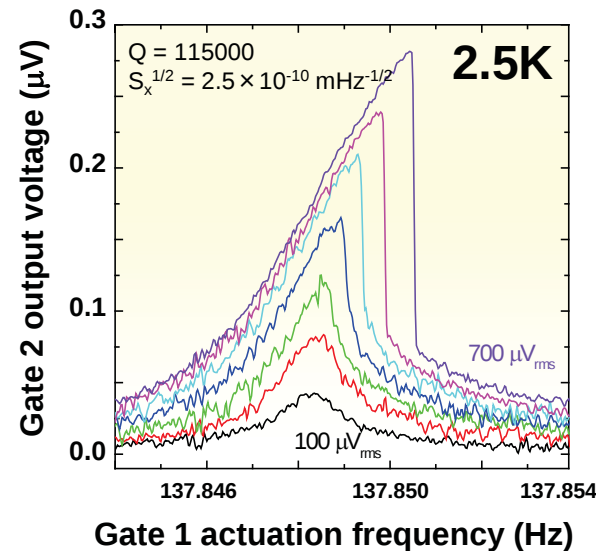
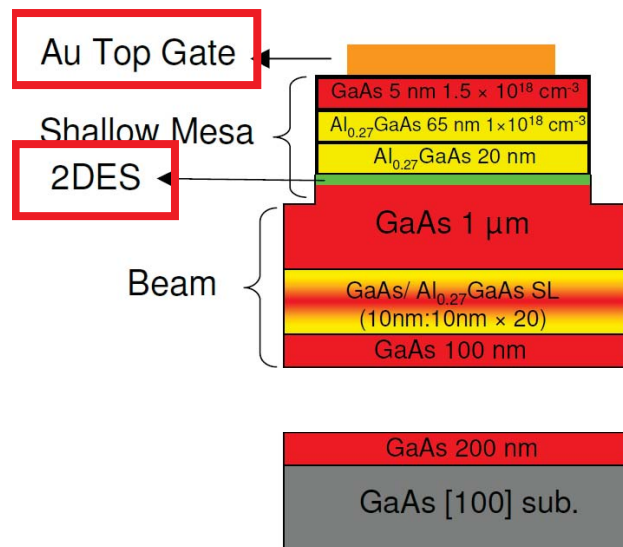
Fabricated device (top view)



**Gate 1: Application of AC voltage**  
 → *Actuation through bending moment*

**Gate 2: Measurement of generated voltage**  
 → *Beam-motion detection*

**Gate 3: Application of DC voltage**  
 → *Resonance frequency modulation*



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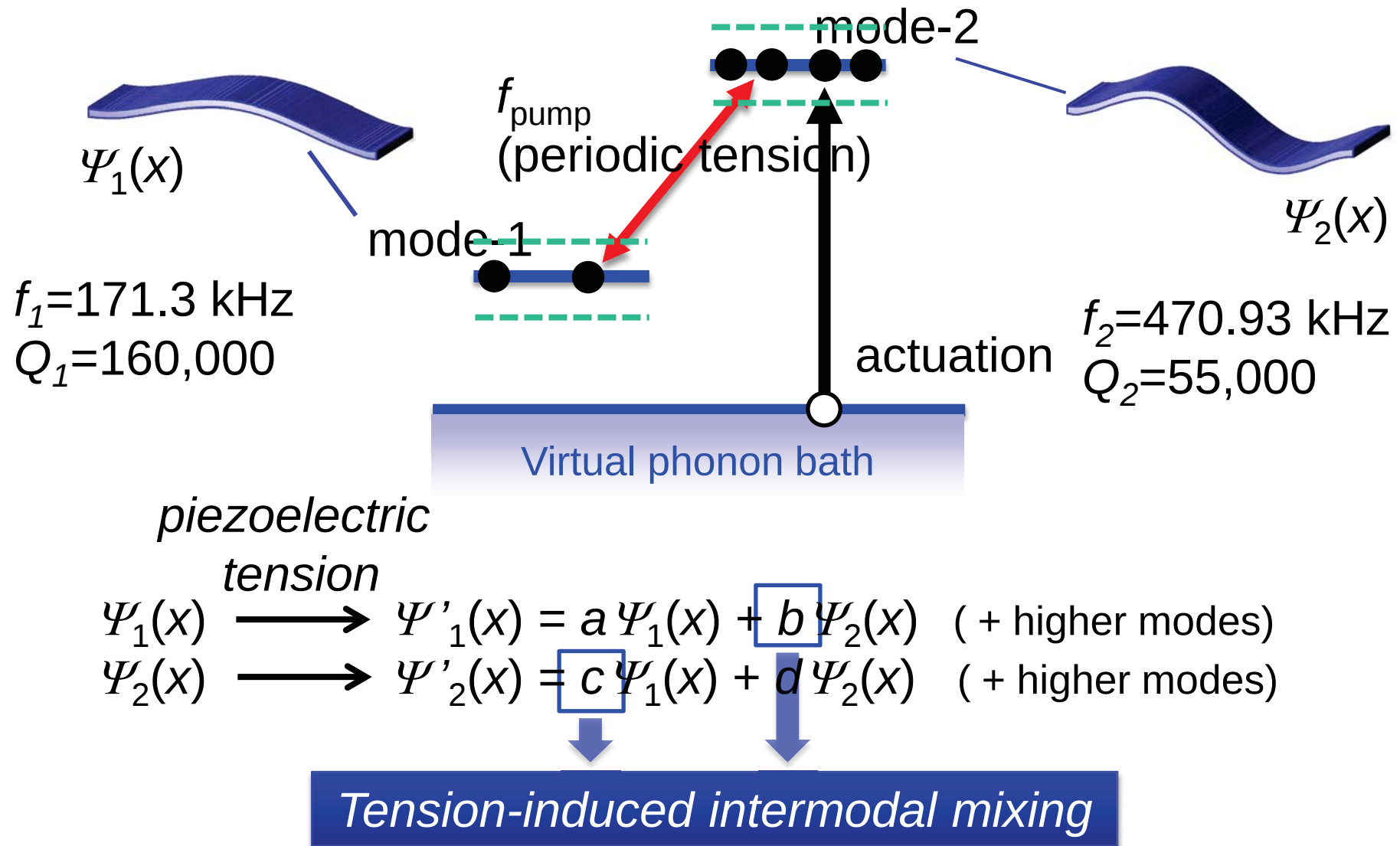
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- Basic concepts of phonon lasing
- Noise-excited sharp mechanical oscillation and threshold properties

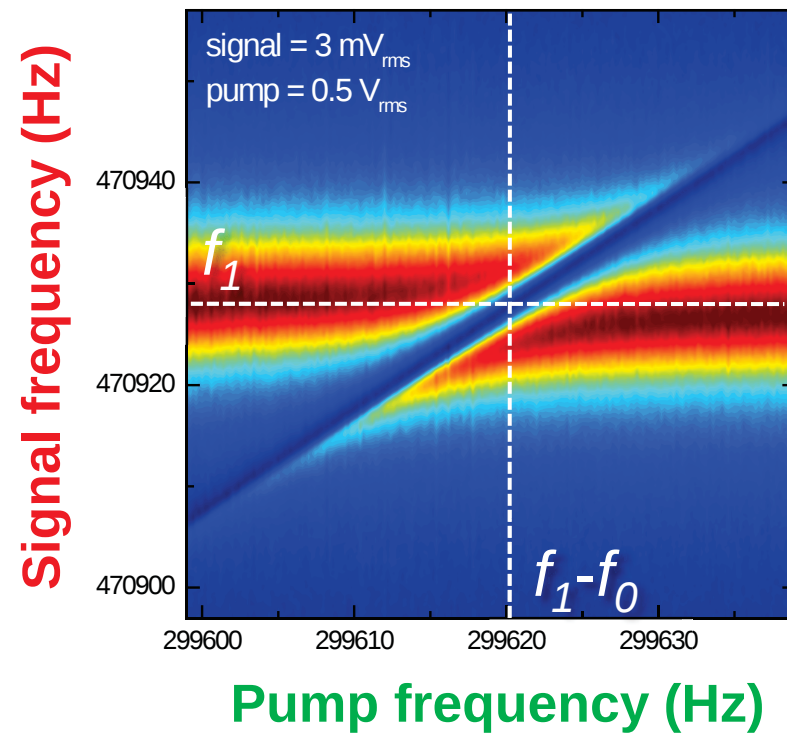
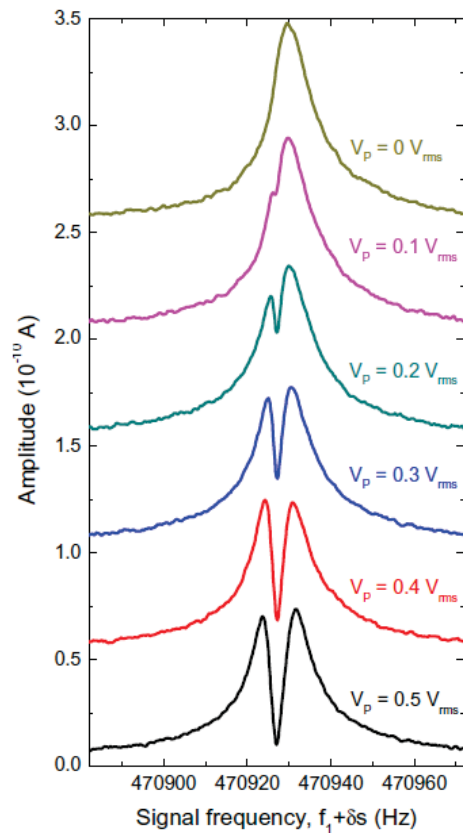
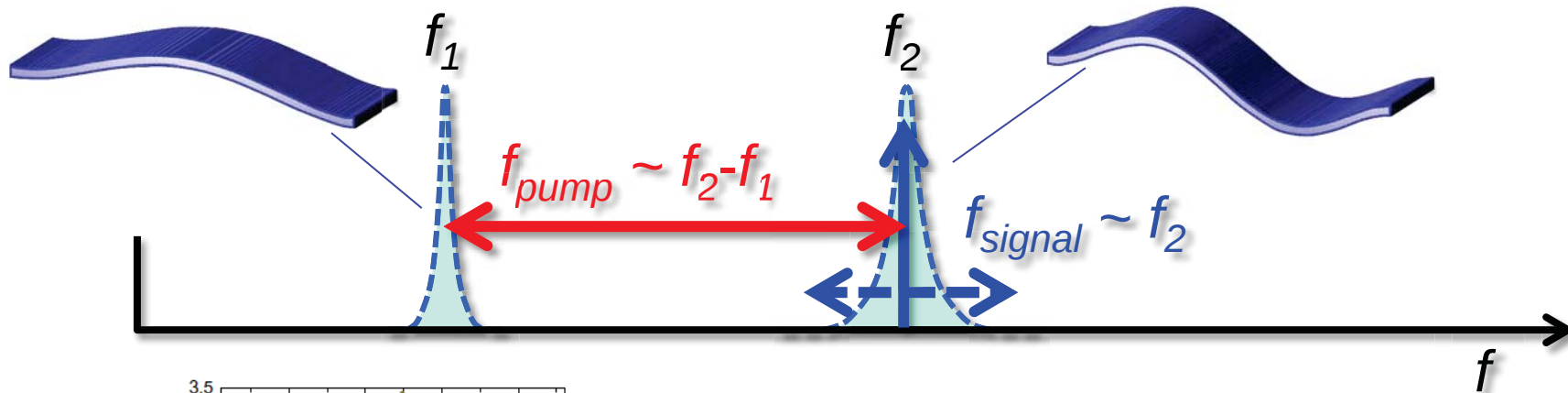
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# Mechanical two-mode system



