

# Mixing in Oceans and Seas

W.G. Large

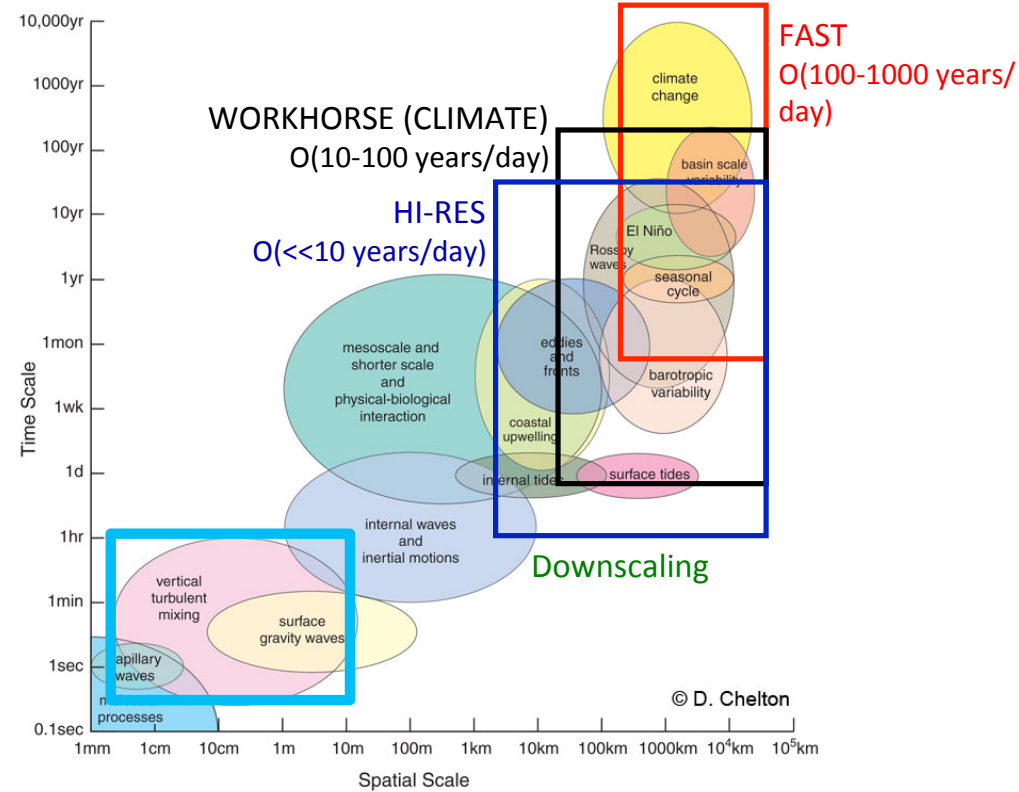
Climate and Global Dynamics Laboratory  
National Center for Atmospheric Research  
Boulder, Colorado  
([wily@ucar.edu](mailto:wily@ucar.edu))

Ocean Climate Modelling:  
**Physical** and biogeochemical **dynamics** of semi-enclosed **seas**.

METU Campus, Ankara, September 2015

# Ocean Modeling Challenges

## Space – Time Scales and Global Ocean Models



# Outline

1. **Non-linear mixing**
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
4. The Surface Boundary Layer & Similarity Theory
5. The Convective Boundary Layer

---

6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. A Practical Example: Diurnal Cycling

Non-linear terms of Navier-Stokes Equations →  
[3-dimensional flow;  $\underline{U} = (U, V, W) = U_i, i=1,3$ ]

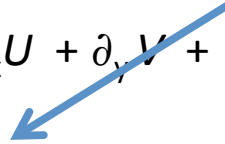
$$\partial_t U_i = - U \partial_x U_i - V \partial_y U_i - W \partial_z U_i$$

$$= - \underline{U} \cdot \nabla U_i$$

$$= - \partial_x (U U_i) - \partial_y (V U_i) - \partial_z (W U_i) \quad (\text{flux form})$$

$$+ U_i [ \partial_x U + \partial_y V + \partial_z W ]$$

0 (continuity, incompressible)



## Reynolds' Decomposition (Mean + Fluctuation)

For any state variable:  $Q = \{U, V, W, T, S, P, \rho(T, S, P)\}$

$$Q = \bar{Q} + q \quad : \quad \langle Q \rangle = \bar{Q} ; \quad \langle q \rangle = 0$$

= Mean + fluctuation

$$\begin{aligned} \text{Products : e.g. } (WQ) &= (W + w)(Q + q) \\ &= (WQ) + wQ + Wq + wq \end{aligned}$$

$$\text{Average} \quad \langle WQ \rangle = (WQ) + \langle wq \rangle$$

(eddy fluxes)

## Navier-Stokes Equations → Primitive Equations

Consider mean, U - momentum equation:  $\partial_t U =$

$- U \partial_x U - V \partial_y U - W \partial_z U$ , Advection (non-linear)

$+ f V$ , Coriolis (earth's rotation)

$- \partial_x P / \rho$ , Pressure gradient

$- \partial_z \langle wu \rangle$ , Turbulent vertical mixing (NL)

$- \partial_z \langle uu \rangle - \partial_z \langle vu \rangle$ , Lateral mixing (NL)

$+ \nu_m \partial_{zz} U$ , Molecular viscosity (Damping)

## Numerical Model Decomposition:

$Q = \text{Resolved} + \text{Unresolved (sub-grid-scale)}$

$$Q = \bar{Q} + q$$

Use of same equations implicitly assumes equivalence to Reynolds' Mean + fluctuation decomposition

BUT in general  $\langle \text{Unresolved}, q \rangle \neq 0$

Questions: What about  $\langle wQ \rangle$  and  $\langle Wq \rangle$  terms ?

Is  $\langle w \rangle$  in upwelling regions identically zero ?

## Outline

1. Non-linear mixing

### **2. Turbulent Eddy Viscosity and Closures**

3. Mixing Regimes in Oceans and Seas

4. The Surface Boundary Layer & Similarity Theory

5. The Convective Boundary Layer

6. Modeling the Surface Boundary Layer

--- Mixed Layer Models

--- First Order Closures

7. The Viscous Surface Layer

8. A Practical Example: Diurnal Cycling



## Eddy Viscosity :

Reynolds' Stress Tensor,  $\underline{\sigma}$

$$\sigma_{ij} = -\langle u_i u_j \rangle = -\frac{1}{3} \delta_{ij} \langle u_k u_k \rangle + d_{ij}$$

Eddy viscosity is a **parameterization** of the deviatoric component,  $d_{ij}$ ,

in terms of resolved shear  $e_{kl} = \frac{1}{2} [\nabla_k U_l + \nabla_l U_k]$  :

$$d_{ij} = T_{ijkl} e_{kl}, \text{ where } T_{ijkl} \text{ is a } 3^4 = 81 \text{ element tensor}$$

Symmetries  $T_{ijkl} = T_{jikl} = T_{ijlk} = T_{klij}$  leave only 21 independent

## Eddy Viscosity in Ocean Models :

Usually specify only two viscosities: a vertical,  $K_u$   
a horizontal (lateral),  $v_H$

Some specify three :

- a vertical  $K_u$
- a downstream lateral,  $A_H$
- a cross-stream lateral,  $B_H$

$$T_{1111} = T_{2222} = 2 v_H = A_H + B_H$$

$$T_{3333} = K_u + v_H = K_u + A_H$$

$$T_{1212} = v_H = B_H$$

$$T_{1313} = T_{2323} = K_u = K_u$$

$$T_{1133} = T_{2233} = v_H - K_u = B_H - K_u$$

Large , et. al., 2001, J. Phys. Oceanogr.)

## Cartesian Constant Coefficients, $A_H$ & $B_H$

$$\partial_t U = -\partial_x \langle uu \rangle - \partial_y \langle vu \rangle - \partial_z \langle wu \rangle + \dots$$

$$= A_H \partial_{xx} U + B_H \partial_{yy} U + K_u \partial_{zz} U + \dots$$

$$\partial_t V = -\partial_x \langle uv \rangle - \partial_y \langle vv \rangle - \partial_z \langle wv \rangle + \dots$$

$$= B_H \partial_{xx} V + A_H \partial_{yy} V + K_u \partial_{zz} V + \dots$$

Low  $B_H$  allows currents to grow  
High  $A_H$  keeps numerics stable

## Turbulence Closures :

The order ( $n^{\text{th}}$ ) of a turbulence closure is given by the moment (  $n^{\text{th}}$  ) of the highest prognostic equation

$$\partial_t U = - \partial_z \langle wu \rangle \quad \text{U is a 1}^{\text{st}} \text{ moment; 1}^{\text{st}} \text{ order)}$$

$$\partial_t \langle uw \rangle = \text{terms with 3}^{\text{rd}} \text{ moments (e.g. } \langle uwq \rangle \text{)} \quad (2^{\text{nd}} \text{ order)}$$

$$\partial_t \langle uwx \rangle = \text{terms with 4}^{\text{th}} \text{ moments (e.g. } \langle uwq^2 \rangle \text{)} \quad (3^{\text{rd}} \text{ order)}$$

..... And so on and so on and so on .....

## The Fundamental Problem of Turbulence :

Consider a system of  $Q = \{ U, W, T \}$  :

Order	1 <sup>st</sup>	2 <sup>nd</sup>	3 <sup>rd</sup>	4 <sup>th</sup> ....
Unknowns	U W T	uu ww tt uw ut wt	uuu www ttt uuw uut uwt utt uww wwt wtt	$N_4 > 10$

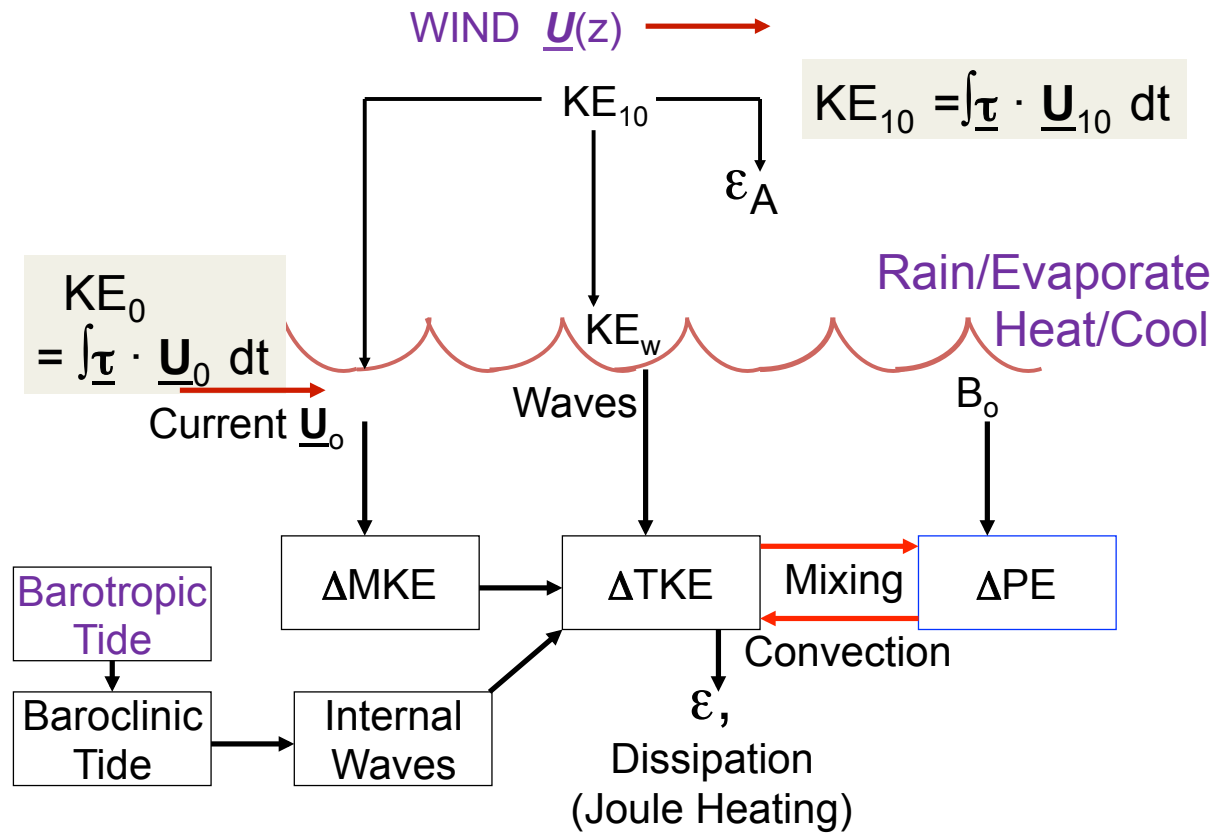
	Equations	Unknowns	Excess Unknowns
1 <sup>st</sup> order	3	$3+6 = 9$	6
2 <sup>nd</sup> order	9	$9+10 = 19$	10
3 <sup>rd</sup> order	19	$19 + N_4$	$N_4 > 10$

As the order of the closure (number of prognostic equations) increases the number of unknowns increases faster and solutions don't converge.

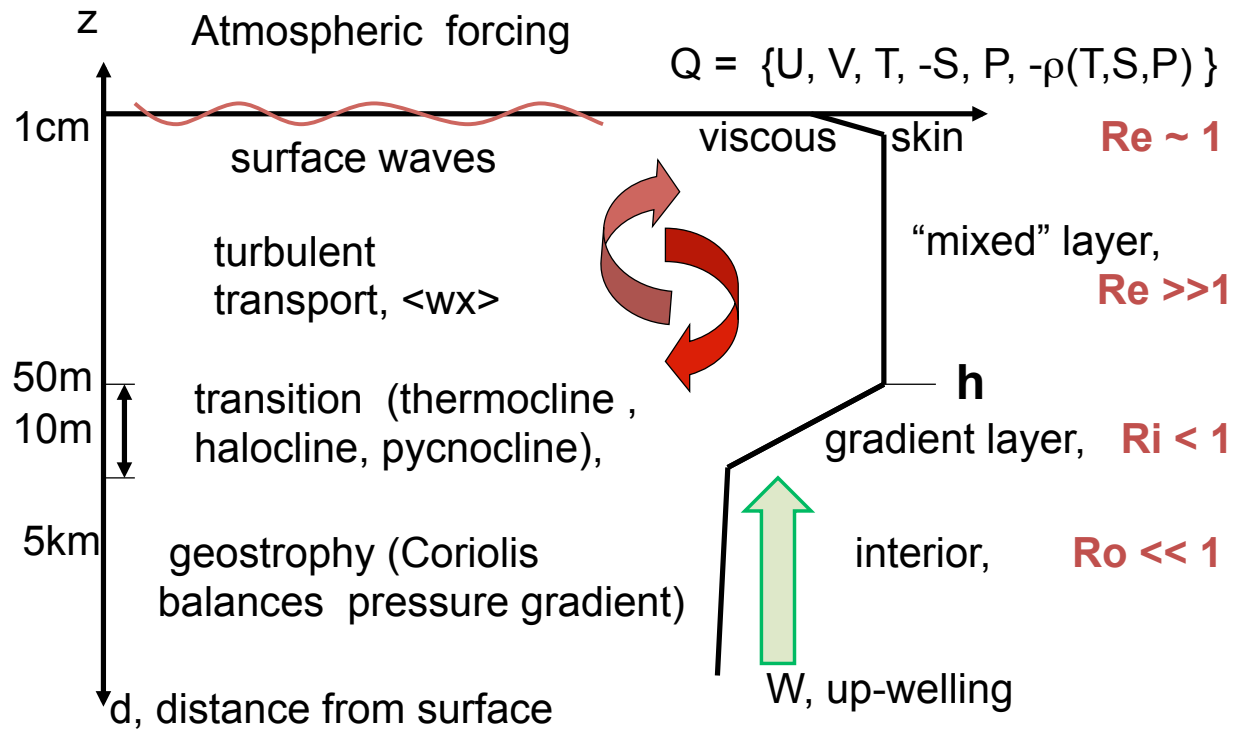
## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
- 3. Mixing Regimes in Oceans and Seas**
4. The Surface Boundary Layer & Similarity Theory
5. The Convective Boundary Layer
6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. A Practical Example: Diurnal Cycling

## Mixing Energetics (Sources)



## Turbulent Mixing Regimes (changing balance of terms with, $d$ )





## Interior ( small Rossby Number)

$$\text{Rossby Number, } Ro = \frac{\text{non-linear}}{\text{Coriolis}} = \frac{U}{f d},$$

Where  $f = 2 \Omega \sin(\text{latitude})$  is the vertical Coriolis parameter  
 $\approx 10^{-4} \text{ s}^{-1}$

Therefore , far from the boundary there will be a geophysical fluid interior , characterized by  $Ro \ll 1$  :

$$\text{geostrophic flow} \implies [ f U = - \partial_y P / \rho ; f V = \partial_x P / \rho ]$$

$$\begin{aligned} \text{Vertical velocity given by continuity : } \partial_z W &= - [ \partial_x U + \partial_y V ] \\ W(\text{bottom}) &= 0 \end{aligned}$$

$$\text{Pressure, } P = \int_{-d}^0 \rho(T,S,P) dz$$

## Interior (Vertical) Mixing

Viscosity,  $K_u$        $Pr = \frac{\text{Viscosity}}{\text{Diffusivity}}$

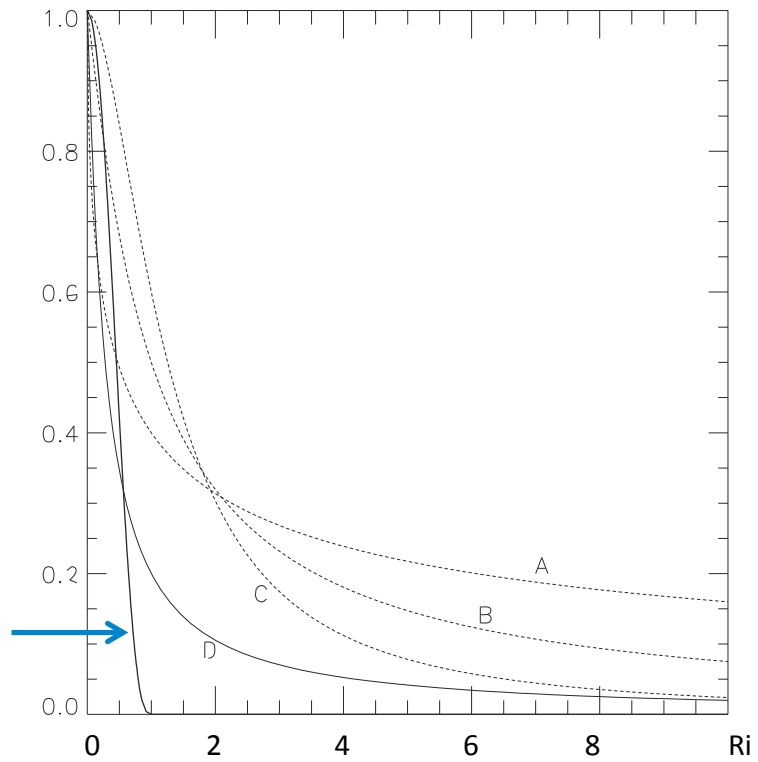
- Dynamic instability (K-H)       $K_o^{sh} f(Ri)$       1
- Double diffusion instability       $K_q^{dd}(R_\rho)$       1
- Internal wave breaking       $K_o^{iw}$       10
- Tidal Energy (Bryan and Lewis, JGR, 1979)  
(Simmons et. al., Ocn. Mod. 2004)

$$K_o^{iw} = 1 \text{ cm}^2/\text{s} \quad ; \quad K_o^{sh} = 50 \text{ cm}^2/\text{s} \quad ; \quad K_q^{dd}(R_\rho) < 5 \text{ cm}^2/\text{s}$$

## Functions of $Ri$ , $f(Ri)$

Equatorial Undercurrent  
Pacanowski-Philander, 81

$$K_v = .1 + 50(\text{cm}^2/\text{s}) f(Ri)$$



## Low Richardson Number, $Ri < 1$

Stratified Shear Flow : Buoyancy  $B(z) = -g \rho(z) / \rho_0$  [m/s<sup>2</sup>]

Stratification gives Buoyancy Frequency,  $N$ ,  $N^2 = \partial_z B > 0$  [s<sup>-2</sup>]

Shear is  $\partial_z \mathbf{V}$  [s<sup>-1</sup>] for  $\mathbf{V} = (U, V)$ , high shear is unstable  
lots of kinetic energy, KE