# Dynamic inter-mode coupling



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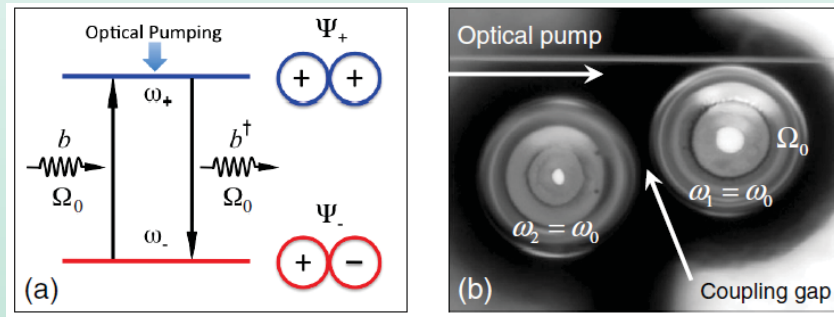
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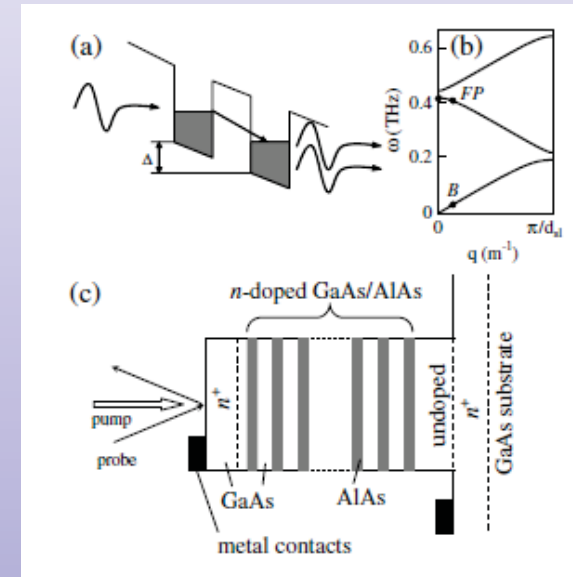
## Optomechanical systems



Ivan S. Grudinin et al. PRL2010

- **Photon transition between two optical modes induce the stimulated emission of phonon.**
- **Mechanical oscillation at 23.4 MHz was induced by optical pump.**
- **Threshold characteristics was confirmed.**

## Stark Ladder Superlattices

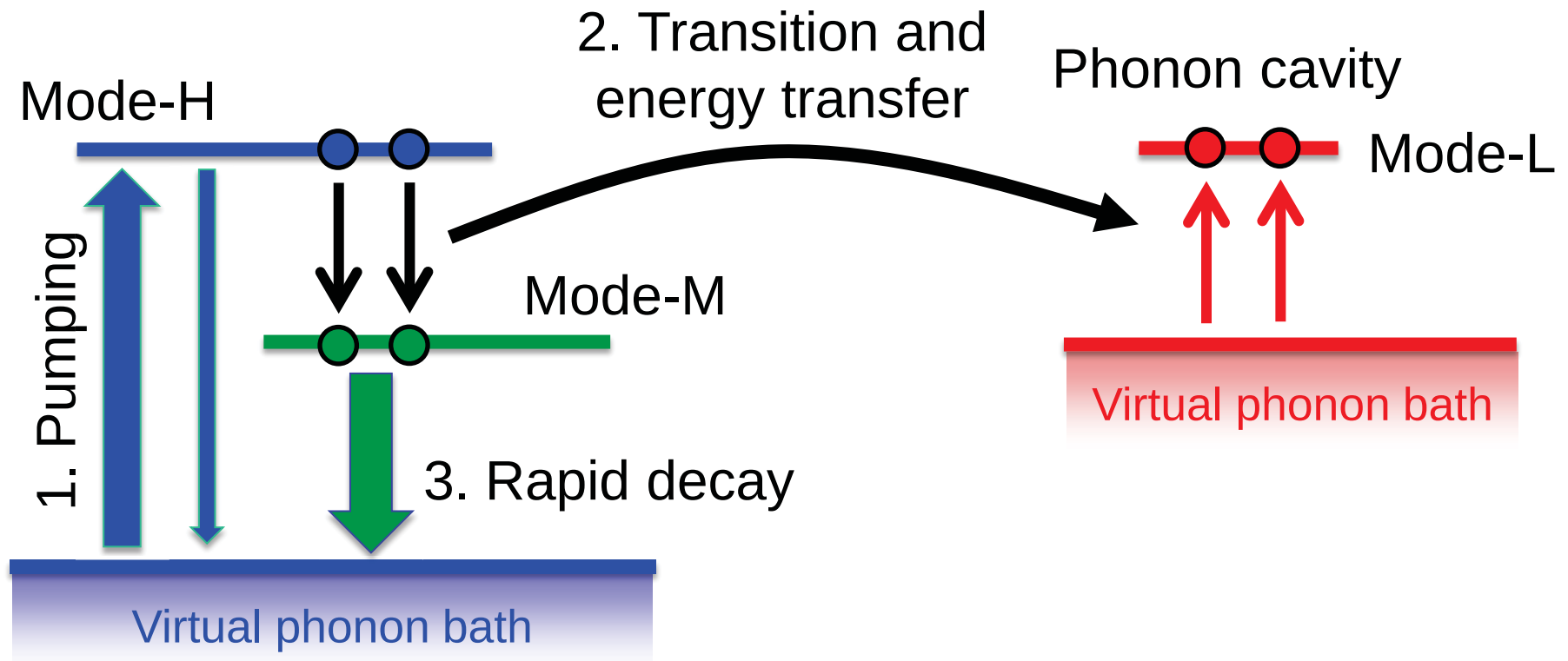


R. P. Beardsley et al. PRL2010

- **Phonon generation by the transition of electron states.**
- **Amplification for 0.4 THz lattice vibration was confirmed.**

*Two-level systems coupled with the frequency-matched phonon cavity are required for the phonon lasing operation.*

**Phonon/Sound amplification by stimulated emission of radiation (PHSER/SASER)**

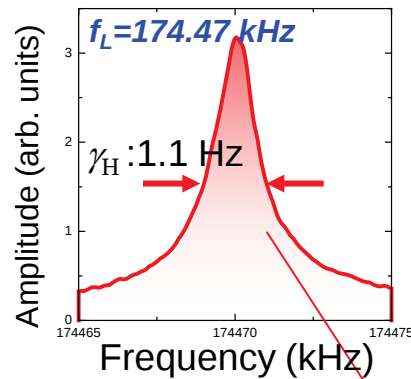


## Requirements:

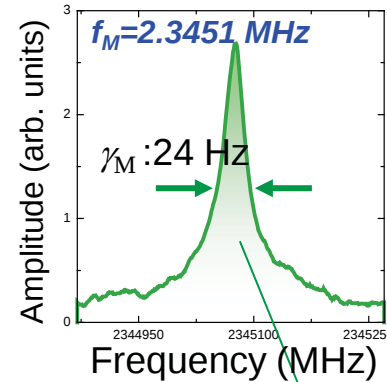
1. Two level systems (can be both fermionic and bosonic)  
→ **Two mechanical modes (mode-H and -M)**
  2. Energy-matched phonon cavity  
→ **One mechanical mode (Mode-L)**
  3. Coupling between two level systems and cavity phonon  
→ **Parametric coupling**
- Three mechanical modes**

## 1. Choosing three modes with frequency matching: $f_H - f_M \sim f_L$

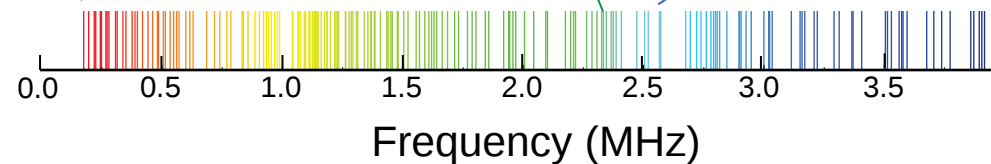
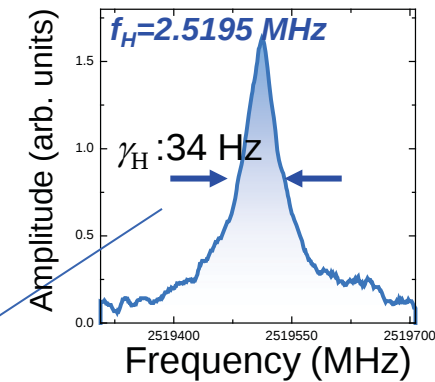
Mode-L