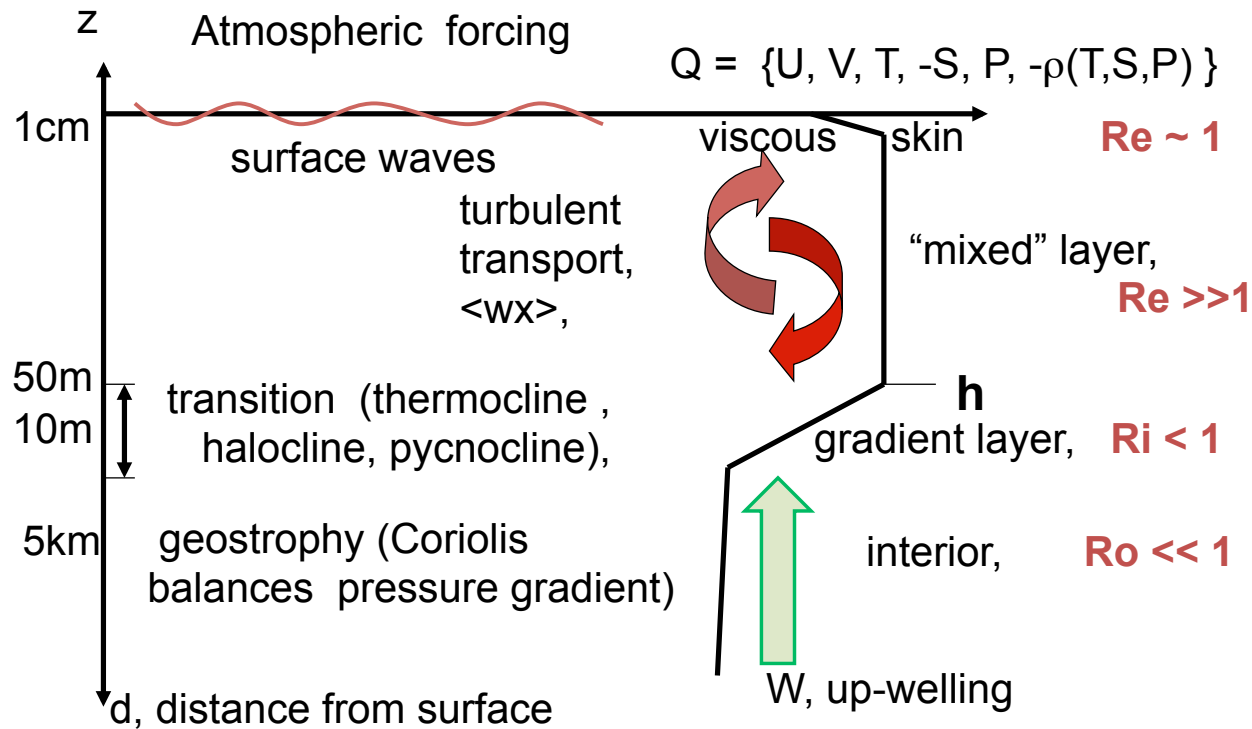
High stratification means stable (negative) potential energy, PE

$$Ri = \frac{N^2}{(\partial_z \mathbf{V})^2} = \frac{\text{stable PE}}{\text{available KE}} < 0.25 \quad \text{==> local turbulent mixing (K-H) (Kelvin-Helmholtz)}$$

(empirical)

NON - DIMENSIONAL

## Turbulent Mixing Regimes (changing balance of terms with, d)

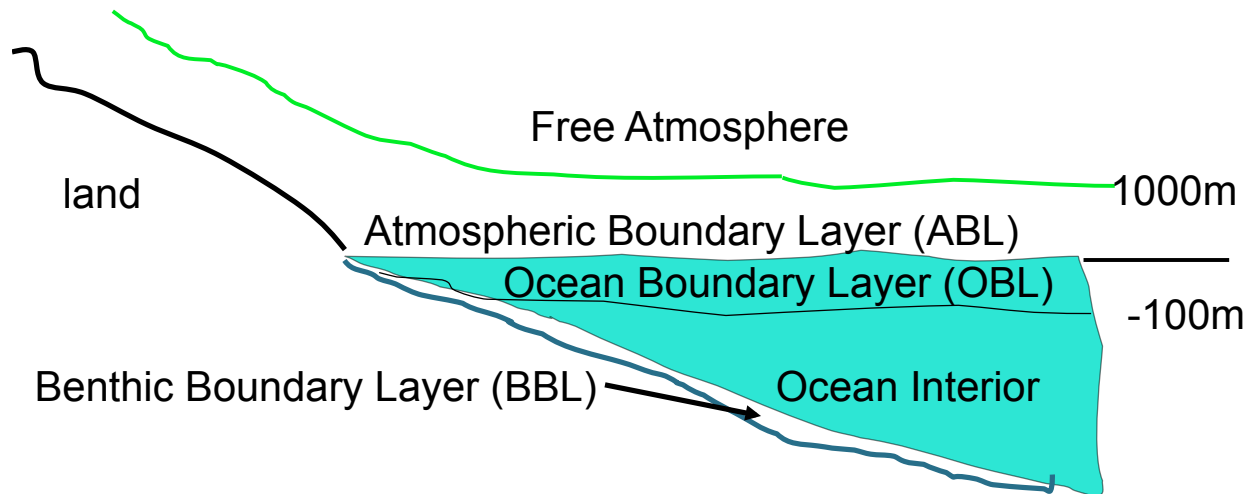


## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
- 4. The Surface Boundary Layer & Similarity Theory**
5. The Convective Boundary Layer
6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. A Practical Example: Diurnal Cycling

## The Sea Surface Boundary Layer

- The portion of an ocean or sea that is directly influenced (forced) by the boundary
- Geophysical fluids “feel” the earth’s rotation,  $\Omega = 7.3 \times 10^{-5} \text{ s}^{-1}$



The free atmosphere and ocean interior connect through the OBL and ABL

## Turbulent Surface Forcing

Wind Stress,  $\underline{\tau}_o = (\tau_x, \tau_y)_o$

Freshwater flux,  $F_o =$   
 $P$  , Precipitation,  $> 0$   
 $+ E$  , Evaporation, usually  $< 0$   
 $+ M$  , Melt; Sea-ice. Ice-bergs

Surface heat flux,  $Q_o$   
 $= Q_{\text{nsol}}$  , non-solar heat fluxes  $< 0$   
 $+ SW_{\text{net}}(0)$  , net surface solar radiation  $> 0$   
 $- SW_{\text{net}}(d_s)$  , solar not driving the OBL

In limit of  $d_s = 0$ , solar radiation does not drive OBL,  
 Clearly  $d_s$  should not be beyond the OBL



### 3) Surface Kinematic Fluxes

$$| \langle \mathbf{v} w \rangle_o | = | \tau_o | / \rho_o = u^* u^* = u^{*2}$$

$$\langle w t \rangle_o = - Q_o / (\rho_o C_p) = u^* t^*$$

$$\langle w s \rangle_o = F_o S_o / \rho_o = u^* s^*$$

Surface buoyancy flux  $B_o = -g ( \alpha \langle w t \rangle_o - \beta \langle w s \rangle_o )$

$$\alpha = (2 \rightarrow 4) \times 10^{-4} \text{ } ^\circ\text{C}^{-1} ; \quad \beta = 3.5 \times 10^{-4} (\text{psu})^{-1}$$

Monin-Obukhov Length,  $L = u^{*3} / (\kappa B_o) ; \quad < 0 \text{ unstable}$

Depth where wind power ( = Force x Velocity =  $u^{*3}$  )  
equals PE loss (gain) due to  $B_o > 0$  ( $B_o < 0$ ) =  $\kappa B_o L$

### 3) Monin-Obukhov Similarity Theory

Near the surface of a boundary layer, but away from the surface roughness elements, the ONLY important turbulence parameters are the distance,  $d$ , and the surface kinematic fluxes.

$$| \langle \mathbf{v} w \rangle_o | = | \boldsymbol{\tau}_o | / \rho_o = u^* \mathbf{u}^* = u^{*2}$$

$$\langle w t \rangle_o = - Q_o / (\rho_o C_p) = u^* t^*$$

$$\langle w s \rangle_o = F_o S_o / \rho_o = u^* s^*$$

Monin-Obukhov Length,  $L = u^{*3} / (\kappa B_o)$  ;  $< 0$  unstable

Depth where wind power ( = Force x Velocity =  $\kappa u^{*3}$  )  
equals PE loss (gain) due to  $B_o > 0$  ( $B_o < 0$ ) =  $B_o L$

### 3) Monin-Obukhov Similarity Theory

Near the surface of a boundary layer, but away from the surface roughness elements, the ONLY important turbulence parameters are the distance,  $d$ , and the surface kinematic fluxes.

KEY : Dimensional Analysis

5 parameters ( $u^*$ ,  $t^*$ ,  $s^*$ ,  $d$ ,  $L$ )

4 units (m, s, °K, psu)

Non-dimensional groups are functions of  $(d/L)$ ,  
the stability parameter ( $< 0$ , unstable)

### 3) Dimensional Analysis ( $d = -z$ )

Non-dimensional gradients :  $-\partial_z Q \ d / q^* \propto \phi_q(d/L)$ ,

Empirically  $\kappa = 0.4$ , von Karman constant ,  
makes  $\phi_q(0) = 1$  in neutral (wind only) forcing ( $B_o = 0$ ,  $L \rightarrow \infty$  )

$\kappa \partial_z Q = q^* / z \rightarrow$  neutral logarithmic profiles,  $Q(z)$

Let :  $\langle w q \rangle_o = u^* q^* = -K_q \partial_z Q$  , defines diffusivity,  $K_q$

Near the surface of a PBL similarity theory (MOS) says

$$K_q \rightarrow - \frac{u^* x^*}{\partial_z Q} = \frac{\kappa d u^*}{\phi_q(d/L)} \rightarrow \kappa u^* d \quad \text{neutral}$$

## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
4. The Surface Boundary Layer & Similarity Theory
- 5. The Convective Boundary Layer**
6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. A Practical Example: Diurnal Cycling

## The convective SBL ( $B_o < 0$ )

Surface buoyancy flux,  $B_o = -\langle wb \rangle_o < 0$

Wind stress,  $\tau_o = 0$  ;  $u^* = 0$

Convective Velocity Scale ,  $w^* = (-B_o h)^{1/3}$  ,

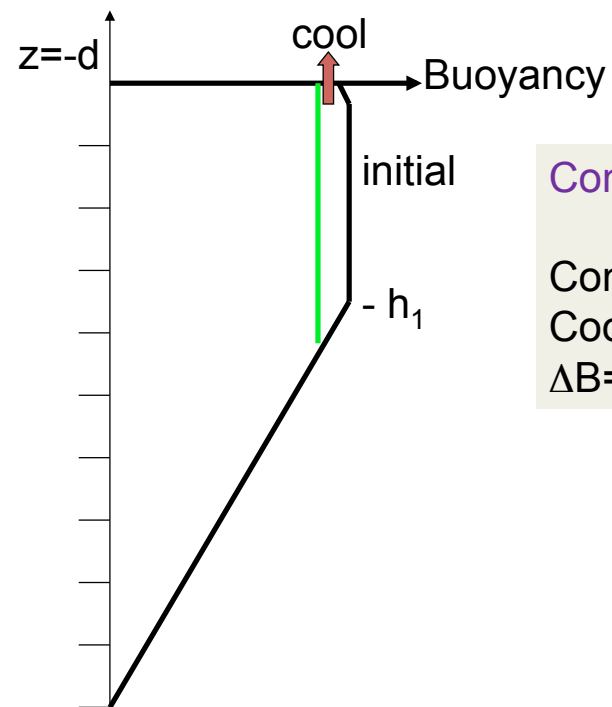
Where h is boundary layer depth :  $\sigma = d / h$

$$d/L = \kappa d B_o / u^{*3} \rightarrow -\infty$$

$$\phi_q(d/L) \rightarrow (1 - c d/L)^{-1/3} = (1 - c \sigma h/L)^{-1/3}$$

$$w_q = u^* / \phi_q \rightarrow (u^{*3} - c \kappa d B_o)^{1/3} \rightarrow (c \kappa \sigma)^{1/3} w^*$$

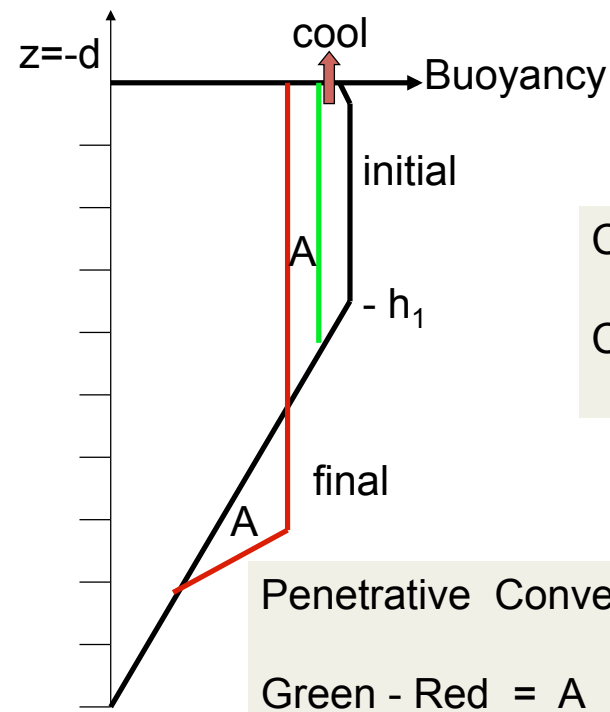
## Simple Cooling (Buoyancy Loss)



### Convective Adjustment

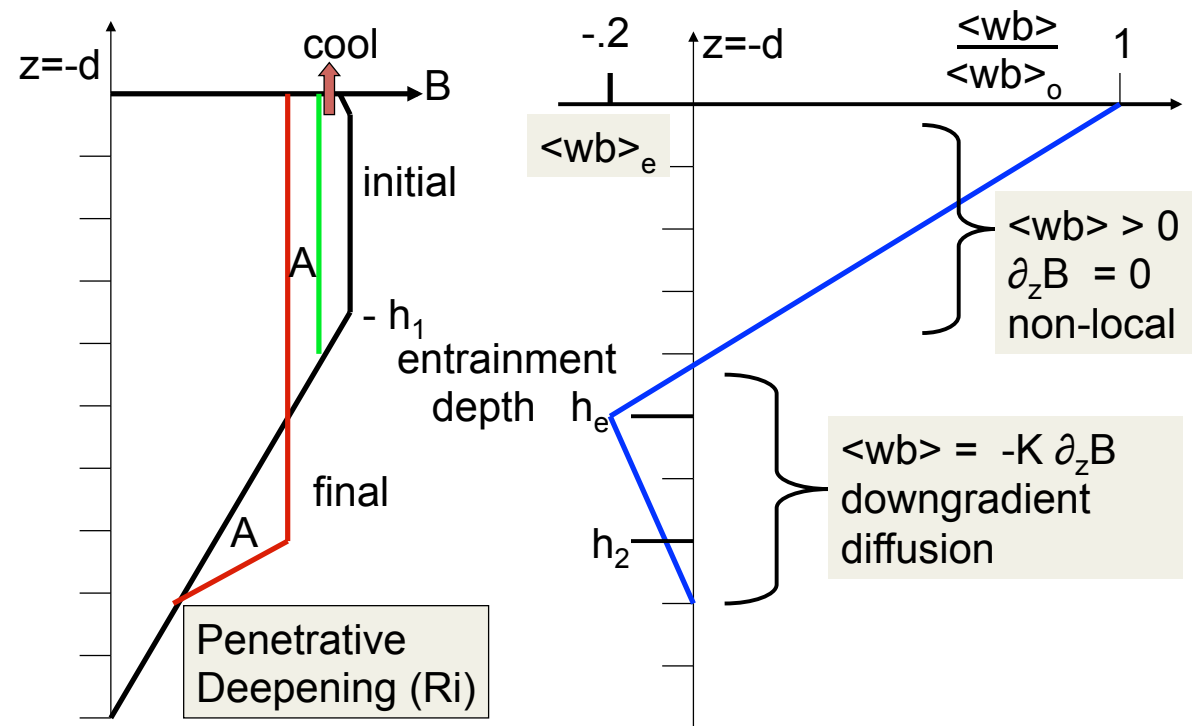
Conservation :  
Cool = Initial-Green  
 $\Delta B = \Delta t \partial_z - \langle wb \rangle$

## Penetrative Convection





## Convective SBL Turbulent Fluxes:



Questions ?

## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
4. The Surface Boundary Layer & Similarity Theory
5. The Convective Boundary Layer
- 6. Modeling the Surface Boundary Layer**
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. A Practical Example: Diurnal Cycling

## Modeling the SBL

Solve 1<sup>st</sup> order conservation equations  
(prognostic variables are 1<sup>st</sup> moments, or means)

$$\text{1-D in vertical : } \partial_t T = -\partial_z \langle wT \rangle \quad ; \quad \partial_t S = -\partial_z \langle wS \rangle$$

$$\partial_t U = -f V - \partial_z \langle wU \rangle \quad ; \quad \partial_t V = f U - \partial_z \langle wV \rangle$$

The surface boundary conditions are the kinematic fluxes

$$\text{Linearize density, } \rho = \rho_o ( 1 - \alpha ( T - T_o ) + \beta ( S - S_o ) )$$

$$\text{e.g. } \rho_o = 1025 \text{ kg/m}^3 \quad ; \quad T_o = 17 \text{ C} \quad ; \quad S_o = 36 \text{ psu}$$

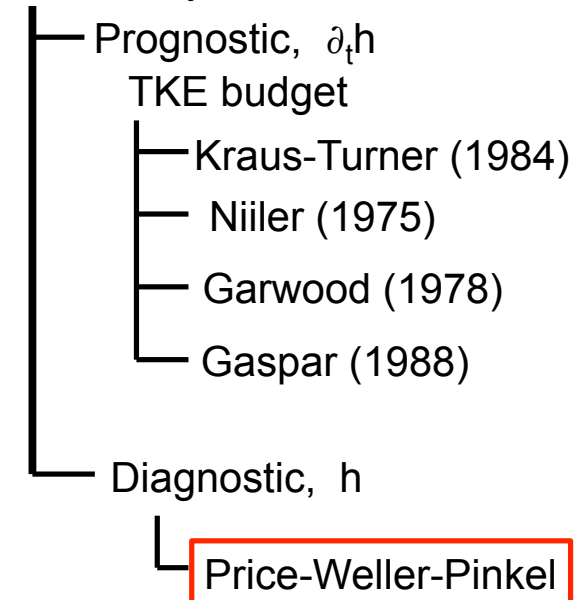
$$\alpha = .00023 \text{ C}^{-1} \quad ; \quad \beta = .00075 \text{ psu}^{-1}$$

How to solve a system of 4 equations in 8 unknowns ???????

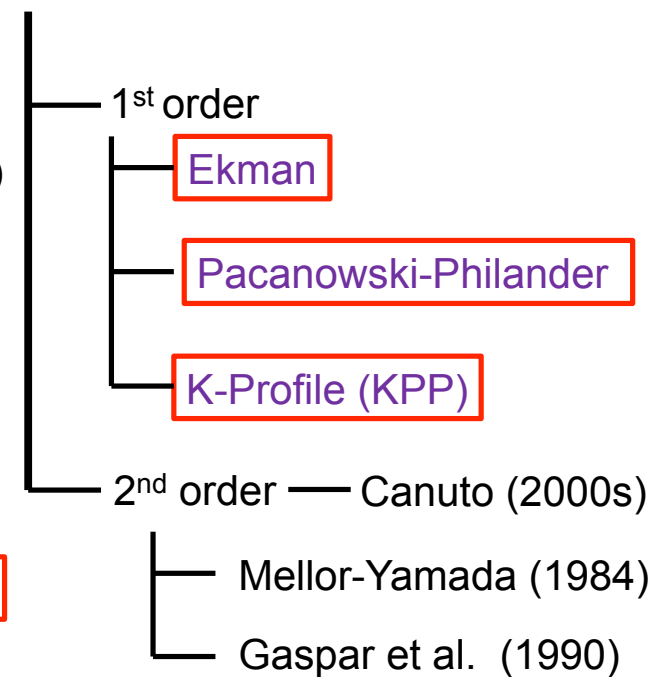
Poorly constrained, therefore many options !!!!!!!