Mode-M

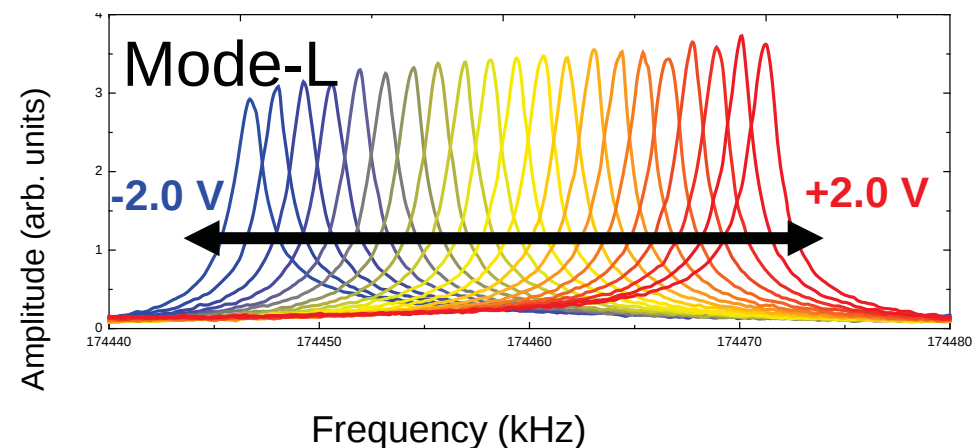


Mode-H

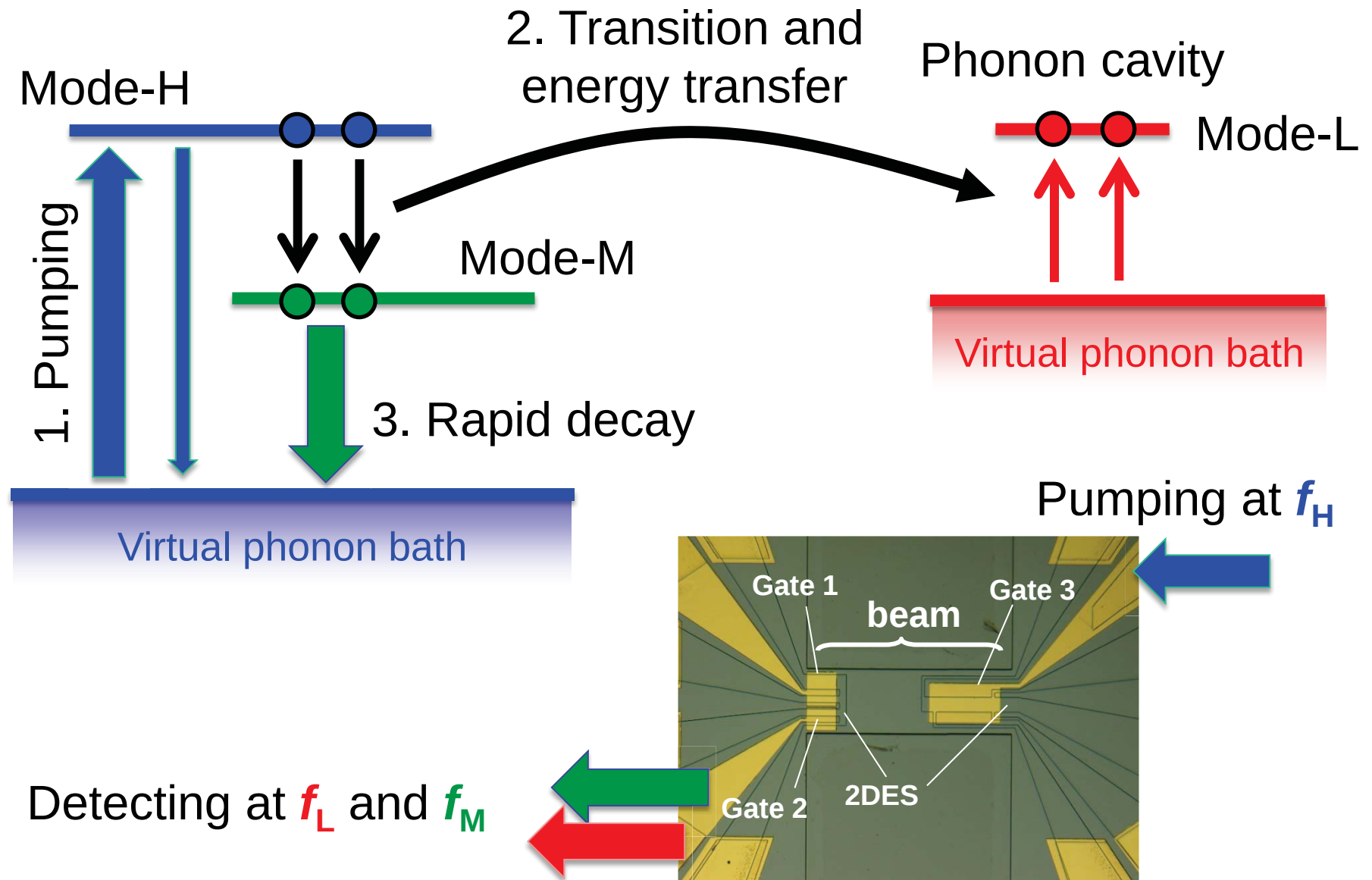


## 2. Fine tuning by applying a gate voltage

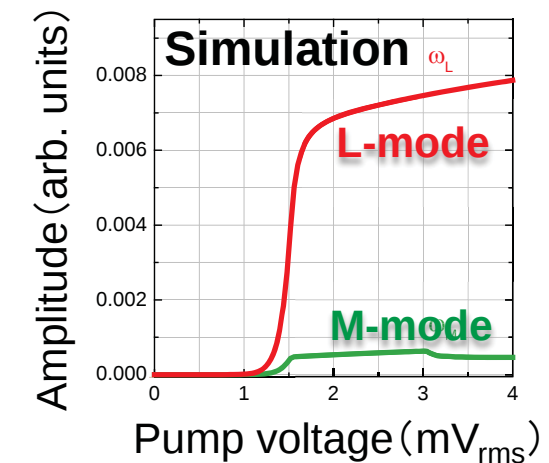
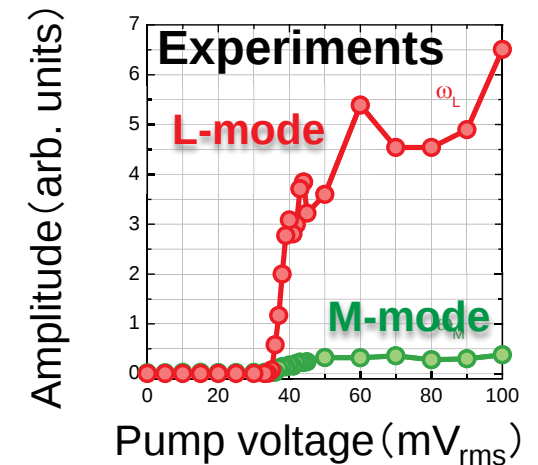
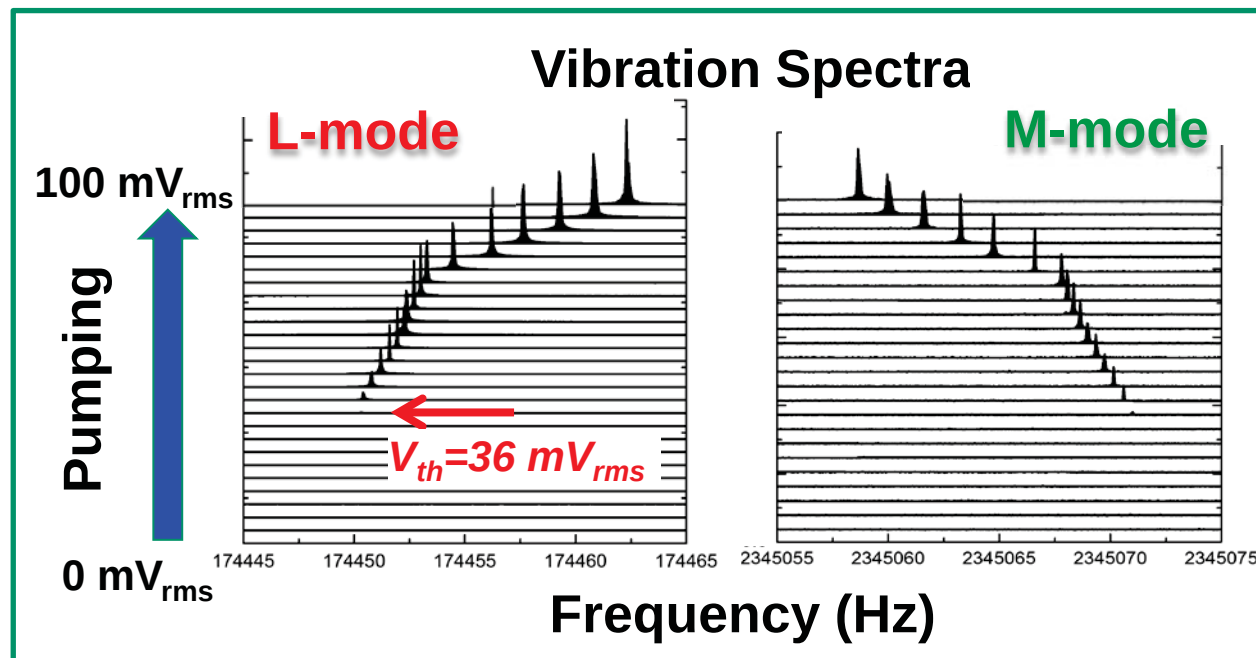
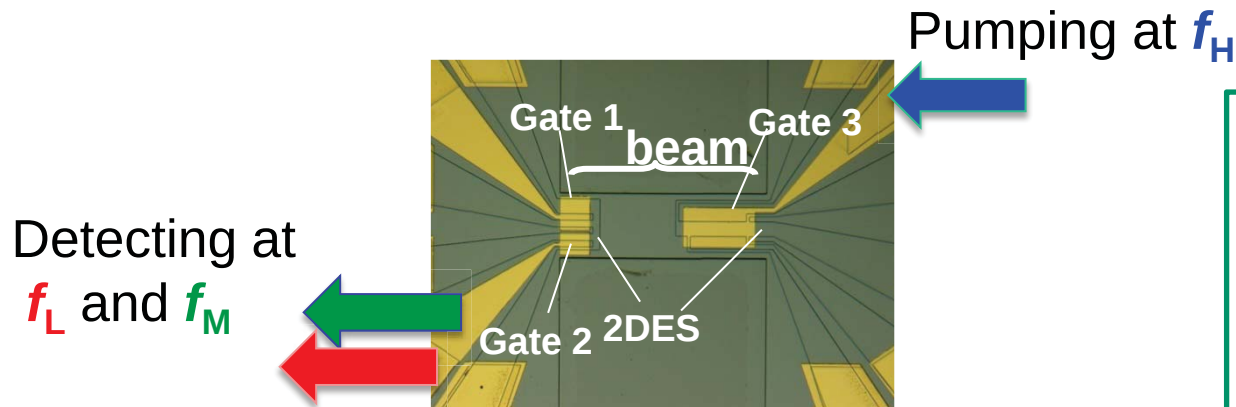
$$\rightarrow f_H - f_M - f_L < \gamma_H, \gamma_M$$



# Basic processes for “phonon lasing” operation

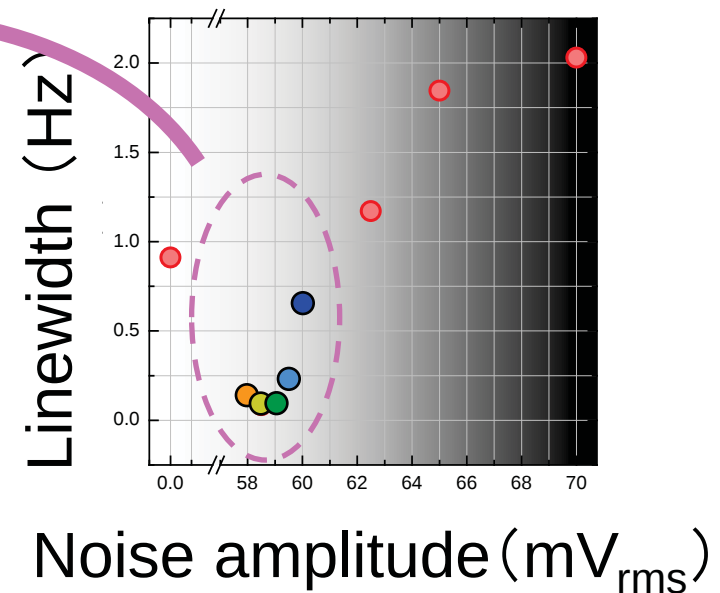
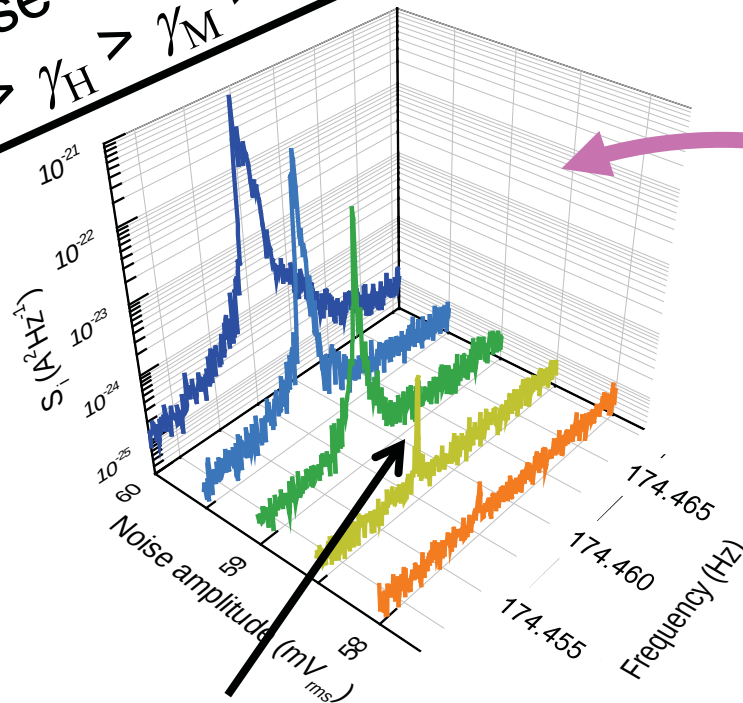


# Threshold characteristics



- ✓ Clear threshold characteristics was observed
- ✓ Good agreement with theoretical simulation

Input noise band width:  
 $70\text{Hz} > \gamma_H > \gamma_M \gg \gamma_L$



Minimum spectral linewidth : 80 mHz

- ✓ Noise pumping can also induce oscillation.
- ✓ Line narrowing was observed.
- ✓ Incoherent pumping results in coherent oscillation.