## SBL Models/Schemes

### Mixed-Layer Models



### Turbulence Closure Models



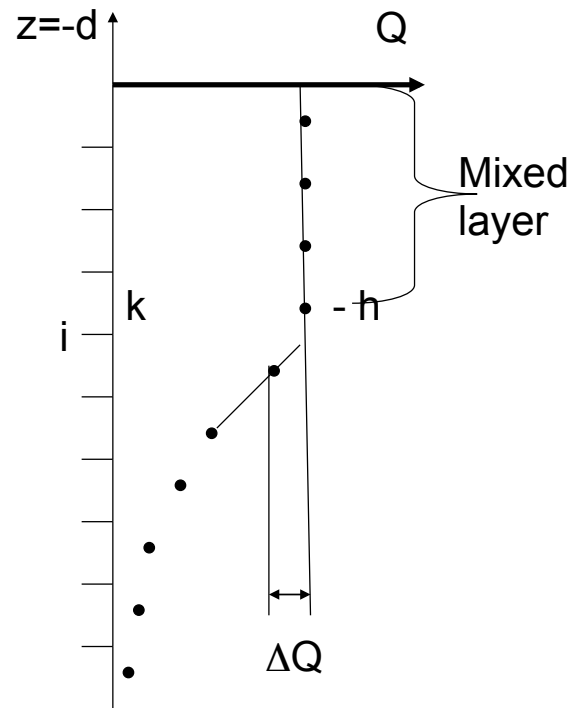
## Mixed - Layer Models

ASSUME : a well mixed, homogenous, layer of depth,  $h$   
diagnose or compute evolution of  $h$  with time

ISSUES :

- boundary layers are not homogenous (skin, transition, MOS)
- the implicit diffusivity is infinite, contrary to MOS
- discontinuities in  $Q$  or  $\partial_z Q$  at  $h$  that are not observed
- parameters are not always found to be universal

## Price-Weller-Pinkel (1986)



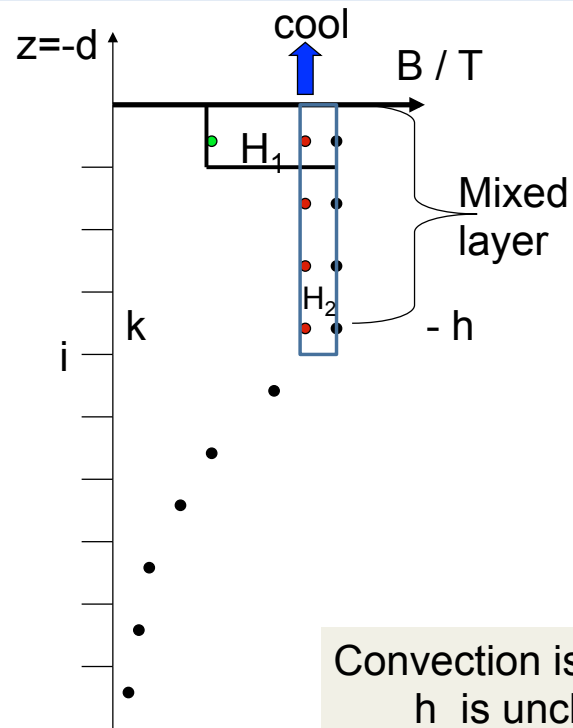
Turbulent fluxes across interfaces,  $i$ , are diagnosed to change grid point values  $Q_k$  to satisfy 3 stability criteria

A)  $\partial_z \rho < 0$  , static stability

B)  $Ri_b = \frac{g \Delta \rho h}{\rho_o |\Delta \mathbf{V}|^2} > 0.6$  "tuned"

C)  $Ri_g = \frac{N^2}{(\partial_z \mathbf{V})^2} > 0.25$

## PWP Convection

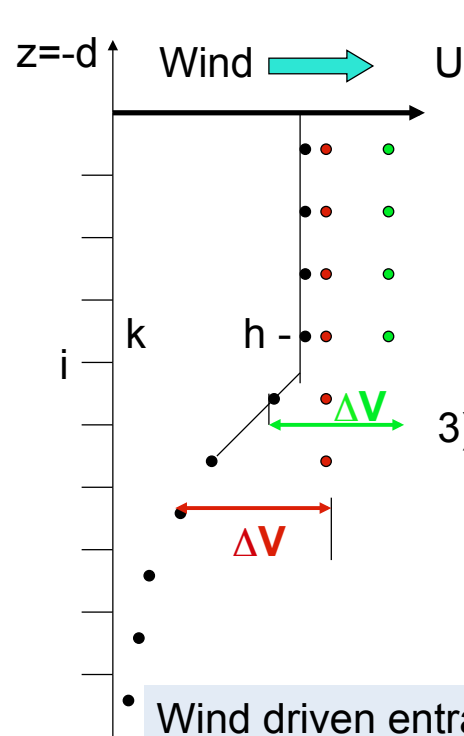


- 1) From initial (black) profile
- 2) Remove Heat (Buoyancy) equivalent to area  $H_1$  from upper layer (green) .
- 3) "Mix" to final profile (red) such that area  $H_2 = H_1$  and  
A)  $\partial_z \rho < 0$  , is satisfied

Convection is non-penetrative  
h is unchanged !!!



## PWP Entrainment



1) From initial profile (black).  
distribute momentum uniformly  
across mixed-layer (green).

2) "Mix" until profile satisfies

$$B) R_b = \frac{g \Delta \rho h}{\rho_0 |\Delta \mathbf{V}|^2} > 0.6$$

3) As  $h$  increases so does  $\Delta B$  ( $\Delta T$ ),  
but any large "jumps" are smoothed by

$$(C) R_g = \frac{N^2}{(\partial_z \mathbf{V})^2} > 0.25$$

Wind driven entrainment can be penetrative,  $h$  increases !

### Ekman 1<sup>st</sup> order closure (local):

ASSUME : analogy to molecular diffusion  $\langle wq \rangle = -K_v \partial_z X$

:  $K_v = \text{CONSTANT}$

: Produces Ekman Transport and distribution (Spiral)

BUT non-zero scalar fluxes are **observed** in regions of zero local gradient.

Therefore, the analogy is known to be wrong for scalars in a PBL, and can't be corrected by any choice of constant  $K_v$ , but may be good enough for some dynamic problems.

## Pakanowski -- Philander (1<sup>st</sup> order local)

$$\langle wq \rangle = -K_V \partial_z X$$

$$K_V = K_o^{iw} + K_o^{sh} f(Ri) :$$

$$K_o^{iw} = 10 \text{ cm}^2/\text{s} \quad \text{Pr} = 10$$

$$K_o^{sh} = (40-100) \text{ cm}^2/\text{s} \quad \text{Pr} = 1$$

$K_V(Ri)$  formulations are popular despite being local

e.g. Pakanowski and Philander, JPO 1981) studied the Equatorial Pacific, but in their 25m upper layer,  $K_V$  is effectively infinite.

## K-Profile Parameterization, KPP (1<sup>st</sup> order, non-local)

Temperature variance equation (2<sup>nd</sup> order) says

$$\langle wq \rangle = -K_q \left( \partial_z Q - \gamma_q \right)$$

OBL of depth,  $h$  for  $0 < (\sigma = d/h) < 1$

$$K_q(\sigma) = h \, w_q \, G(\sigma)$$

Non-local -  $K_q$  knows about  $h$ ,  $\sigma$ , and surface forcing  
-  $\gamma_q$  gives non-zero flux for  $\partial_z Q = 0$ .

## KPP (Vertical Profile)

$$K_q(\sigma) = h w_q G(\sigma)$$

$$G(\sigma) = a_0 + a_1 \sigma + a_2 \sigma^2 + a_3 \sigma^3$$

$a_0 = 0$  ; turbulent eddies don't pass through the surface

$a_1 = 1$  ; then for  $\sigma \rightarrow 0$  ;  $G(\sigma) \rightarrow d/h$  ;  $K_q \rightarrow w_q d$

Consistent with MOS  $w_q = \frac{\kappa u^*}{\phi_q(d/L)}$

$a_2$  &  $a_3$  match  $G(\sigma)$  and its slope at  $\sigma=1$ ; to interior

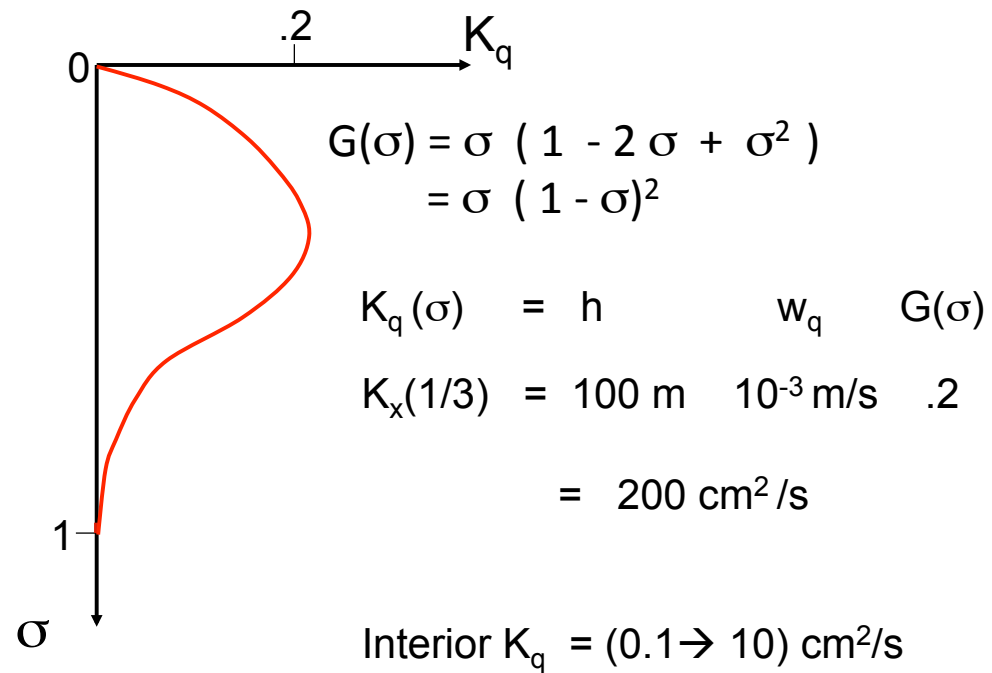
KPP at  $h$ , ( $\sigma = 1$ )