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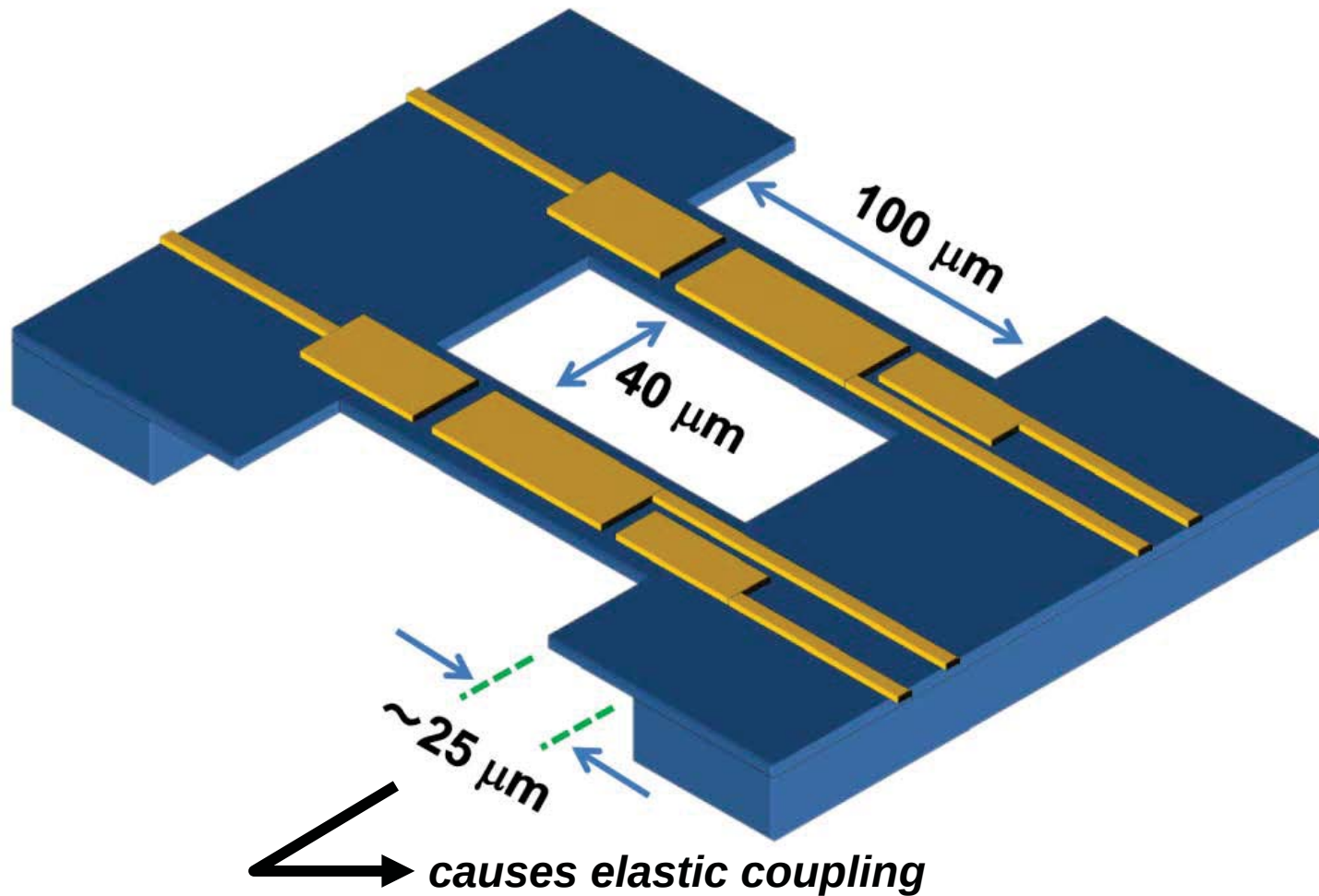
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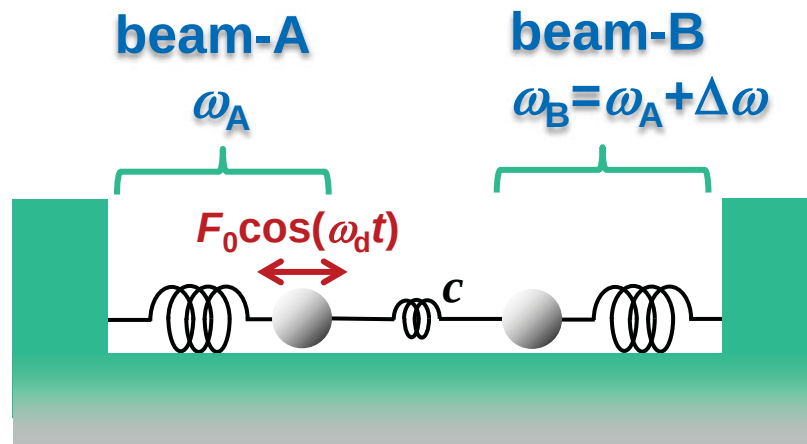
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***Coupled parametric electromechanical resonators***



## Mass and spring model



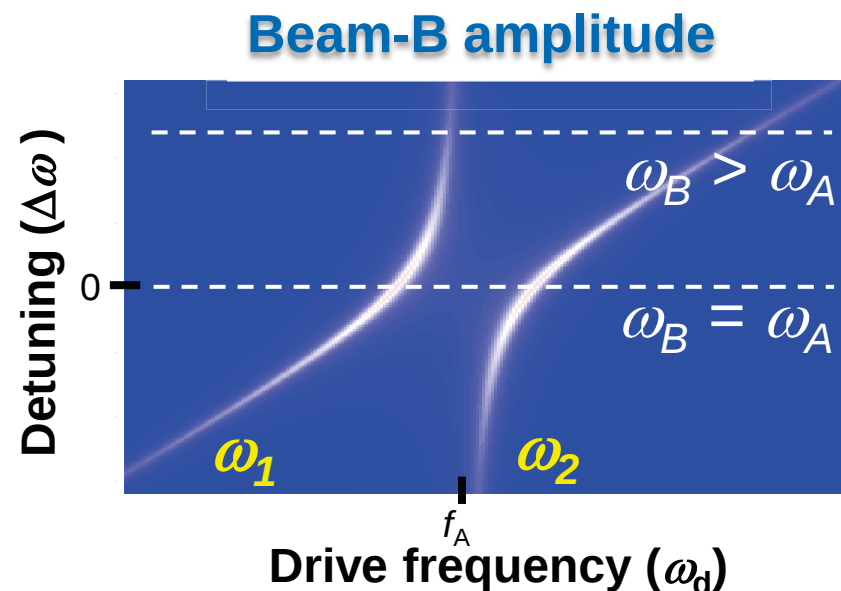
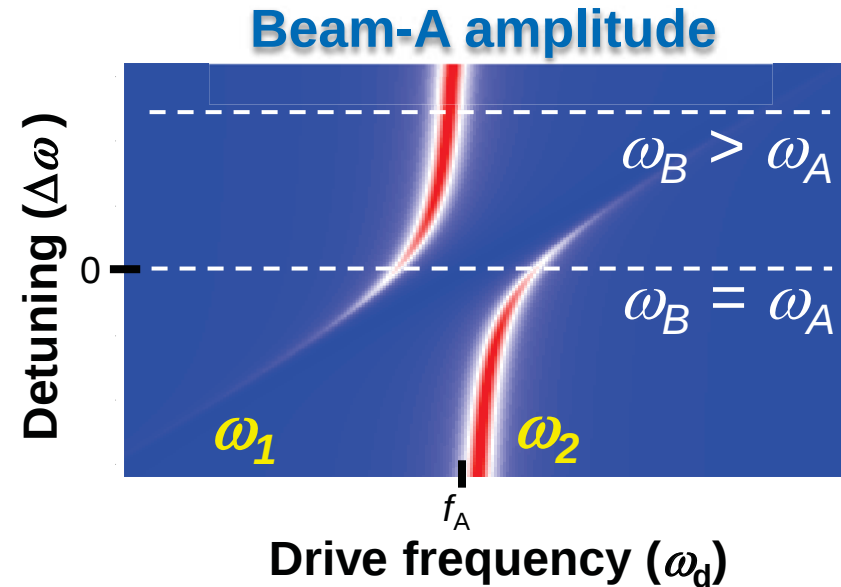
$$\ddot{x}_A + \gamma \dot{x}_A + \omega_A^2 x_A = c(x_B - x_A) + F_0 \cos(\omega_d t)$$

$$\ddot{x}_B + \gamma \dot{x}_B + \omega_B^2 x_B = c(x_A - x_B)$$

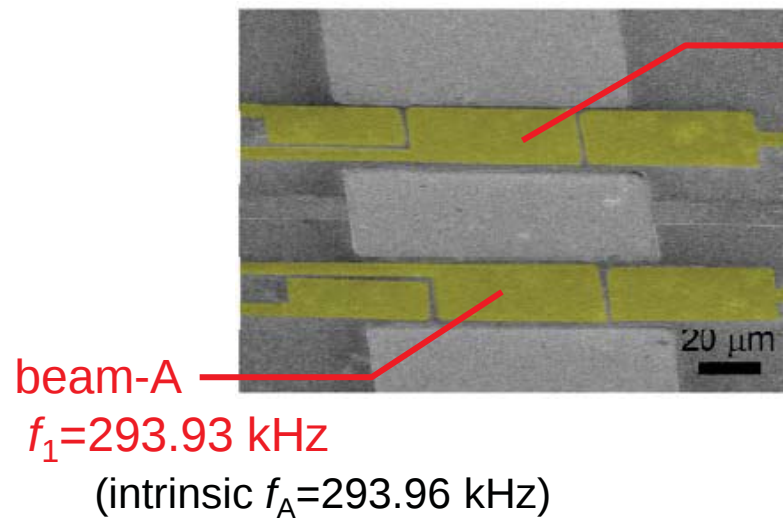
labels A and B  $\rightarrow$  beams

labels 1 and 2  $\rightarrow$  modes

When  $\omega_B$  is detuned from  $\omega_A$ ,  
the coupling is inefficient.



# Dynamical coupling by parametric pumping



$$\omega_* = 2\pi f_*$$

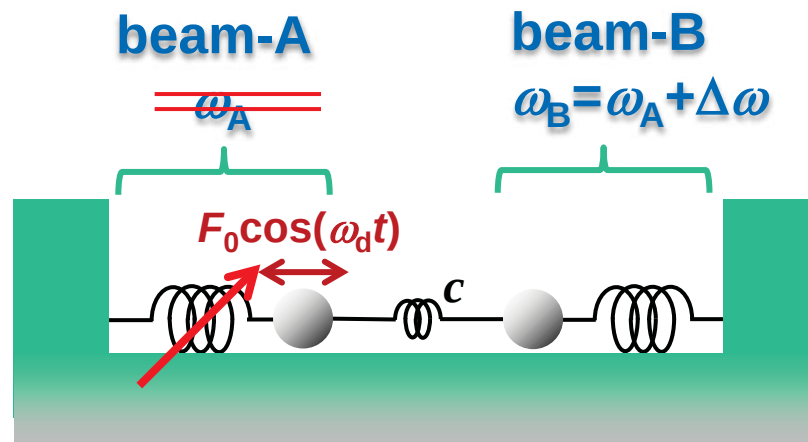
$$f_2 - f_1 = 440 \text{ Hz}$$

$$(\Delta f = f_B - f_A = 380 \text{ Hz})$$



**Coupling is inefficient.**

## Parametric pumping



For the modulation at  $f_p = \omega_p / 2\pi = (f_2 - f_1)$

The frequency mismatch is compensated by the spring constant modulation.