$a_2$  and  $a_3$  used to match  $K_x$  and  $\partial_z K_x$  at  $h$ , ( $\sigma = 1$ )

for  $K_x = \partial_z K_x = 0$  at  $h$

$$a_2 = -2 \quad ; \quad a_3 = 1$$

## KPP Magnitude



## 5) KPP -- non local transport

Empirically :  $\gamma_u = \gamma_v = 0$

$q$  = scalar

$$\gamma_q = 0 \quad ; \quad d/L > 0 \text{ (stable forcing)}$$

$$\gamma_q = \frac{C \langle wq \rangle_o}{w_q h} \quad ; \quad d/L < 0 \text{ (convective forcing)}$$

$$\text{non-local } \langle wq \rangle = K_q \gamma_q = G(\sigma) C \langle wq \rangle_o$$

$C$  is order 10



5) KPP -- boundary layer depth,  $h$

$$Ri_b(d) = \frac{(B(0) - B(d)) d}{|\mathbf{V}(0) - \mathbf{V}(d)|^2 + V_t^2}$$

in a convective OBL :  $Ri_b(d) = \frac{(B(0) - B(d)) d}{V_t^2}$

so  $V_t^2$  is formulated to make  $\langle wb \rangle_e = -0.2 \langle wb \rangle_o$

Empirically

$h$  is shallowest depth where  $Ri_b(h) = 0.3$

## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
4. The Surface Boundary Layer & Similarity Theory
5. The Convective Boundary Layer
6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. **The Viscous Surface Layer**
8. A Practical Example: Diurnal Cycling

## Low Reynolds' Number, Re order 1

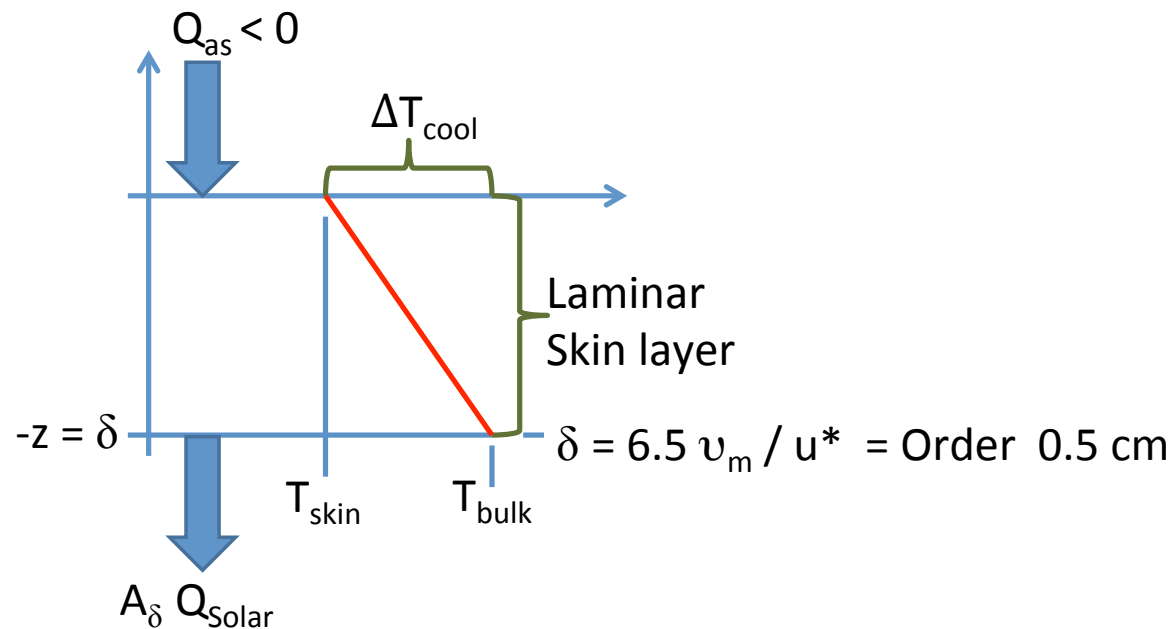
$$\begin{aligned} \partial_t U = & -U \partial_x U - V \partial_y U - W \partial_z U, & \text{Advection (non-linear)} \\ & + f V, & \text{Coriolis (earth's rotation)} \\ & - \rho \partial_x P, & \text{Pressure gradient} \\ & - \partial_z \langle wu \rangle, & \text{Vertical turbulent mixing (non-linear)} \\ & + \nu_m \partial_{zz} U, & \text{Molecular viscosity} \end{aligned}$$

$$\text{Reynolds Number, } Re = \frac{\text{non-linear}}{\text{viscous}} = \frac{d u^*}{\nu_m} = \frac{10^{-2} \cdot 10^{-4}}{10^{-6}} = 1$$

At small  $d$  ( $< 1$  cm) there is a viscous sub-layer !!!

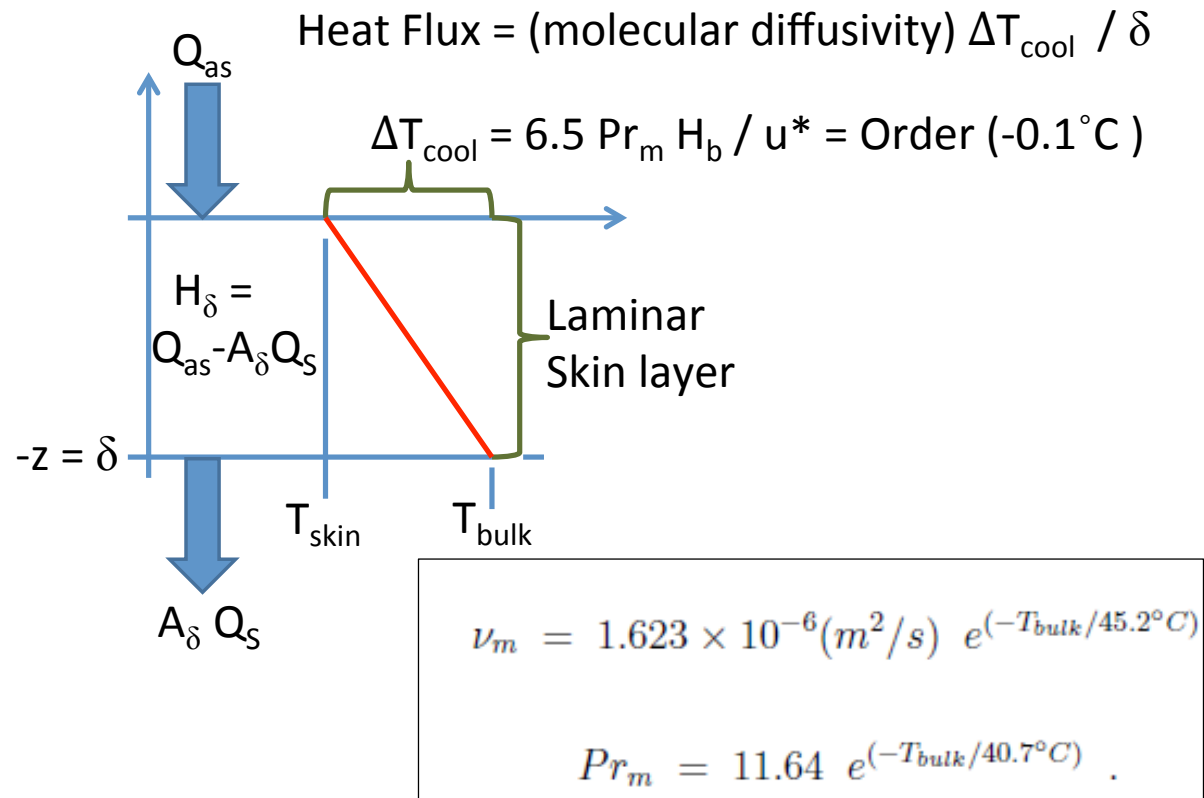
Deeper there is a ( $Re \gg 1$ ) turbulent (3-d) layer !!!

## Viscous Surface Layer Thickness, $\delta$



C.E. Fairall, et. al., 1996, J. Geophys. Res.)

## Sea Surface Cool Skin

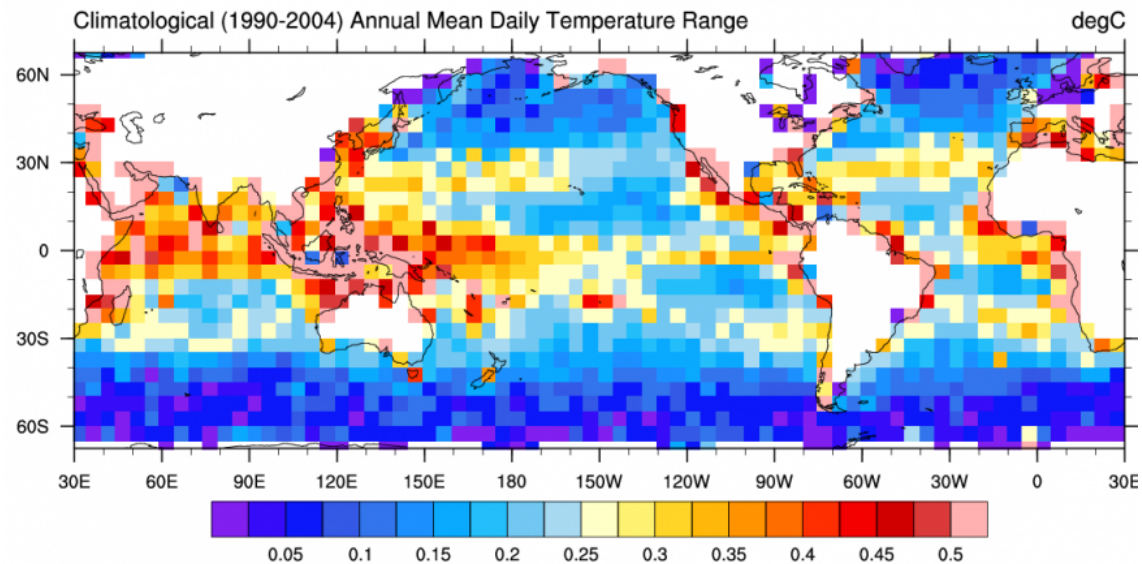


## Outline

1. Non-linear mixing
2. Turbulent Eddy Viscosity and Closures
3. Mixing Regimes in Oceans and Seas
4. The Surface Boundary Layer & Similarity Theory
5. The Convective Boundary Layer
6. Modeling the Surface Boundary Layer
  - Mixed Layer Models
  - First Order Closures
7. The Viscous Surface Layer
8. **A Practical Example: Diurnal Cycling**