**Two resonators are coupled despite the frequency mismatch.**

The coupling efficiency can be externally controlled by changing the pump amplitude and frequency.

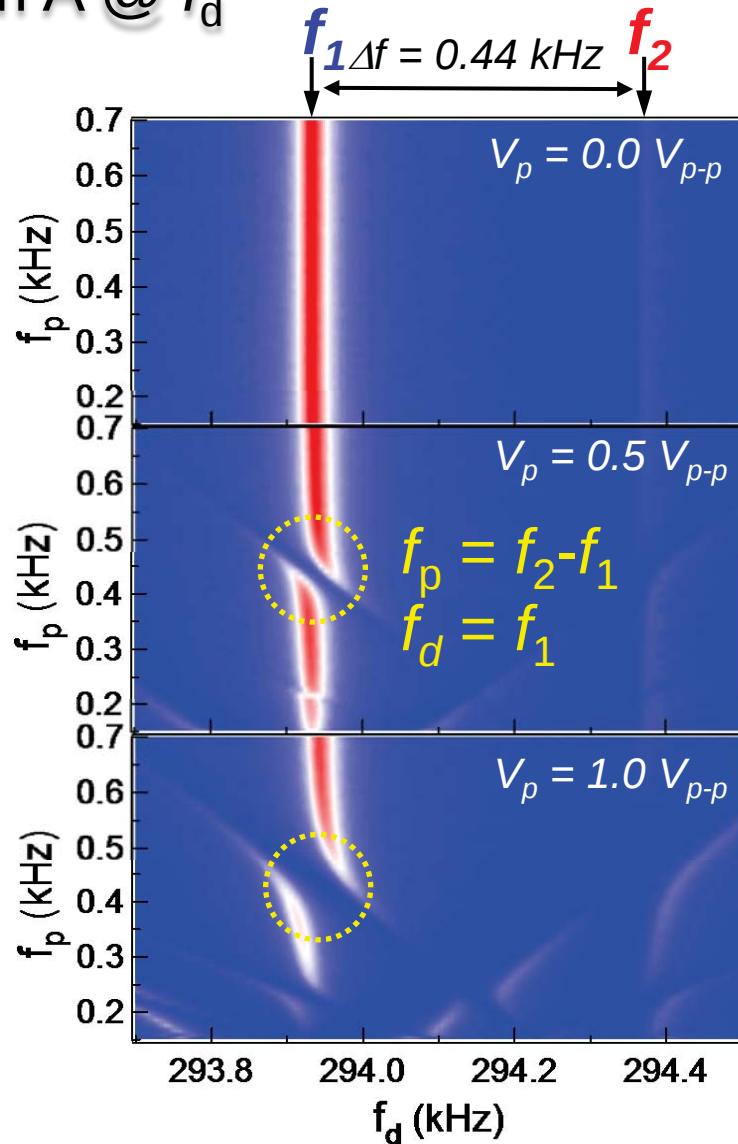
$$\omega_A(t) = \omega_0 + (\Gamma/2\omega_0)\cos(\omega_p t)$$

$$\ddot{x}_A + \gamma\dot{x}_A + [\omega_0^2 + \Gamma\cos(\omega_p t)]x_1 = F_0 \cos(\omega_d t + \delta) + c(x_B - x_A)$$

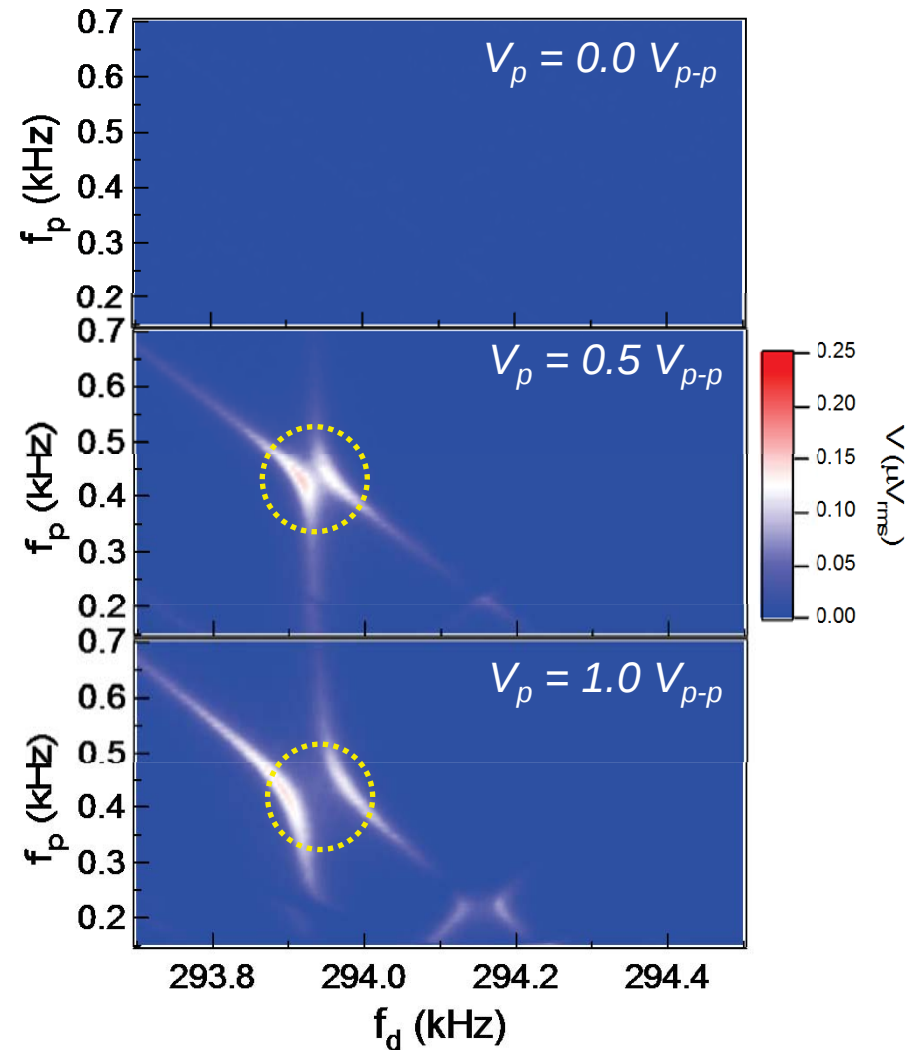
$$\ddot{x}_B + \gamma\dot{x}_B + (\omega_0 + \Delta\omega)^2 x_B = c(x_A - x_B)$$

# Results of experiments

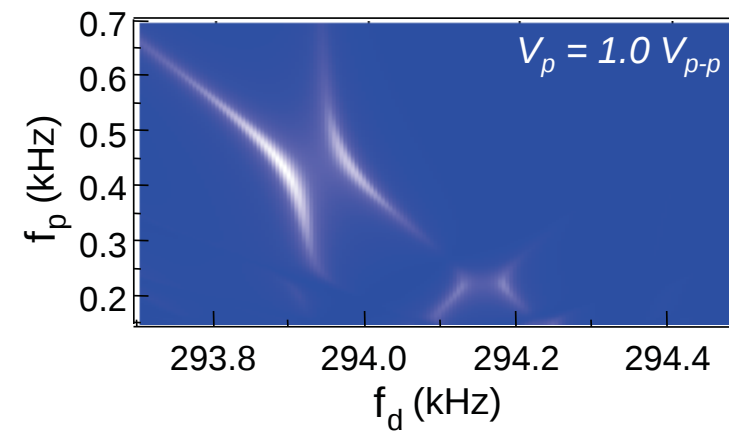
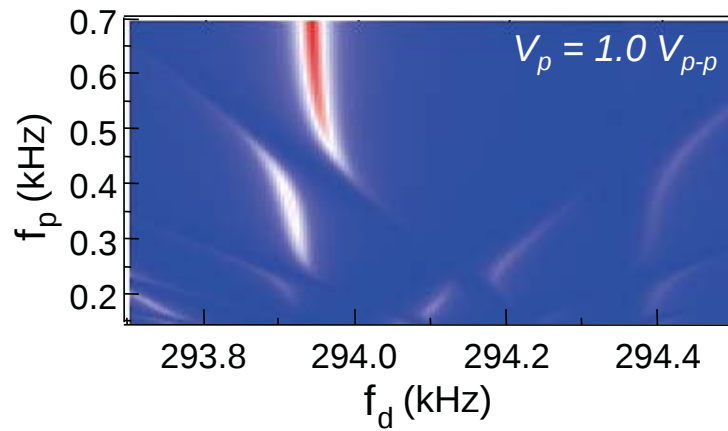
beam A @  $f_d$



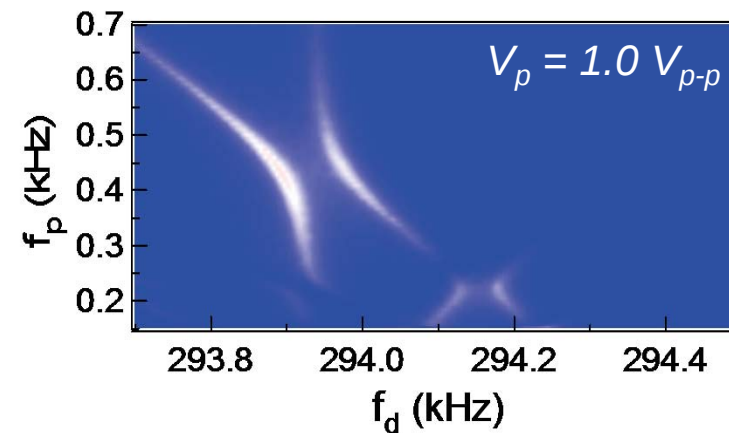
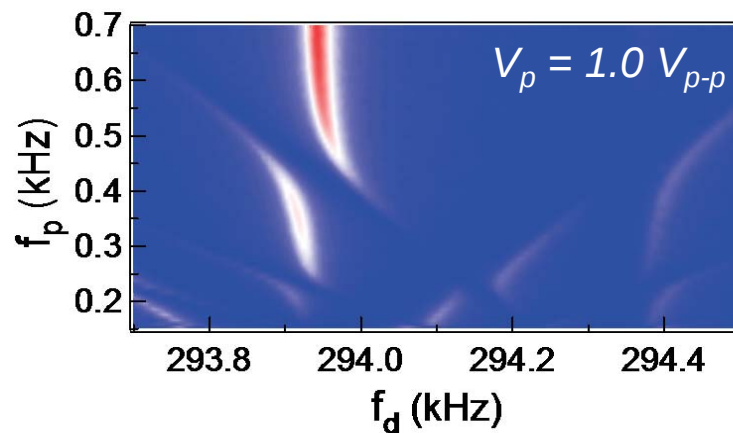
beam B @  $f_d + f_p$



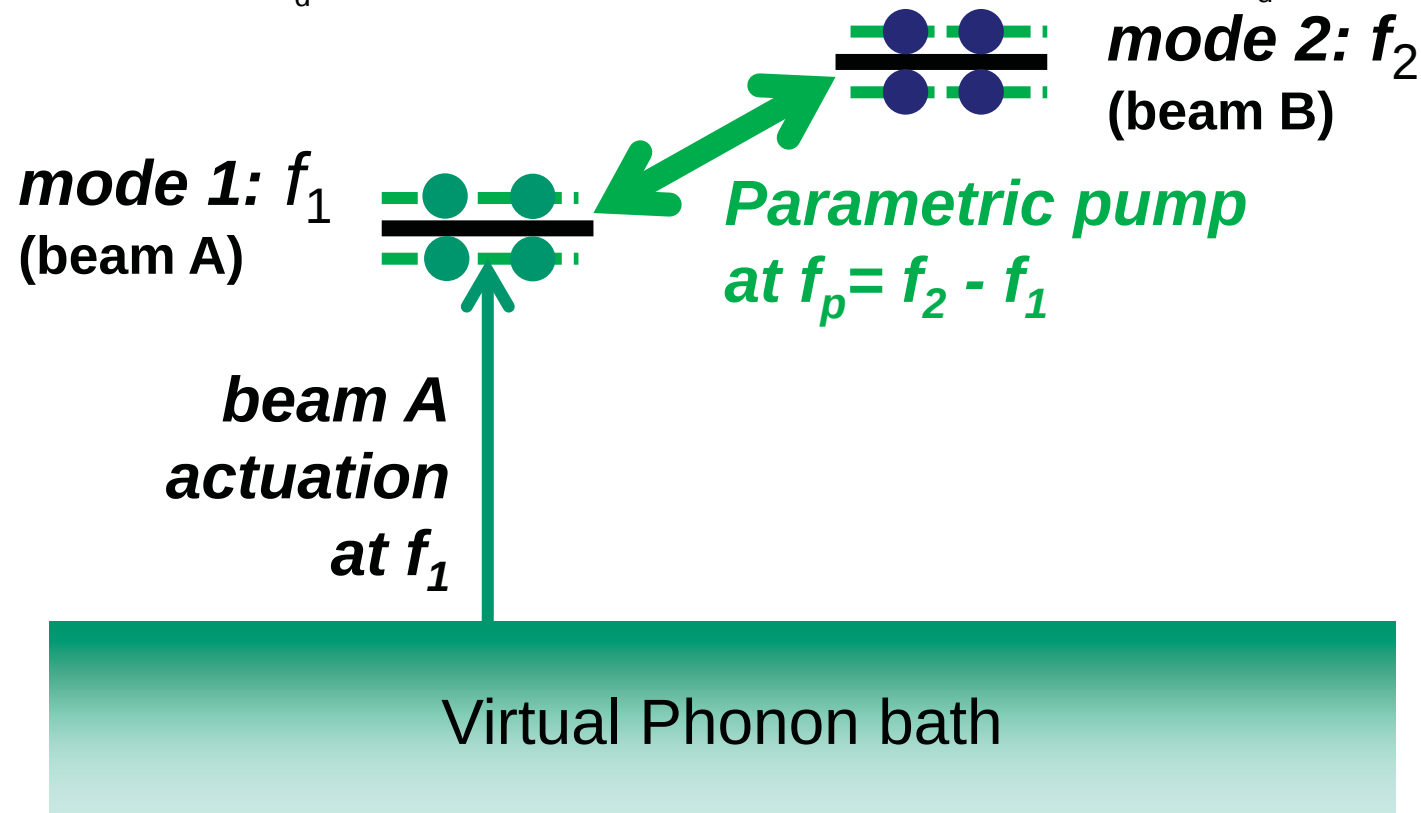
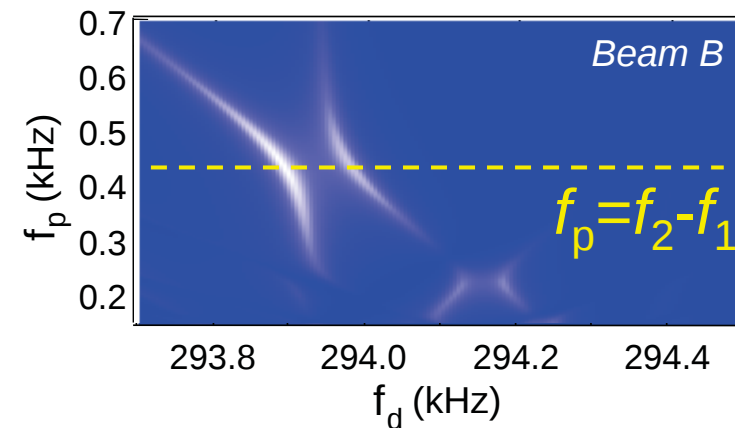
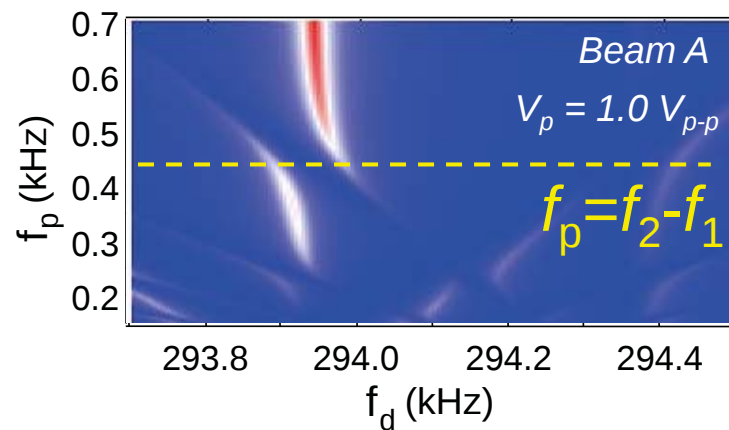
## Simulation



## Experiment



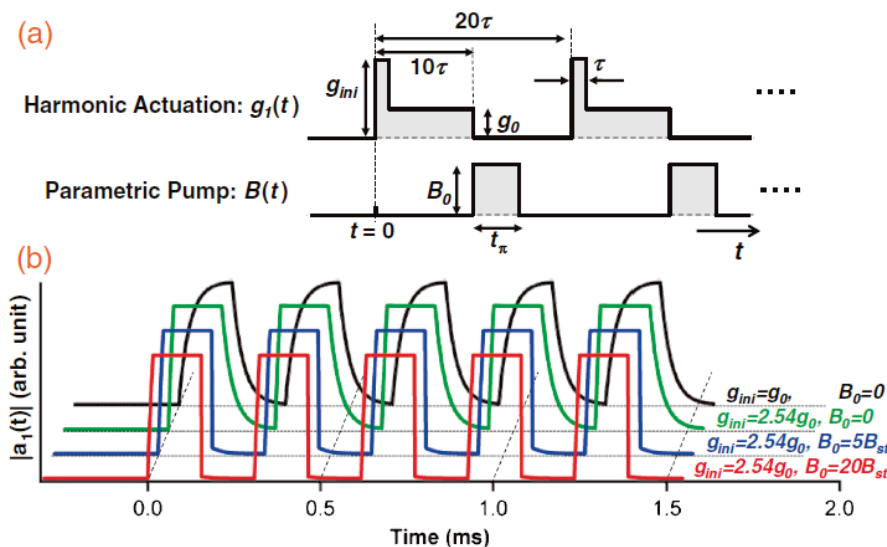
# Quantum mechanical picture using phonon mode



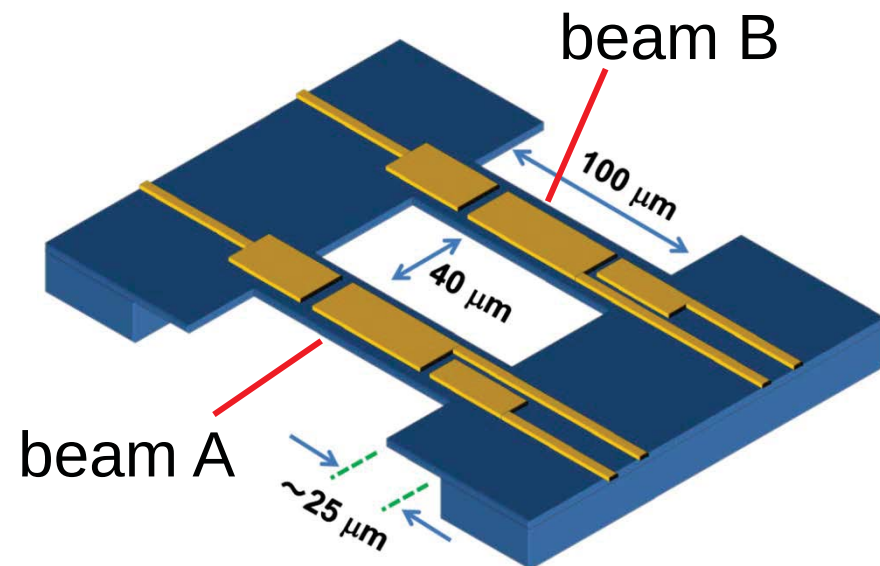
# How we utilize the dynamic strong coupling ?

- The coupling between two modes can be controlled electrically.
- Strong coupling (Rabi splitting) allows the mode transition more rapidly than the energy relaxation rate.
- Therefore, the pulse pumping enables the quick transfer of oscillation energy than the damping rate using Rabi oscillation.

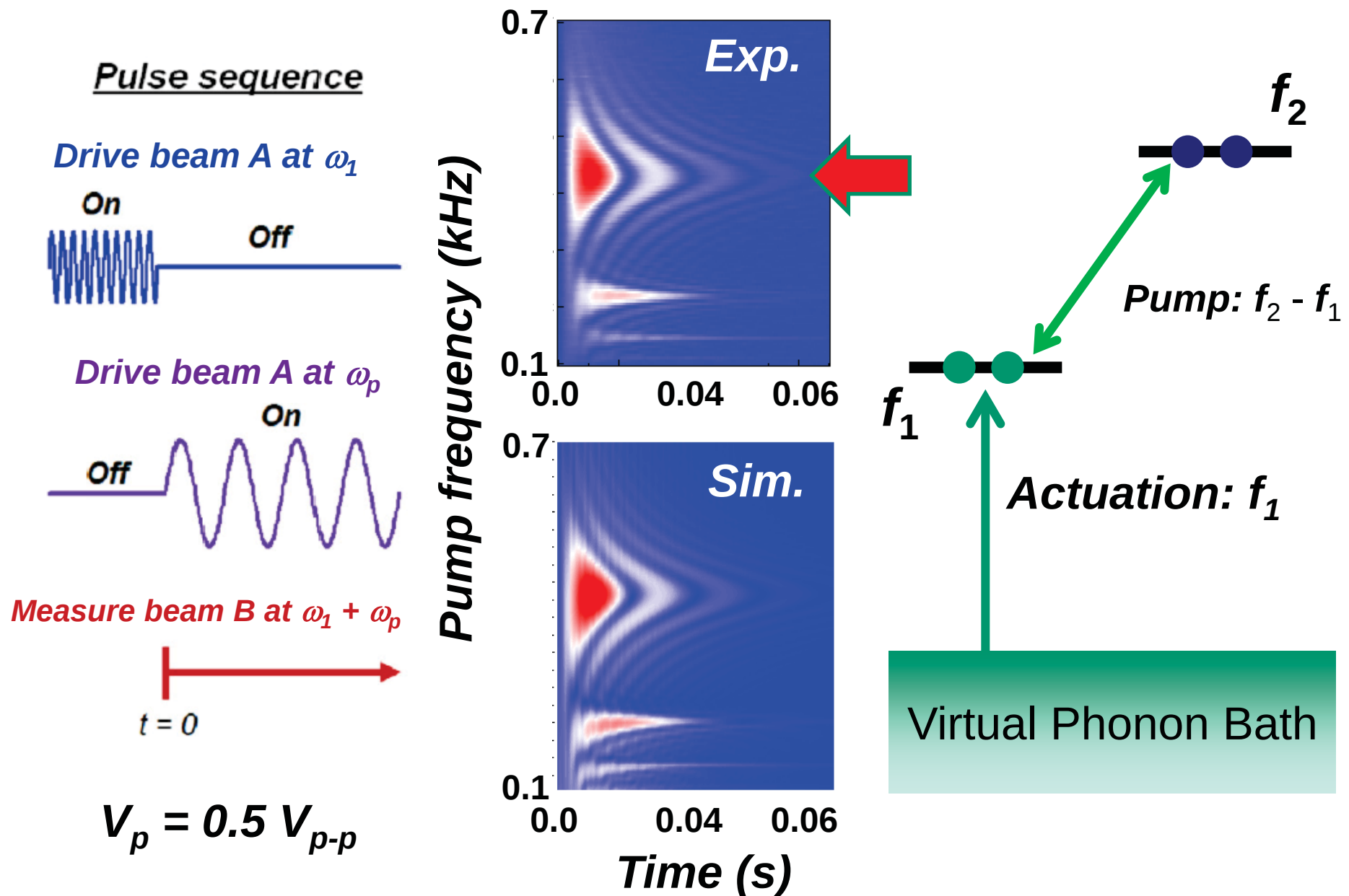
Actuation  $\rightarrow$  beam A  
Detection  $\rightarrow$  beam B