# Mean Diurnal Warming

$$T_{\text{skin}}(14:00\text{h}) - T_{\text{skin}}(\text{Night})$$



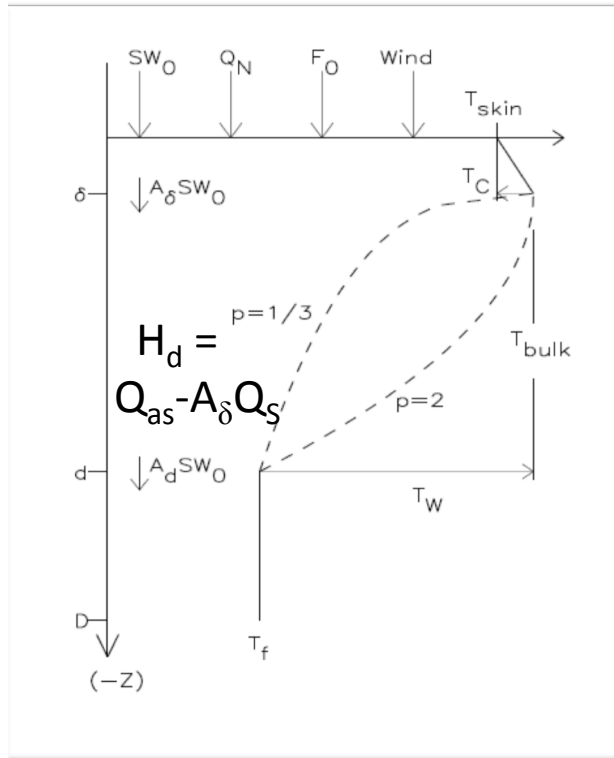
Westerlies  
High latitudes

Trades

Doldrums

Tropics

## Low Reynolds' Number, Re order 1



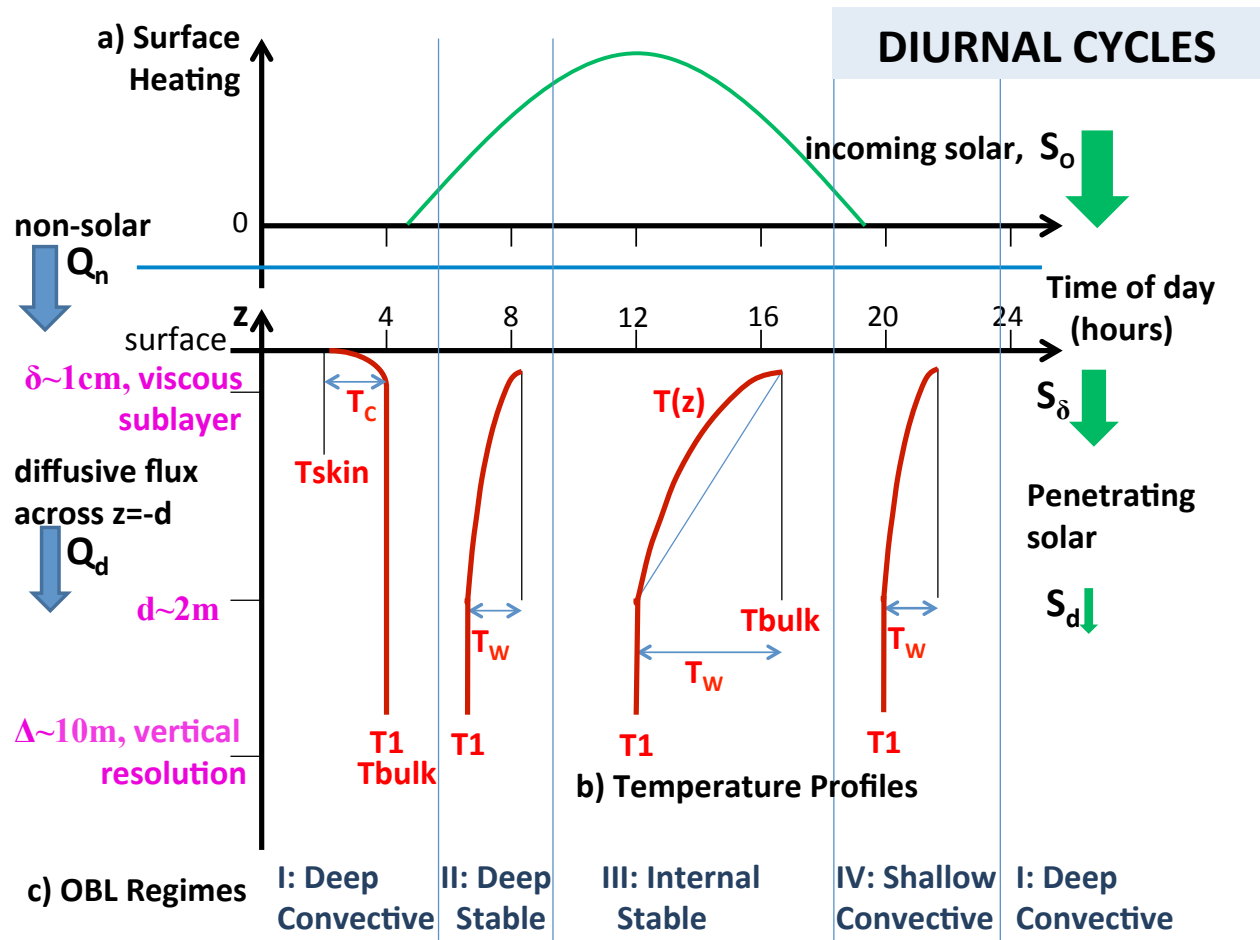
$$T(z) = T_{bulk} - \left[ \frac{(z + \delta)}{(-d + \delta)} \right]^p T_W$$

$$\partial_t T_M = \frac{p}{(p+1)} \partial_t T_W$$

$$K_d \partial_z T(d) = K_d T_W \frac{p}{d}$$

$$\partial_t T_W = H_d \frac{(p+1)}{p d} - K_d T_W \frac{(p+1)}{d^2}$$





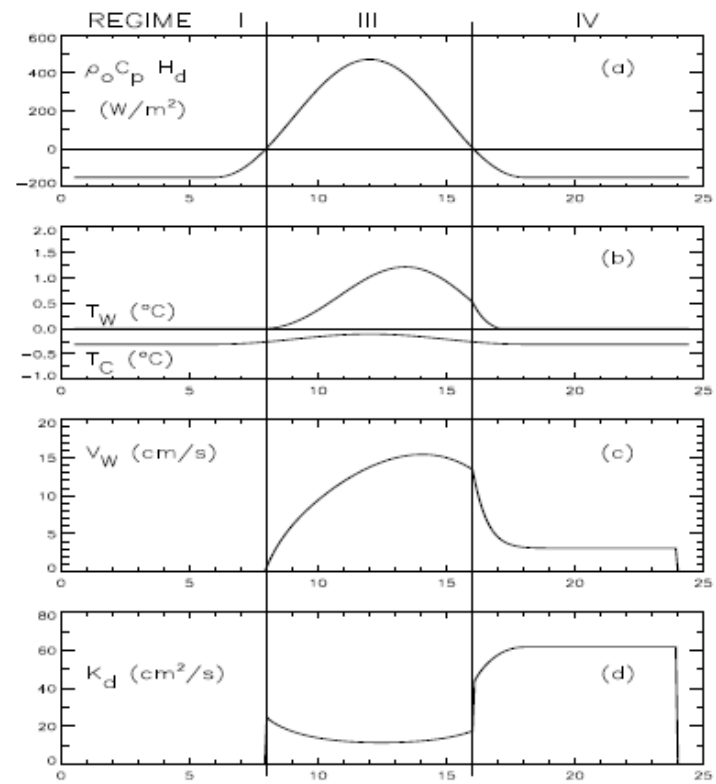
## Diffusivity at $-z = d$ , by Regime

REGIME	$d/L$	$K_d$
I Deep Convective	$< 0$	
II Deep Stable	$0 \rightarrow \Lambda \sim 1$	$\frac{\kappa u^* d}{(1 + 5 d/L)} \left( 1 + a_2 \left[ \frac{d}{\Lambda L} \right] + a_3 \left[ \frac{d}{\Lambda L} \right]^2 \right)$
III Shallow Stable	$> 1$	$\kappa_o + \nu_o \nu(Ri_d)$
IV Deepening Convective	$< 0$	$\kappa u^* d (1 - C_s d/L)^{\frac{1}{3}}$