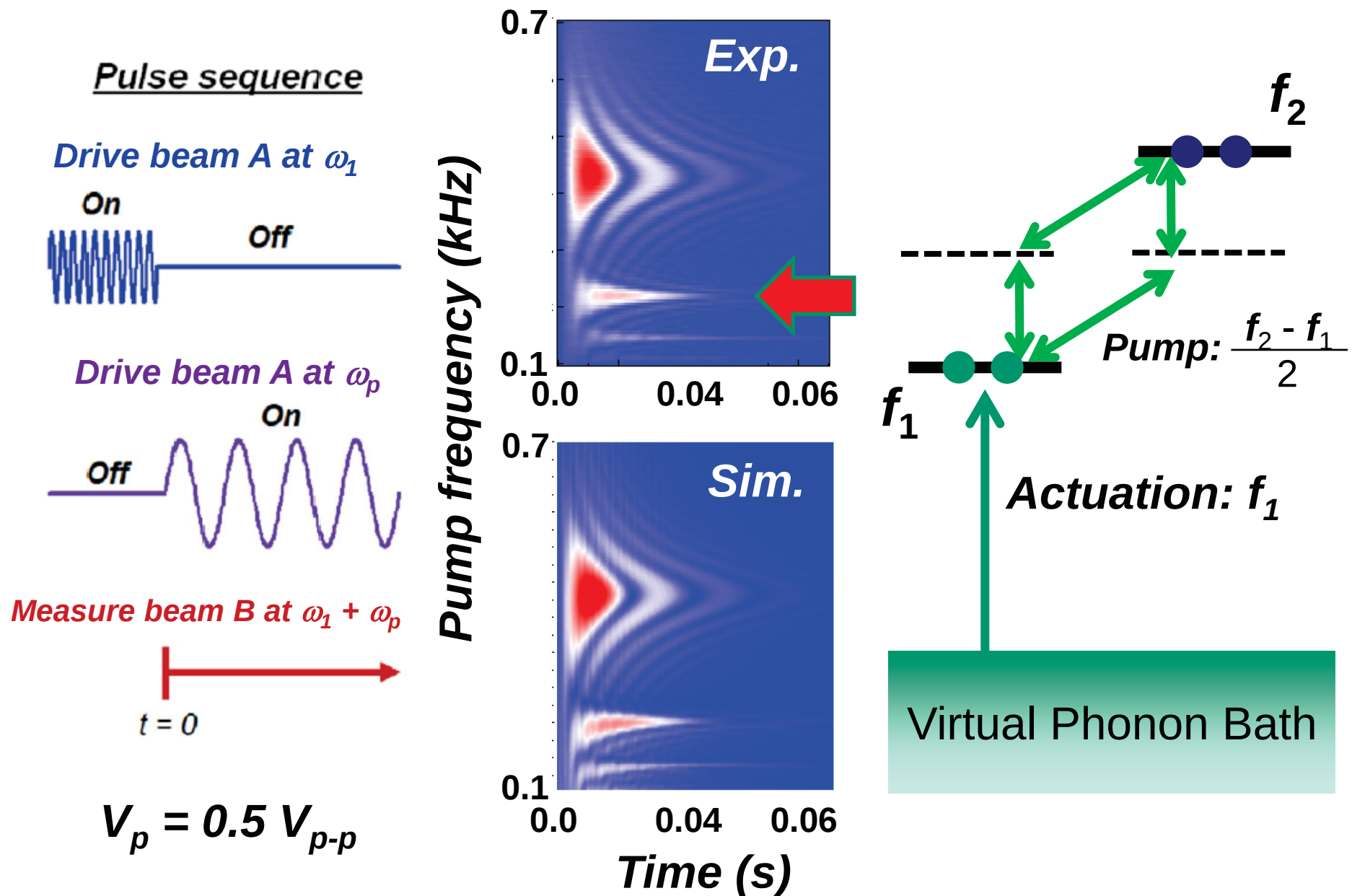
H. Yamaguchi et al., Appl. Phys. Express 5, 014001 (2012)



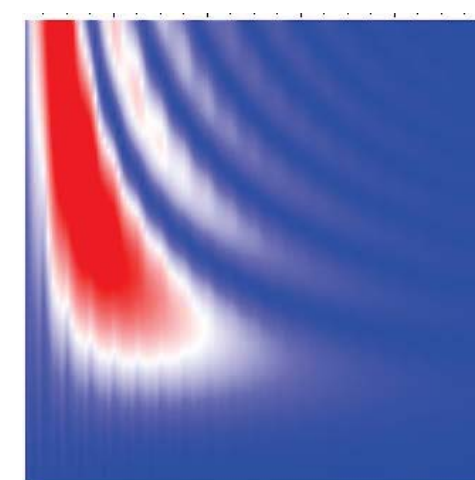
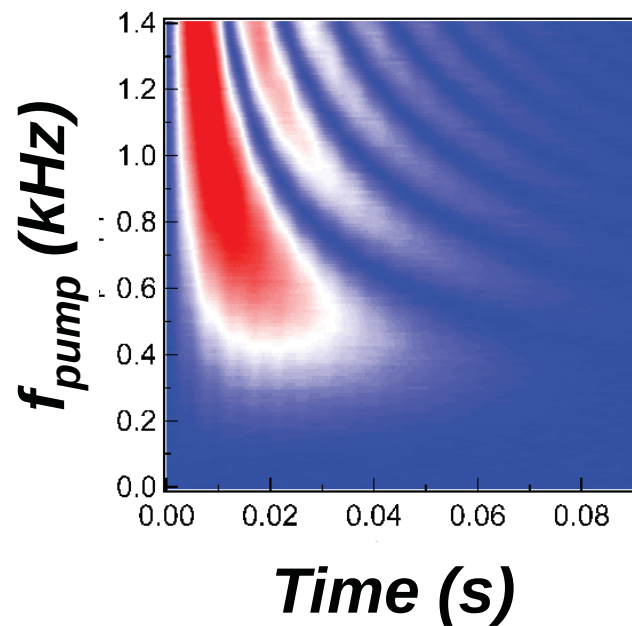
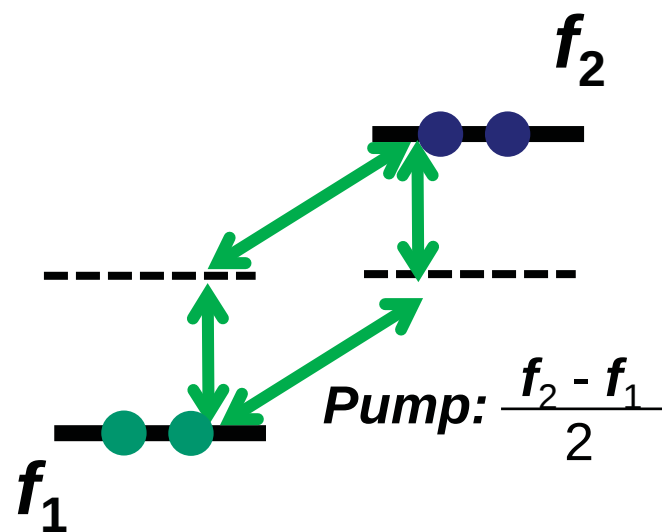
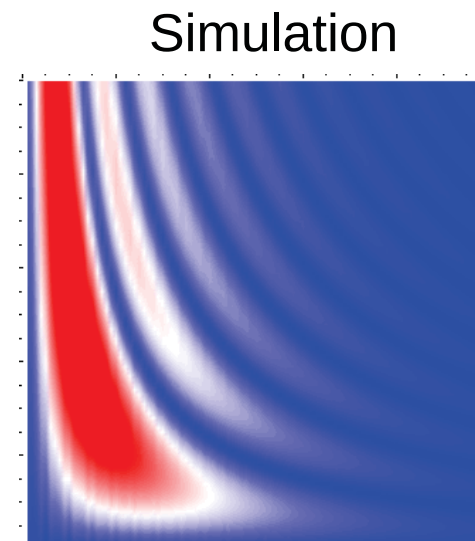
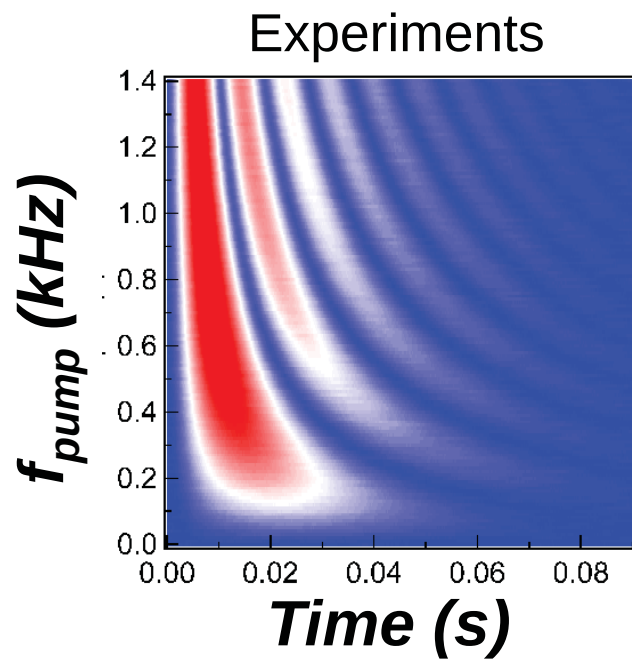
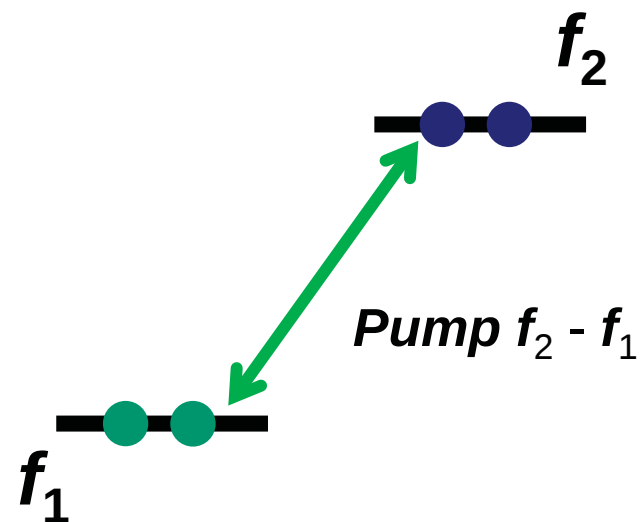
# Pump Frequency Dependence of Rabi Oscillation

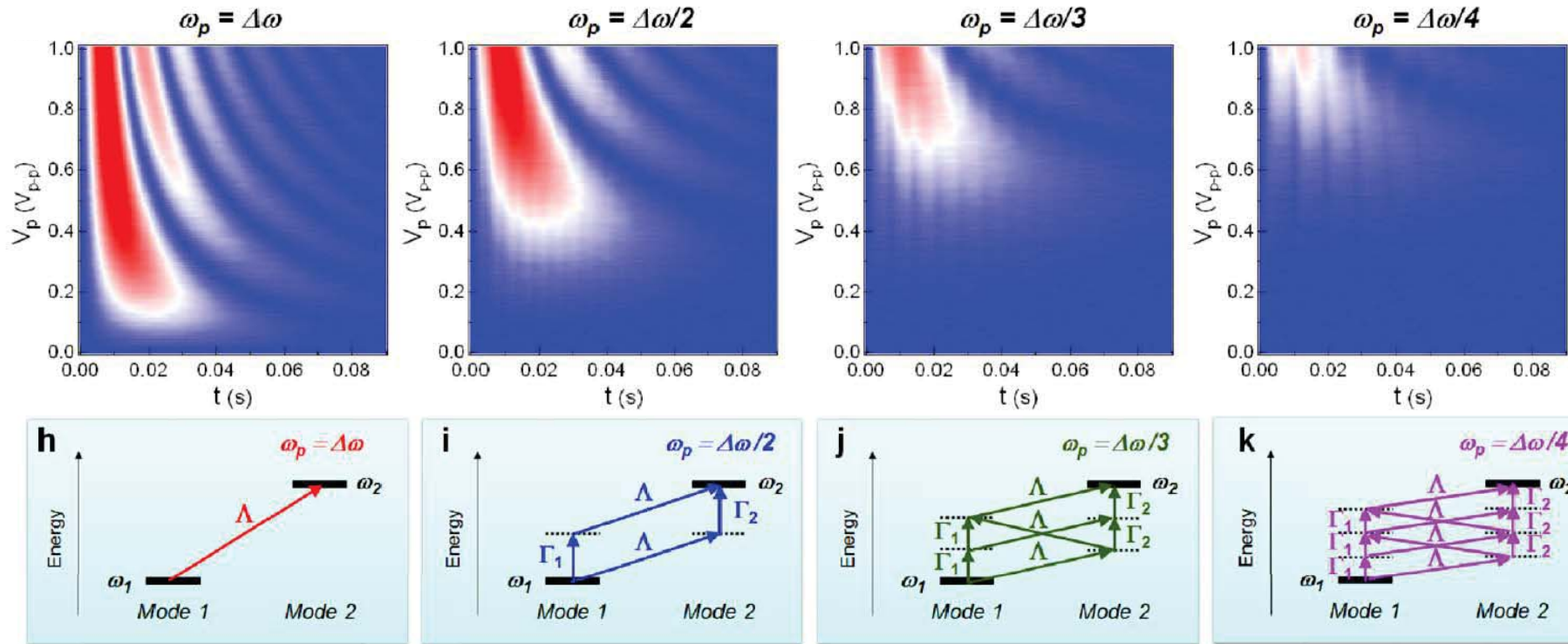


# Pump Frequency Dependence of Rabi Oscillation



# Pump Power Dependence of Rabi Oscillation





Equations of motion for **mode** variables

$$\ddot{X}_1 + \gamma \dot{X}_1 + \omega_1^2 X_1 + \Gamma_1 \cos(\omega_p t) X_1 + \Lambda \cos(\omega_p t) X_2 = U_{11} f_0 \cos(\omega t + \delta)$$

$$\ddot{X}_2 + \gamma \dot{X}_2 + \omega_2^2 X_2 + \Gamma_2 \cos(\omega_p t) X_2 + \Lambda \cos(\omega_p t) X_1 = U_{21} f_0 \cos(\omega t + \delta)$$

$$\Gamma_1 = \Gamma(1 + \omega_0 \Delta\omega / \sqrt{c^2 + \omega_0^2 \Delta\omega^2}) / 2$$

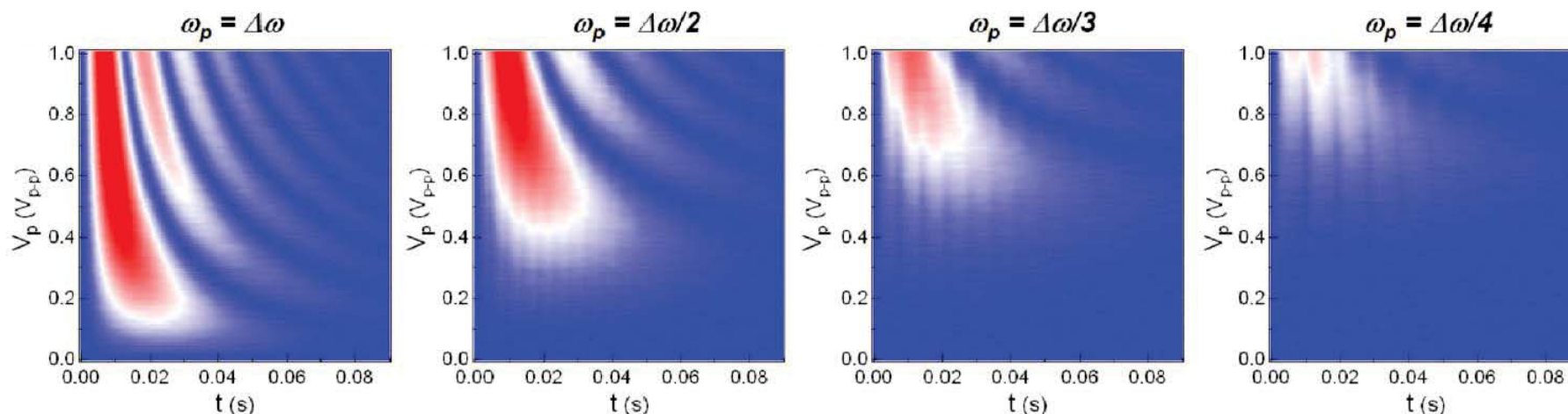
$$\Gamma_2 = \Gamma(1 - \omega_0 \Delta\omega / \sqrt{c^2 + \omega_0^2 \Delta\omega^2}) / 2$$

$$\Lambda = \Gamma c / \sqrt{c^2 + \omega_0^2 \Delta\omega^2} / 2$$

**intra**-modal coupling

**inter**-modal coupling

# Higher order coherent oscillation



$$g^{(1)} \sim \frac{\Lambda}{2\sqrt{\omega_1\omega_2}}$$

$$g^{(2)} \sim \frac{\Lambda|-\Gamma_1/\omega_1 + \Gamma_2/\omega_2|}{4(\omega_2 - \omega_1)\sqrt{\omega_1\omega_2}}$$

$$g^{(3)} \sim \frac{9\Lambda[2\Gamma_1^2/\omega_1^2 + 2\Gamma_2^2/\omega_2^2 - (4\Gamma_1\Gamma_2 + \Lambda^2)/\omega_1\omega_2]}{128(\omega_2 - \omega_1)^2\sqrt{\omega_1\omega_2}}$$

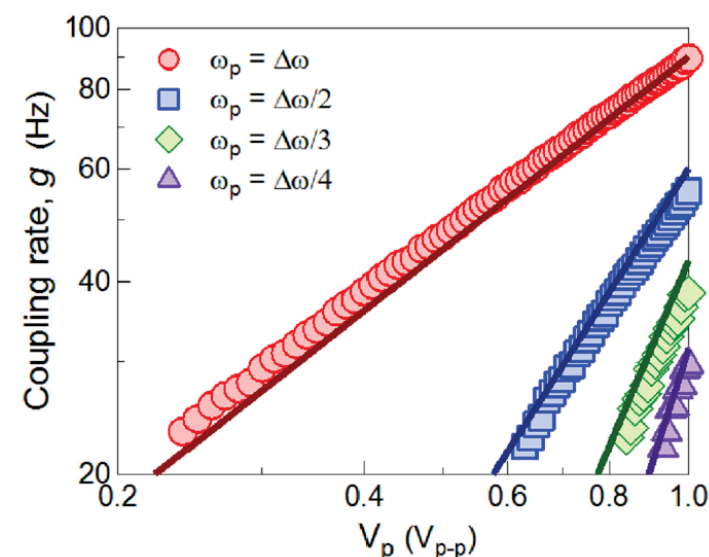
$$g^{(4)} \sim \frac{\Lambda|-3\Gamma_1^3/\omega_1^3 + 9\Gamma_1^2\Gamma_2/\omega_1^2\omega_2 + 4\Lambda^2\Gamma_1/\omega_1^2\omega_2 - 9\Gamma_1\Gamma_2^2/\omega_1\omega_2^2 - 4\Lambda^2\Gamma_2/\omega_1\omega_2^2 + 3\Gamma_2^3/\omega_2^3|}{36(\omega_2 - \omega_1)^3\sqrt{\omega_1\omega_2}}$$

$$\Gamma_1 = \Gamma(1 + \omega_0\Delta\omega/\sqrt{c^2 + \omega_0^2\Delta\omega^2})/2$$

$$\Gamma_2 = \Gamma(1 - \omega_0\Delta\omega/\sqrt{c^2 + \omega_0^2\Delta\omega^2})/2$$

$$\Lambda = \Gamma c/\sqrt{c^2 + \omega_0^2\Delta\omega^2}/2$$

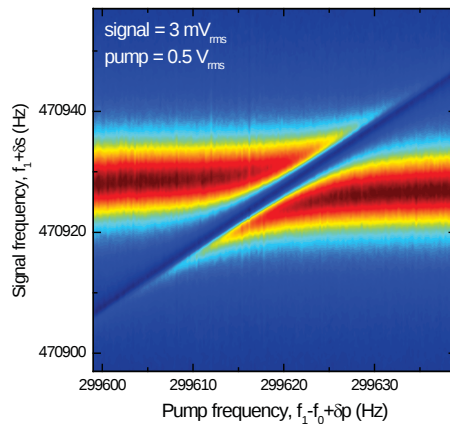
*good agreement with  
no fitting parameter !*



## ✓ Piezoelectric transduction in a GaAs/AlGaAs parametric resonator



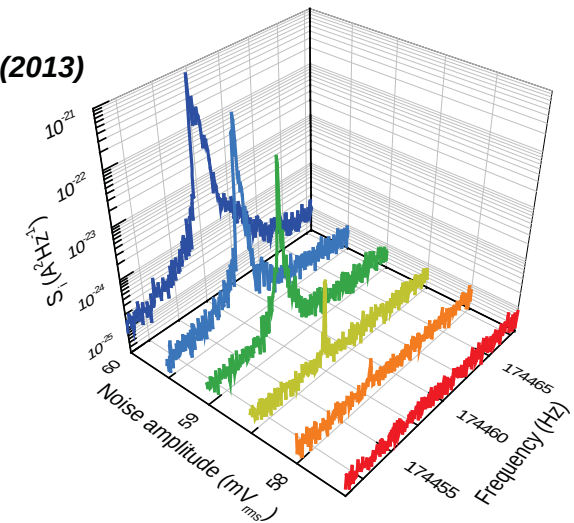
I. Mahboob and H. Yamaguchi, *Nature Nanotechnology* 3, 275 (2008)



## ✓ Mechanical two-mode systems and tension-induced strong coupling

I. Mahboob, et al. *Nature Phys.* 8, 387 (2012)

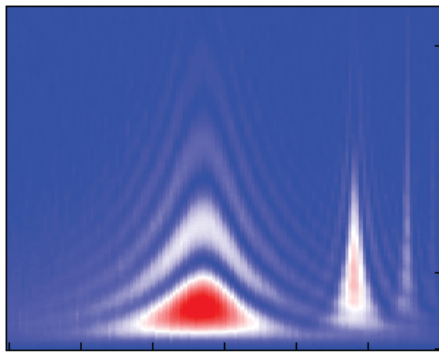
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