$$Ri_d = g \frac{(\alpha T_W - \beta S_W)}{V_W^2} \frac{d}{p}$$

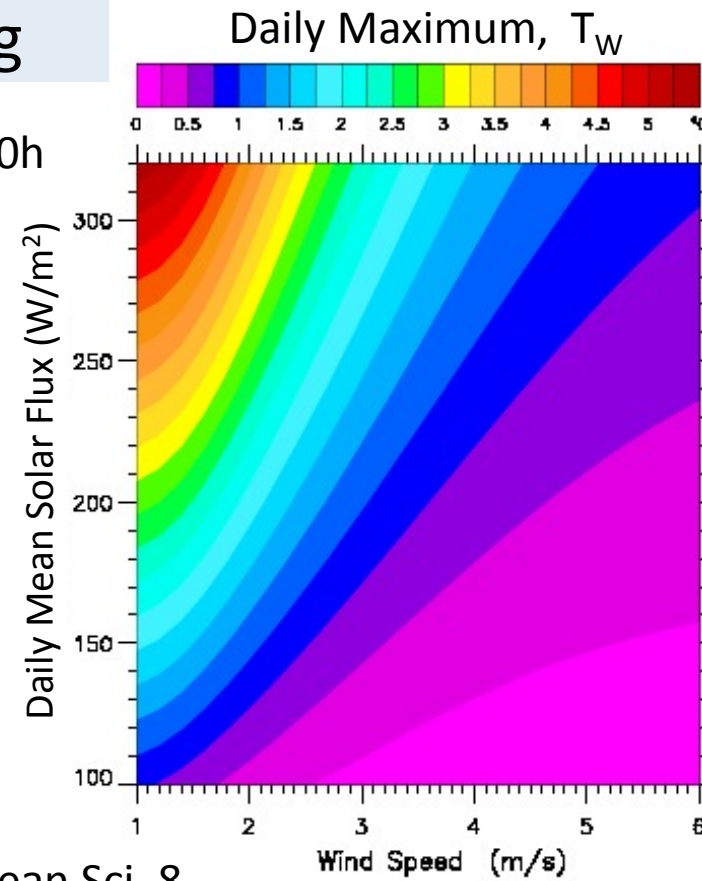
$$C_s \sim 7 ; \Lambda \sim 1$$

## Diurnal Cycles



## Peak Warming

Typically at about 14:00h

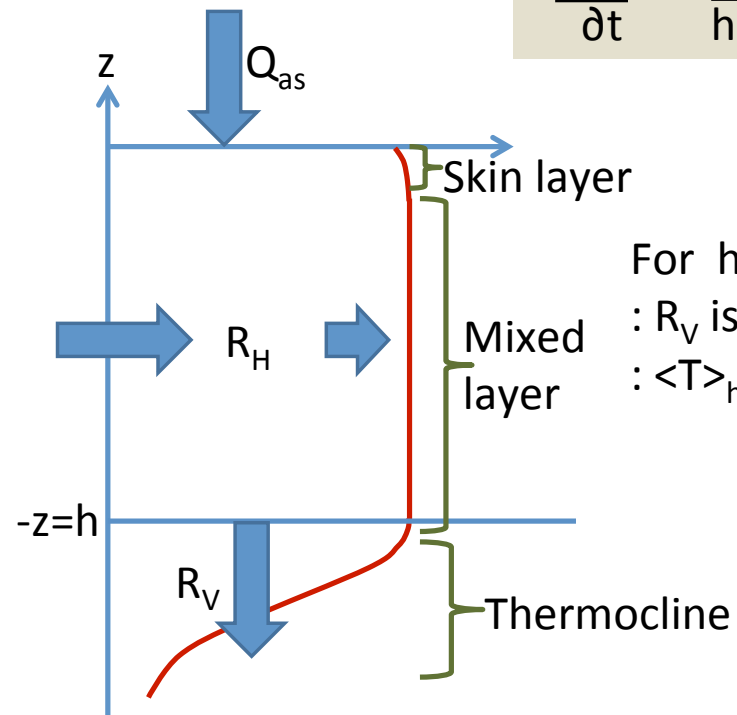


Filipiak, et. al., 2012, Ocean Sci, 8

Fin

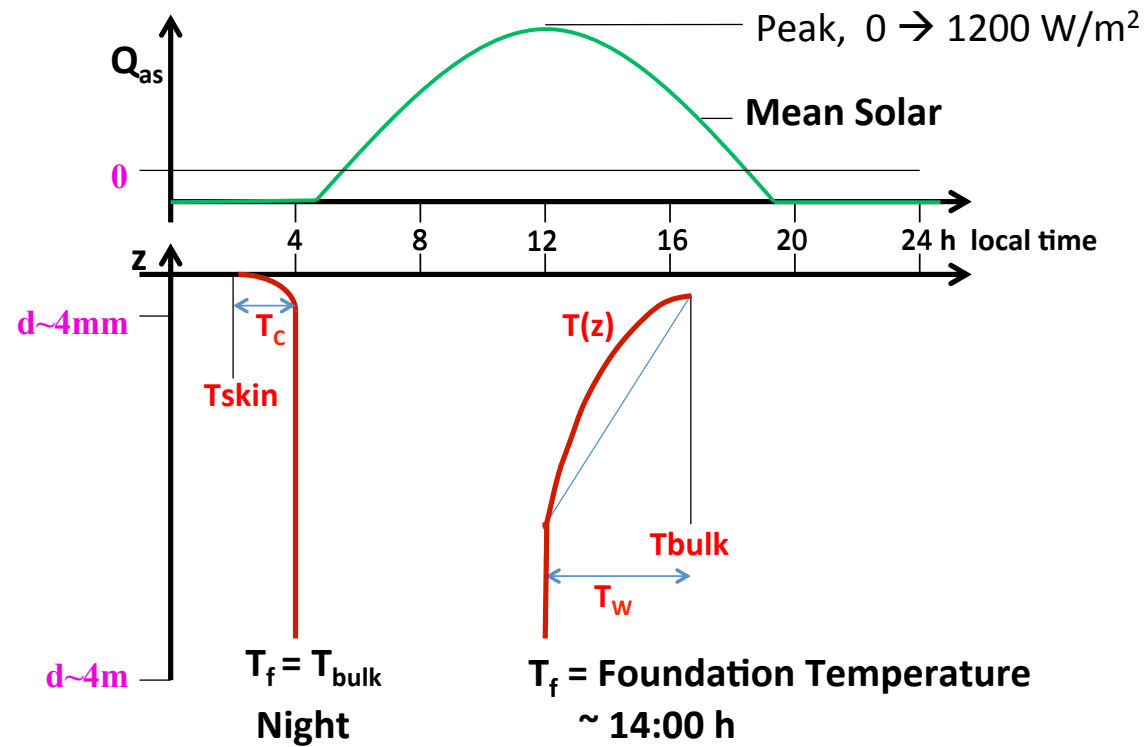
## III.2 A prognostic SST equation

$$\frac{\partial \text{SST}}{\partial t} = \frac{Q_{\text{as}}}{h (\rho c_p)_{\text{ocn}}} - \frac{R_V}{h} + \frac{\partial R_H}{\partial x}$$

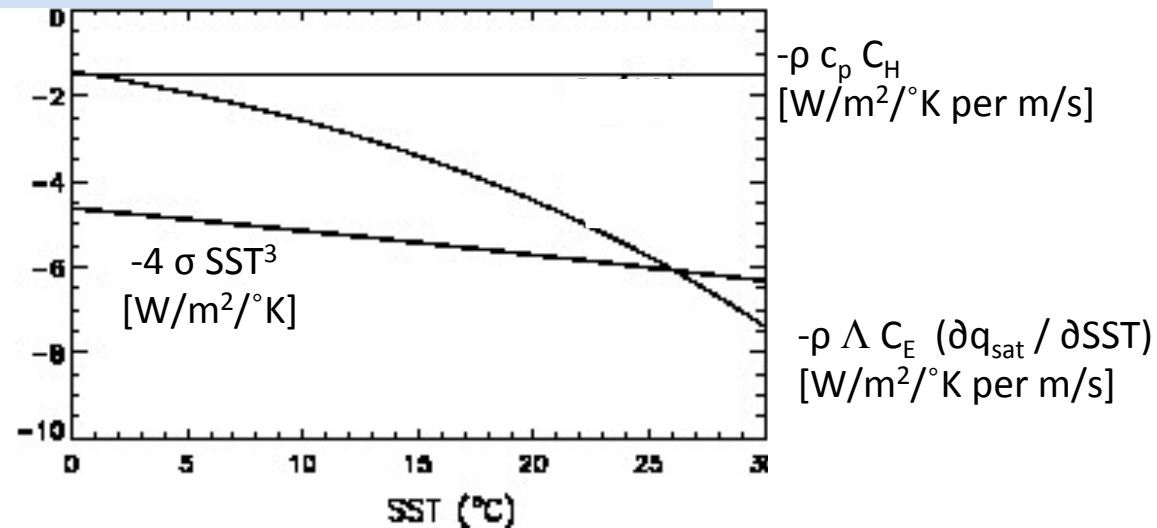


For  $h$  near thermocline top  
:  $R_V$  is tractable  
:  $\langle T \rangle_h \approx \text{SST}$

### III.3 : Diurnal Cycling ( $T_{\text{bulk}}$ )



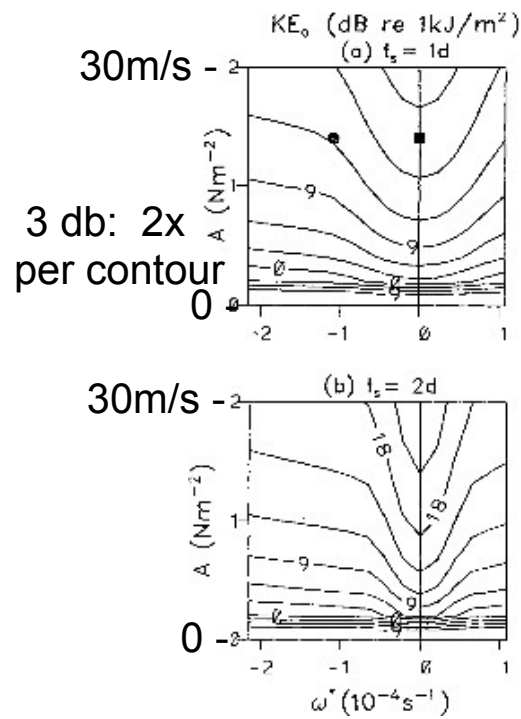
### III.3: Diurnal Heat Fluxes



- Warming 5°C @ 1m/s ; 2°C @ 3m/s
- $-Q_L$  :  $\sim 25 \rightarrow 3.0 \text{ W/m}^2$  ;  $25 \rightarrow 30 \text{ W/m}^2$
  - $-Q_H$  :  $\sim 7.5 \text{ W/m}^2$  ;  $9 \text{ W/m}^2$
  - $-Q_E$  :  $\sim 7.5 \rightarrow 35 \text{ W/m}^2$  ;  $25 \rightarrow 42 \text{ W/m}^2$



Inertial Resonance ,  $KE_0 : \omega^* = (\omega - f)$   
 $\tau = A \sin^n(\pi t/\Delta t) \exp\{-j(\omega^*+f)t/\Delta t\}$



### 3) Evaporation (usually dominates $Q_{\text{nsol}}$ variability)

For a surface evaporation,  $E < 0$ , that increases salinity by  $\Delta S$ , there is a latent heat flux,  $Q_E = \Lambda E$ , that cools the ocean by  $\Delta T$  ( $\Lambda$  is the latent heat of vaporization)

$$\frac{\Delta T}{\Delta S} = \frac{\Lambda}{S_o C_p} = \frac{2.5 \times 10^6 \text{ (j/kg)}}{35\text{psu} \cdot 4000 \text{ (j/kg/ } ^\circ\text{C)}} = 17 ^\circ\text{C/psu}$$

Evaporation changes temperature more than salinity,  
And 90% of the buoyancy change is due to  $\Delta T$ .

Other heat fluxes only change temperature  
Precipitation changes Salinity

## Turbulent Mixing Regimes (changing balance of terms with, $d$ )

